

July 19, 2023

To: All Bidders

From: Kate Bailey Director of Procurement

Re: ADDENDUM NO. 5 23-026.1 - RFP for Design Build of Temperature Controlled Warehouse

This Addendum No. 5 is issued to:

1. Provide the Geotechnical Report. (attached)

All other terms and conditions remain unchanged.

Bidders shall acknowledge receipt of this addendum by immediately emailing a copy of the completed acknowledgment to Kate Bailey at <u>procurement@philaport.com</u>

ACKNOWLEDGMENT OF RECEIPT OF ADDENDUM NO. 5 Project #23-026.1 RFP for Design Build of Temperature Controlled Warehouse

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Philadelphia Regional Port Authority 3460 North Delaware Ave. 2nd Floor Philadelphia, PA 19134

Geotechnical Report



GEOTECHNICAL ENGINEERING SERVICES

PhilaPort Distribution Warehouse Packer Avenue Philadelphia, PA



Submitted To:

Philadelphia Regional Port Authority 3460 N. Delaware Avenue Philadelphia, PA 19134

Submitted By:

Pennoni Associates Inc. 2041 Ave C, Suite 100 Bethlehem, PA 18017

1

Daniel P. Marano Jr., PE Geotechnical Project Engineer



January 25, 2018 (Revised May 13, 2019)

PRPAX 17013.04



January 25, 2018 (Revised May 13, 2019)

PRPAX 17013.04

Ms. Lisa Magee, PE Chief Engineer/Director of Engineering Philadelphia Reginal Port Authority 3460 N. Delaware Avenue Philadelphia, PA 19134

Re: Geotechnical Engineering Services PhilaPort Distribution Warehouse Philadelphia, Pennsylvania

Ms. Magee:

We are pleased to submit our geotechnical engineering report for the referenced project. Work was initiated in general accordance with our revised proposal dated December 6, 2017, and your subsequent authorization to proceed.

In January of 2019 the project details began to finalize, this included building size, location, building loads and finished floor elevation. We have revised our report and recommendations based on the changes described above.

We trust that the information presented herein is what you require at this time and we thank you for the opportunity to assist you with this project. If you have any questions, or if you need any further assistance with this project, please contact this office at your earliest convenience.

Respectfully yours,

PENNONI ASSOCIATES INC.

Daniel P. Marano Jr., PE

Geotechnical Project Manager

Erederick A. Brinker, PE Associate Vice President Geotechnical Division Manager



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1. EXECUTIVE SUMMARY

Pennoni Associates, Inc. (Pennoni) has completed field exploration for the proposed PhilaPort Distribution Warehouse, located in the City of Philadelphia, Pennsylvania. The project area will occupy the existing new car parking lot between Pattison and Packer Avenues. The purpose of our study was to determine the subsurface conditions at the project site within the footprint of the proposed warehouse building, evaluate these conditions with respect to the proposed development, and present foundation recommendations.

It is our understanding the proposed construction consists of an approximate 197,000 ft² dry storage building with 42 loading dock spaces on the west side of the building. The finished floor elevation is anticipated to be established at Elev. 13.5+/-. An approximate 215,000 ft² cold storage addition is proposed on the south side of the dry storage warehouse. It is our understanding that the dry storage building will be approximately 45 ft high and house four storage levels (first level is the floor and three pallet levels supported by pallet racks above). Additionally, the use of high mast fork trucks will be used inside of the building and will require minimal differential settlement in the floor slab (1/8 in.) in order to operate. Typical warehouse column, and floor loads are anticipated not to exceed 70 kips, and 450 psf respectively. Structural loading information was provided by our Structural Technologies group.

Between the period of July 25 through August 1, 2017, five borings were drilled by Allied Well Drilling, as part of a preliminary subsurface exploration conducted by others. Appendix A includes the preliminary boring logs.

Between the period of December 21, 2017 through January 3, 2018, 20 borings were drilled by C.G.C. Geoservices, LLC. within the proposed warehouse building footprint. Appendix A includes the boring logs and the Boring Location Plan.

On April 18 and April 19, 2019, 20 test pits were excavated by Ambient Group within the property; 10 shallow test pits were excavated to evaluate the pavement thickness, and 10 test pits were excavated for the infiltration testing. Appendix A includes all test pits logs.

Based on the results from the above explorations, laboratory testing, engineering analyses, and our experience, we conclude that construction of the proposed warehouse is feasible. Based on the soils encountered and the anticipated loading, it is our professional opinion that the proposed structure can be supported on either shallow foundations after ground improvement (Controlled modulus columns/Rigid inclusions) is performed, or on deep foundations. Additionally, the proposed floor slab has higher than normal loading and limited tolerances for movement, so we recommend that the ground floor slab should be constructed as a structural slab supported on improved soils or deep foundations. Encountering obstructions (construction debris) should be anticipated during foundation and utility installation. Encountering groundwater in excavations (on the order of 6 to 8 ft) should be anticipated. Due to the proximity to the Delaware River the groundwater elevation may vary with the tidal action. On-site existing inert granular portions of the fill soils can be reused in compacted load bearing fill. Detrimental long-term post-construction settlements are not expected if the recommendations provided herein are followed.

This report provides a more detailed summary of the field and laboratory testing program as well as a discussion of the conclusions and recommendations pertaining to design and construction of the proposed structure.



2. INTRODUCTION

2.1. LOCATION

The project site is located west of the Delaware River in south Philadelphia, Pennsylvania. The site is bounded on the north by commercial buildings (seafood market, cold storage, bank) and South Galloway Street followed by Packer Avenue, on the east by South 3rd Street, on the south by Pattison Avenue, on the west by commercial buildings followed by South Lawrence Street.

2.2. PROPOSED CONSTRUCTION

It is our understanding the proposed construction consists of an approximate 197,000 ft² steel frame, dry storage building with 42 loading dock spaces on the west side of the building. An approximate 215,000 ft² cold storage addition is proposed on the south side of the dry storage warehouse. The finished floor elevation of the dry storage building is anticipated to be established at Elev. 13.5+/-. It is also anticipated that the exterior of the buildings will be clad with insulated metal sandwich wall panels with hardening of the lower exterior and interior face of the façade provided via masonry or concrete panel walls. The dry storage building will be approximately 45 ft high and house four storage levels (first level is the floor and three pallet levels supported by pallet racks above). Additionally, the use of high mast fork trucks will be used inside of the building and will require minimal differential settlement in the floor slab (no more than 1/8 in.) in order to operate. Typical warehouse column, and floor loads are anticipated not to exceed 70 kips, and 450 psf respectively. Structural loading information was provided by our Structural Technologies group.

2.3. OBJECTIVES

Our objectives were to determine the subsurface conditions at the project site within the footprint of the proposed building, evaluate these conditions with respect to the proposed construction, and present recommendations regarding:

- foundation design, including a discussion of alternate solutions, if applicable, anticipated total and differential settlements;
- design frost depth;
- floor slab design;
- lateral earth pressure parameters;
- discussion of potential for consolidation and/or differential settlements of substrata encountered;
- "general procedure" Seismic Soil Site Classification in accordance with Table 1613.5.2 of the 2009 International Building Code;
- evaluation and determination of the earthwork requirements for use in preparation of the site area, including material selection and placement operations;
- suitability of on-site material for re-use as fill/backfill as part of the site work for the project;
- ground water conditions;
- removal or treatment of objectionable material, and;
- quality assurance, field-testing, and observations during construction.



3. FIELD AND LABORATORY WORK

3.1. PREVIOUS FIELD WORK

Between the period of July 25 through August 1, 2017, five borings were drilled by Allied Well Drilling, as part of a due-diligence subsurface exploration conducted by others. Soil samples were reported to have been obtained in general accordance with ASTM D 1586. The data obtained from the previous exploration were used in our analyses.

3.2. FIELD WORK

Between the period of December 21, 2017 through January 3, 2018, 20 borings were drilled by C.G.C. Geoservices, LLC. within the proposed warehouse building footprint at the approximate locations presented on Drawing No. LP-1. The boring locations were selected and established in the field by Pennoni personnel. Soil samples were obtained in general accordance with ASTM D 1586 and ASTM D1587 methods. Appendix A includes the boring logs and Drawing No. LP-1.

Our D. Marano, PE directed the field work; our D. Copeland, EIT, and S. Corcoran, performed a site reconnaissance and full-timed monitored the drilling operations.

Additionally, on April 18 and April 19, 2019, 20 test pits were excavated by Ambient Group within the property; 10 shallow test pits were excavated to evaluate the pavement thickness, and 10 test pits were excavated for the infiltration testing. Appendix A includes all test pits logs. The test pits locations were selected and established in the field by Pennoni personnel.

Our D. Marano, PE directed the field work; our N. Rex and E. Iannetti, full-timed monitored the excavating operations.

3.3. LABORATORY WORK

The soil samples collected during our fieldwork were delivered to our laboratory. Representative samples were selected and tested to determine moisture contents, organic contents, plasticity indices, unconfined compressive strengths, volumetric (unit weight, void ratio), gradation and consolidation characteristics of the subsoils. Additionally, laboratory testing data from the preliminary study performed by others was used in our study. Appendix B includes the results from both studies and a list of testing procedures.

4. SITE CHARACTERISTICS

4.1. SITE HISTORY

Review of historical documents dating back to 1940 indicates the site underwent massive earthwork during the 1940's and 50's. Due to the limited detail and resolution of the published data it is not clear what the site was used for during this period. Between 1957 and 1963, two large rectangular commercial buildings were constructed. The buildings stretched from Packer Avenue to Pattison Avenue and were separated in the middle by South Galloway Street.

The site remained largely unchanged through 2013. Between 2013 and present day, the buildings were razed. Evidence of the razed buildings is evident where the ground cover consists of compacted



processed aggregate over the former building footprints. The site is currently being used as a parking lot for new cars.

4.2. SURFACE FEATURES

Currently the project site consists of a bituminous paved parking lot with associated curbing and light pole structures. The groundcover in the areas of the razed buildings consisted of compacted processed aggregate. The topography of the site is "bowl" shaped with perimeter elevations varying from Elev. 12 to Elev. 10 and descend towards the center of the site to approximate Elev. 9 to Elev. 8. Overhead electrical utilities were observed traversing in the northerly/southerly direction the center of the site. Stormwater inlets and associated underground utilizes were observed running bilaterally along the center of the site from the northern limit to the southern limit of the site.

4.3. GEOLOGY

The project site is located within the Lowland and Intermediate Upland section of the Atlantic Coastal Plain Province. The dominant topographic features of this section include very low local relief and a flat upper terrace surface cut by narrow, steep-sided to open valleys, shallow valleys; includes the Delaware River floodplain. The underlying subsurface material types consist of unconsolidated to poorly consolidated sand and gravel deposits, underlain by very complex, faulted and folded schist, gneiss, and other metamorphic rocks.

Available geological data indicates that the subject site is underlain by the Trenton Gravel Formation consisting of gray or pale-reddish-brown, very gravelly sand interstratified with crossbedded sand and clay-silt beds. This formation also includes areas of Holocene alluvium and swamp deposits

Underlying the Trenton Gravel Formation is the Wissahickon Formation. The Wissahickon Formation consists of a coarsely crystalline, excessively micaceous schist. Fracturing results in a well-developed, platy pattern. This formation is fissile to thinly bedded, moderately resistant to weathering, and often highly weathered to a moderate depth.

4.4. SUBSOILS

The borings and test pits revealed bituminous concrete/concrete/processed aggregate pavement or processed aggregate layer at the surface that varied in thickness from 5 to 13 inches. Appendix D presents pavement thickness encountered in all borings and test pits performed on site. The underlying subsoils have been grouped by us into six principal strata based on their physical and engineering properties and our interpretation of their origin. Following are descriptions of the subsoils encountered at this site.

Stratum F – Urban Fill

The borings and test pits disclosed an Urban Fill layer with a thickness that varies from approximately 7 to 18 ft. The fill generally consists of granular fine to medium SAND, some to trace gravel size rock fragments (brick, ash, cinder, glass, organics), some to trace silt, or SILT, some to trace fine to medium sand, some to trace gravel size rock fragments (brick, ash, cinder, glass, organics).

Standard penetration test (SPT) N-values indicate the density/consistency of this stratum varies from "very loose"/"soft" to "very dense"/"very hard". Typical USCS Classifications associated with this stratum are SM, SP-SM, and ML.



Although not encountered in the borings, encountering remnants of previous foundations and shoring systems during construction, should be expected within Stratum F. If encountered, these obstructions will most likely impair the construction process, especially utility and foundation construction.

Stratum 1 – Silty Clay/Clay (Alluvial)

A stratum of Silty CLAY/CLAY with varying amounts of fine sand gravel and organics (7.9% to 10.5%) was encountered beneath Stratum F fill in many of the borings. The thickness of this layer varies from approximately 5 to 15 ft. SPT N-values indicate the consistency of this soil varies from "very soft" to "firm". The typical USCS Classifications associated with this stratum are OL and OH.

Consolidation testing disclosed a preconsolidation pressure (tsf), compression and recompression index of 0.95, 0.49 and 0.03, respectively. Laboratory testing and visual classification disclosed this layer contained trace to little organics. These data disclose Stratum 1 soils to be compressible.

Stratum 2 – Clayey SILT (Alluvial)

A stratum of SILT with varying amounts of fine sand, gravel and organics (up to 26.2%) was encountered beneath the Stratum F Fill or Stratum 1 soils in many of the borings. The thickness of this layer varies from approximately 5 to 15 ft. SPT N-values indicate the consistency of this stratum varies from "very soft" to "stiff". Typical USCS Classifications associated with this stratum are OH and ML.

Laboratory testing and visual classification disclosed this layer contained trace to some organics. The percentage of organics in Stratum 2 is generally associated with high compressibility, significant secondary compression, often unsatisfactory strength characteristics, and low unit weight. This stratum is also considered compressible.

Stratum 3 – Sand/Gravel (Alluvial)

A stratum of SAND ranging in gradation from poorly (generally, gap graded fine to medium) to well graded with varying amounts of gravel and silt, or GRAVEL with varying amounts of sand was encountered beneath Strata 1 and 2. The thickness of this layer varies from approximately 10 to 32 ft. SPT N-values indicate the relative density of this stratum generally varies from "very loose" to "medium dense". Typical USCS Classifications associated with this stratum are SP and SP-SM.

Stratum 4 – Sand/Gravel (Alluvial)

A stratum of well graded SAND with varying amounts of gravel, or poorly to well graded GRAVEL with various amounts of sand was encountered above and/or beneath Stratum 3 in the borings. Stratum 4 was generally encountered at depths ranging from 43 to 80 ft below the ground surface. SPT N-values indicate that the density of this stratum generally varies from "medium dense" to "very dense". Typical USCS Classifications associated with this stratum is SW-SM, GM and GP.

It should be noted that COBBLES encountered Borings B-2 and B-12 at depths ranging from 45 to 50 ft below the ground surface were included in this Stratum. The material was observed when the augers were extracted.



Stratum 5 – Raritan Clay

A stratum of CLAY/Sandy CLAY with varying amounts of fine sand and gravel was encountered beneath and or between Stratum 4 in some of the borings. Stratum 5 was generally encountered at depths ranging from 53 to 80 ft below the ground surface and generally varies in thickness from approximately 5 to 7 ft. SPT N-values indicate the consistency of this soil varies from "stiff" to "very hard". The typical USCS Classification associated with this stratum is CL.

Auger refusal was encountered in Borings B-2 and B-12 at depths of 47 and 50 ft below existing grades, respectively. Auger refusal is thought to be due to cobbles, rather than the top of rock.

4.5. GROUND WATER

Observations for groundwater were made in the borings during sampling and shortly after completion of drilling. Evidence of groundwater was generally encountered in the borings at depths of approximately 6 to 13 ft below existing grades (Elev. 6.5 to Elev. 0.0). Borings B-17, B-18 and B-20 disclosed evidence of groundwater at depths ranging from 18 to 28 ft below existing grades (Elev. -2.0 and Elev.-11.5), respectively. It is our professional opinion that these latter readings were affected by hydraulically restrictive Stratum 1, and not indicative of the static groundwater table.

Additionally, evidence of ground water was generally encountered in test-pits at depths of approximately 8 to 10.5 ft below existing grades. These observations are for the times indicated and may not be indicative of seasonal, daily or tidal variations in the ground water levels.

Given the project site's vicinity to the Delaware River, daily fluctuations in the groundwater table could be influenced by the tide. Daily and seasonal variations of several feet should be anticipated.

5. ANALYSES AND RECOMMENDATIONS

5.1. SEISMIC SITE CLASS

The borings disclosed subsurface conditions generally described according to the 2015 International Building Code (IBC) as having a soil-profile corresponding to Site Class E – soft clay soil profile.

5.2. SITE WORK

Comparison of the proposed grades to existing grades indicates that cuts as on the order of 1 ft deep and fills up to 5 ft high are expected to establish the ground floor slab. Comparison of the proposed grades to existing grades indicates that cuts as deep as 3 ft and fills up to 2 ft high are required for general site grading. The borings and laboratory testing disclosed Stratum 1 and 2 are compressible. Fills greater than 2 ft high will likely result in consolidation related settlement, which may be significant (> 3 inches). New fills should be placed as early as possible within the construction schedule to allow for settlements to occur.

Prior to the construction of foundations, structural slabs, and pavements, any bituminous concrete must be removed from within the proposed areas of construction. Existing utilities located within the proposed building footprint should be abandoned and relocated outside the limits of the new structure. Any existing



utility line abandoned in-place should be grouted or the line should be removed and the trench appropriately backfilled.

From historic aerial photography, it was disclosed that the site was once partially occupied by structures and associated paved parking. At the time of our field work evidence of previous structures was observed throughout the razed building footprints; however, remnants of the former foundations were not observed, or evident in the borings. The excavation of test pits prior to construction should be considered to better determine if remnants of the previous building will interfere with construction.

Any exposed subgrade should be proof-rolled in the presence of Pennoni personnel in an attempt to disclose unstable surface areas. During proof-rolling, any unstable area found should be stabilized by excavating and replacing those soils with suitable soil that is adequately compacted. This can be accomplished by properly adjusting the moisture content of the subgrade soils and compacting them, or by other methods (placing a geotextile and stone layer, etc.).

Our experience indicates that the clean inert granular portions of the Fill stratum can be reused in a compacted fill for backfill of utility excavations as long as it has a maximum particle size of 3 in., and is free of trash, environmental hazards, and other deleterious material. Additionally, demolition debris consisting of concrete and pavement millings can be used in compacted load bearing fills provided there are no environmental hazards associated with the materials and it is crushed to reduce the maximum particle size to less than 3 inches. Adjusting the moisture content prior to fill placement should be expected. Stratum 1 and Stratum 2 soils are not suitable, in their current state, for re-use in compacted load bearing fill.

Imported structural fill should be selected from suitable borrow sources and be approved by the Geotechnical Engineer's representative well in advance of fill construction. Granular fill ideally should consist of well-graded material with not more than 20 percent passing the No. 200 sieve and have a plasticity index not greater than 8 percent; PennDOT 2A, modified stone or recycled concrete can be considered. Other gradations can be considered based on laboratory testing and at the discretion of the Geotechnical Engineer.

Granular fills should be placed in layers not exceeding 10 to 12 in. loose thickness. This criterion might be adjusted by the geotechnical engineer in the field depending on the conditions present at the time of construction, on the compaction equipment used, and on the fill material selected. Fills for support of foundations and pavement should be compacted to at least 98 percent and 95 percent, respectively, of the laboratory determined maximum dry density, ASTM D 698, when small, hand-operated compaction equipment is used, and to at least 95 percent and 93 percent, respectively, of the laboratory determined maximum dry density, ASTM D 698, heavy–duty construction equipment is used. Fills should extend a minimum of 5 ft beyond the exterior edge of a loaded area and have side slopes not steeper than 2 horizontal to 1 vertical.

Specifications should indicate that the percentage of maximum dry density attained in the field is not the only criteria to be used for assessing fill compaction. Observation of the behavior of the fill under the loads of construction equipment should also be used. If the test results indicate that the percentage of compaction is being achieved, but the soil mass is moving under the equipment, placement of additional fill should not be continued until the movement is stabilized. Otherwise, settlement of the fill may occur.



5.3. FOUNDATIONS

Based on the soils encountered and the anticipated loading, it is our professional opinion that the proposed structure should be supported on shallow foundations bearing on improved soils or deep foundations. Controlled Modulus Columns/Rigid Inclusions (CMC's/RI's) can be considered to sufficiently improve the subsoils to allow the construction of shallow spread foundations. Alternatively, deep foundations like concrete filled steel pipe piles and auger cast-in-place piles can be considered for support. Because of the load carrying capacity of the deep foundations, as described, pile load tests (compression and tension) will be necessary.

5.3.1. CMC's/RI's

In order to support the structure on shallow spread footings we recommend improving the subgrade soil by installing CMCs/RIs elements. These elements improve the existing soil conditions to reduce both total and differential settlements by increasing the overall stiffness of the soil mass. A load transfer platform (LTP), sometimes reinforced with a geogrid, is constructed above the CMCs/RIs using granular fill with a thicknesses that may vary from 12 to 36 inches. CMCs/RIs are installed by a drill rig with a specially designed auger that drills down to the designed termination depth followed by a controlled pressure grouting during extraction. The instillation of the CMCs/RIs results in generating minimal auger spoils and vibration. Spread footings can then be designed to bear in the LTP layer for a maximum allowable net bearing capacity of up to 6,000 psf.

Continuous and isolated footings should be at least 1.5 ft wide and 3 ft square, respectively, to prevent localized shear failure in soil. The subgrade of all exterior footings exposed to freezing temperatures, during construction and/or the life of the structure should be established at least 30 in. below adjacent exposed grades or otherwise protected against frost action. Foundation subgrades should be checked by a representative of Pennoni to confirm conditions suitable for support of the design bearing pressure. Where an area is questionable, it should be further explored and/or remedied by removal and replacement of unsuitable material.

5.3.2. Concrete-filled Steel Pipe Piles

Concrete-filled steel pipe piles with an outside diameter (OD) of 16 in. and a minimum wall thickness of 0.5 in. driven into the dense to very dense sand and gravel deposit (Stratum 4) can be considered. Our analyses indicate piles installed to the recommended depths can obtain an allowable load carrying capacity in compression up to 125 tons. A temporary increase in the capacity of up to 33% can be applied to transient loads including wind, etc.

Based on the findings of the test borings and our analyses, the pile tips will be located approximately 60 to 80 ft. below the existing grades. The steel pipe pile should conform to ASTM A-252, Grade 3, specifications. The piles should have a flat boot plate of at least 2 in. thickness fully welded at the tip and flush with the outside wall of the pipe (no projection). The minimum pile spacing should be at least 3 times the pile diameter. In addition to the allowable compression capacity recommended above, the vertical piles can be designed for an allowable uplift capacity of 25 tons, and an allowable lateral capacity of 8 tons per pile.



To facilitate pile installations, the piles may be installed by pre-augering through upper portions of fill layer, if necessary. After pre-augering, the piles should be driven into the dense to very dense sands of Stratum 4, to attain the recommended design capacity. The piles should be driven for at least the last 10 ft. of their length to a resistance determined in accordance with Pile Dynamic Analysis (PDA) testing a suitable dynamic formula, such as a WEAP Analysis, and as verified by successful pile load tests. Production piles may be used for load tests.

5.3.3. Auger Cast Piles

Auger Cast Piles (ACIP) can also be considered for support of the proposed structure. This pile type is constructed by first drilling to the pre-determined depth/elevation using a standard continuous flight auger that removes or displaces material. After reaching the design depth, cement grout is injected, under pressure, as the auger is gradually withdrawn, forming an uncased grout shaft. A 28-day compressive strength of at least 5,000 psi is recommended for the cement grout. The pile shaft can be reinforced with one full-length reinforcing bar extending to the bottom and, if necessary, a reinforcing steel cage can be installed into the upper portion of the grout column while the grout is still fluid.

The piles will derive their capacity by a combination of skin friction and end bearing. An 16-in. diameter ACIP pile will have an estimated allowable axial load carrying capacity of 100 tons per pile. These piles should be constructed estimated to depths of 60 to 80 ft. below existing grade. We estimate these piles as described will have tension and lateral capacities on the order of 50 tons and 8 tons per pile, respectively.

Piles designed to resist uplift loads (tension) should have reinforcing steel extending all the way to the pile tip. Moreover, piles subjected to lateral loads should have properly designed reinforcing in the upper portion of the pile shaft. We further recommend that the piles designed to carry uplift and lateral loads be spaced at least 3 pile diameters apart. The final design and/or allowable capacities should be determined by a specialty contractor with adequate experience in auger cast concrete pile design and construction. Production piles may be used for load tests but should failure occur, the pile can no longer be used. The auger cast pile installer is responsible for closely monitoring the pile during the load test and proving the pile was damaged during testing.

5.4. LOAD TESTING

CONCRETE FILLED STEEL PIPE PILES

The Wave Equation analysis should be used to determine the suitability of the proposed driving equipment. The contractor should incorporate the results of the wave equation analysis within any submittals that are due prior to construction for approval. Consideration should be given to performing dynamic monitoring on a minimum of 5% piles using a Pile Driving Analyzer (PDA). The PDA will provide information on the actual driving stresses, verification of ultimate geotechnical resistance, energy transfer efficiency, pile damage assessments, and verify the refusal criteria during pile installation. A minimum factor of safety of 2.25 should be used during the PDA testing to confirm the recommended installed pile capacity. In addition to the PDA we recommend that static load test piles be installed to better define pile length(s) and to confirm/refine pile installation procedures. We recommend that 2 sets of static load tests (axial, tension and lateral) be conducted.



We recommend that the installation of each pile should be monitored and documented by geotechnical personnel under the direct supervision of a professional engineer.

ACIP

Prior to production pile installation, we recommend that test piles be installed to better define pile length(s) and to confirm/refine pile installation procedures. We recommend that 2 sets of static load tests (axial, tension and lateral) be conducted and dynamic tests conducted on 5% of the production piles. The dynamic integrity testing for the auger cast piles should consist of Pile Integrity Testing (PIT) to confirm the construction of the piles.

GENERAL PILE LOAD TESTING RECOMMENDATIONS

The proposed pipe and auger cast piles are essentially a combination of tip bearing and/or friction piles. The load tests must verify a safe load carrying capacity and they must demonstrate that only a very small net settlement will occur while the full design load is carried by the pile. Therefore, the load test should be conducted in such a fashion and provided with such instrumentation that the loads carried by the pile shaft and pile tip, and the strains of the top, mid-point, and base of the test pile can be measured, where feasible.

The maximum test load should be not less than specified by Code and it is recommended to be higher to facilitate total load transfer to the tip of the pile. Experience has shown that testing a pile to a load greater than the Code requirement, although costlier initially, can prove advantageous during installation because of inconsistencies during construction. Therefore, we recommend that a maximum test load at least 2.5 times the maximum design load carrying capacity of the selected pile should be considered for evaluating maximum load carrying capabilities and load-settlement relationships.

Static and dynamic load tests should be conducted in accordance with the provisions of the latest version of the ASTM Standards. For static testing instrumentation, load test set-up, and loading procedures should be governed by ASTM D-1143 except that the procedures described under "Apparatus for Measuring Movements", "Lateral Movements", and "Incremental Loading Procedures" should be mandatory. PDA testing on driven piles should be performed in accordance with ASTM D-4945.

The geotechnical engineer should select load test locations. Load tests should not be production piles; if the pile/soil interface is failed during testing it will no longer be capable of supporting loads. No construction activity transmitting vibratory or impact loads should be permitted on the project site during load testing. The load test set-up should be protected from inclement weather (wind, rain, intense heat, sunlight, etc.), provided with lights for nighttime readings, and guarded on a full-time basis.

Technical details of the intended pile installation equipment and of the load test set-up (sketch, description, etc.) together with certification of the loading device, etc. should be submitted to the geotechnical engineer at least 1 week in advance of load test construction. Each load test must be monitored on a full-time basis and test results analyzed by a registered geotechnical engineer.



5.5. SETTLEMENT

Settlement of a soil mass is a function of the characteristics of the supporting materials and the stresses imposed on the soils from an external source. Our calculations indicate that settlements will occur due to the stresses imposed on the subsoils by newly placed load bearing fill for site fills and are proportional to the amount of pressure applied (fill height). Additionally, the organic layer of soil was determined to contain approximately 26% of organic material. Long term, secondary settlement is also anticipated in this layer as the material breaks down and consolidates.

The fill heights and secondary settlement may lead to uneven settlement below the floor slab. Therefore, consideration should be given to suspending the utilities from the structural slabs to prevent any serious differential movements in different portions of the utilities. Moreover, flexible connections should be used where the suspended pipes meet the outside pipelines not supported by piling.

Provided the building and structural slab are supported on deep foundations (driven piles, ACIP piles), determinantal total and differential settlements are not anticipated.

5.6. STRUCTURAL SLAB

Because of the differential settlement tolerances the ground floor slab should be designed as structural slab supported by piles and grade beams or they should be designed as "flat plates" supported by piles. The required new fill to attain the finish ground floor subgrade level should be placed as recommended in the Earthwork Section 5.2 to serve as an underside form for slab construction, but it will eventually settle away from the bottoms of the slabs due to consolidation of the compressible organic silt layers.

5.7. GROUND WATER AND SURFACE WATER MANAGEMENT

Observations for groundwater made in each test pit and boring indicate that water was generally encountered 6 to 13 ft. below existing grades. Water table fluctuations may occur with the tidal action of Delaware River. Static water levels could affect utility installation if they are proposed at depths greater than the Mean High Water (MHW) Elevation. The use of sumps and pumps should be expected; well points and/or a sheeting/shoring system comprised of steel interlocking sheeting and high capacity pumps may be required to control ground water during utility installation in deeper excavations (>5 ft. deep).

Surface runoff should be prevented from entering or ponding in excavations by creating soil berms or diversion swales along the perimeter, if the excavation will be left open for an extended period. Where ponding does occur, the water should be removed immediately by pumping. Grades should then be established to prevent further ponding.

5.8. LATERAL EARTH PRESSURE PARAMETERS

The soil parameters presented in Table 1 can be used to estimate earth pressures to design below grade structures and temporary shoring. If the top of the structure is restrained from movement, thereby preventing the mobilization of active soil pressures, the structure should be designed using the at-rest pressure coefficient.



The earth pressure coefficients are based on the assumption of vertical walls, horizontal backfill, no surcharges, no wall friction, and a safety factor of 1.0. A clear distance of 10 ft should be maintained during construction, between perimeter walls and stored materials or the wall must be design to resist the surcharge load from the stored materials. Where sufficient drainage cannot be provided to intercept and re-direct seepage and perched water from structures, hydrostatic pressures must also be considered in the design.

| | | Strata | | | | | | | | | | | |
|---|------|--------|------|------|------|------|--|--|--|--|--|--|--|
| Parameter | F | 1 | 2 | 3 | 4 | 5 | Processed Aggregate (PennDOT Type 2A) | | | | | | |
| Unit Weight (pcf) | 120 | 100 | 90 | 125 | 130 | 118 | 135 | | | | | | |
| Angle of Internal Friction (degrees) | 28 | 17 | 23 | 32 | 38 | 32 | 38 | | | | | | |
| Cohesion (psf) | - | 200 | 0 | - | - | 1000 | - | | | | | | |
| Friction Factor (concrete) | 0.35 | 0.20 | 0.20 | 0.40 | 0.50 | 0.40 | 0.50 | | | | | | |
| Friction Factor (steel) | 0.25 | 0.20 | 0.20 | 0.25 | 0.30 | 0.25 | 0.30 | | | | | | |
| k _a | 0.36 | 0.55 | 0.44 | 0.31 | 0.24 | 0.31 | 0.24 | | | | | | |
| k _o | 0.53 | 0.71 | 0.61 | 0.47 | 0.38 | 0.47 | 0.38 | | | | | | |
| kp | 2.77 | 1.83 | 2.28 | 3.25 | 4.20 | 3.25 | 4.20 | | | | | | |

Table 1. Lateral Earth Pressure Design Parameters

5.9. CONSTRUCTION DIFFICULTIES

Experience has shown that remnant construction and obstructions are often encountered when building within similar, previously developed urban sites. Encountering remnants of previous foundations and shoring systems should be expected. If encountered, these obstructions will most likely impair the construction process. Existing foundations or other structural components disclosed should be removed to a minimum depth of 18 in. below the bottom of new ground floor slabs and 36 in. below the bottom of new foundations.

6. RECOMMENDATIONS FOR FURTHER GEOTECHNICAL SERVICES

Our experience on numerous construction projects is that the interests of the project team are best served by retaining the Geotechnical Engineer to provide construction observations during earthwork and foundation construction operations. To determine if soils, other materials, and ground water conditions encountered during construction are similar to those encountered in the borings and test pits, and that they have comparable engineering properties or influences on the design of the structures, we recommend that Pennoni should provide field observation services during pile driving and load testing, and excavation; construction of compacted fill; preparation of foundation, floor slabs, and pavement subgrades; and installation/construction of foundations, floor slabs, and pavements. Pennoni's Geotechnical Technology should review specifications for earthwork and foundation design/construction when they are prepared.



7. LIMITATIONS

This work has been done in accordance with our authorized scope of work and in accordance with generally accepted professional practice in the fields of geotechnical and foundation engineering. This warranty is in lieu of all other warranties either expressed or implied. Our conclusions and recommendations are based on the data revealed by this exploration. We are not responsible for any conclusions or opinions drawn from the data included herein, other than those specifically stated, nor are the recommendations presented in this report intended for direct use as construction specifications.

This report is intended for use with regard to the specific project described herein; any changes in loads, structures, or locations should be brought to our attention so that we may determine how they may affect our conclusions. An attempt has been made to provide for normal contingencies but the possibility remains that unexpected conditions may be encountered during construction. If this should occur, or if additional or contradictory data are revealed in the future, we should be notified so that modifications to this report can be made, if necessary. If we do not review relevant construction documents and witness the relevant construction operations, then we cannot be responsible for any problems that may result from misinterpretation or misunderstanding of this report or failure to comply with our recommendations.



APPENDICES



APPENDIX A - Field Data

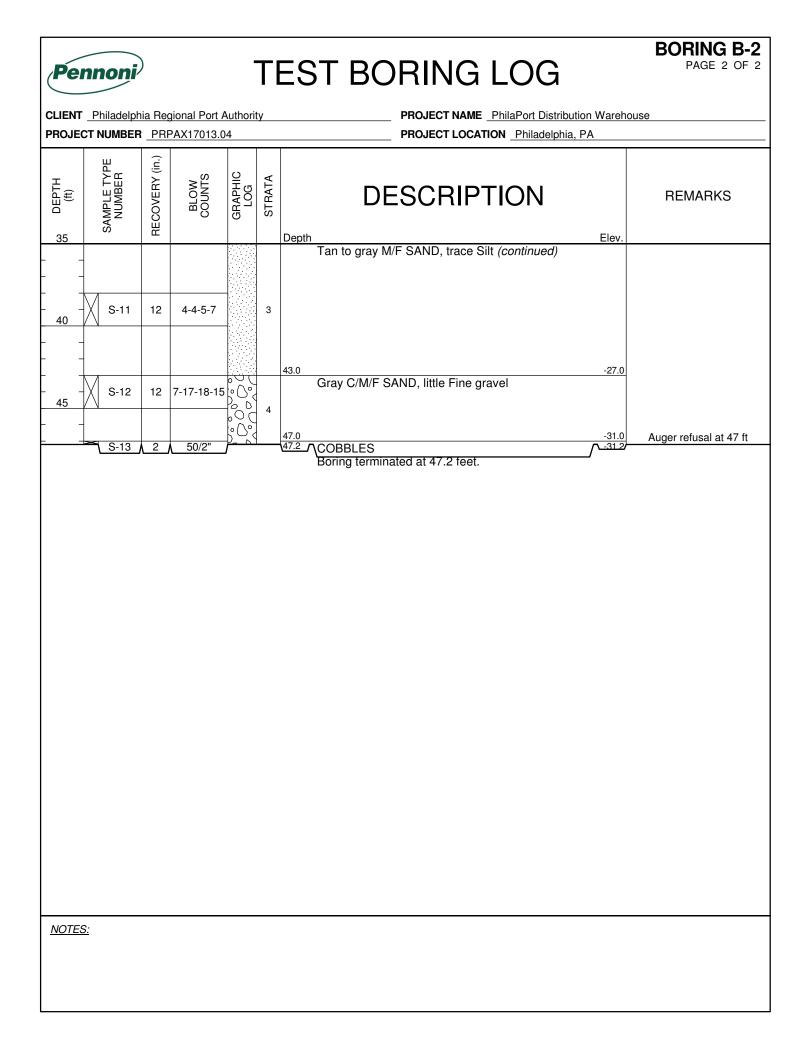


| Pe | nnoi | ņi) | | | Т | ES | ST BORING LOG | BORING B-1 PAGE 1 OF 2 |
|-----------------|------------------------|----------------|-----------------|----------------|------------------|--------|--|---------------------------|
| CLIENT | Philade | elphia R | egional Port | Authori | ty | | PROJECT NAME PhilaPort Distribution Warehou | se |
| | | | RPAX17013.0 | | | | PROJECT LOCATION _ Philadelphia, PA | |
| DATE S | | | | | | | | |
| DRILLI | NG CONT | RACTO | R CGC Geo | oservic | es, L | LC | WATER ENCOUNTERED: | |
| DRILLI | NG METH | IOD Ho | llow Stem A | uger | | | Ū DURING DRILLING <u>13.00 / Elev 2.50</u> | |
| | | | c Blemings | | | | AT END OF DRILLING | |
| LOGGE | D BY _S | . Corcor | an | CHE | CKE | D BY _ | D. Marrano AFTER DRILLING | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | | Deptl | | REMARKS |
| | | | | | Р | 1.0 | 5.0 in. BITUMINOUS CONCRETE 14.5 | |
| | S- | 1 12 | - | | | 2.0 | AND F/M SAND, trace Silt | |
| | -X s-: | 2 24 | 16-20-32- 40 | | | 4.0 | FILL: Black to tan F/M SAND, little Fine Gravel, trace Silt, trace Brick Fragments | |
| 5 | S- | 3 24 | 23-20-21- 27 | | | 6.0 | FILL: Black to tan F/M SAND, some Fine Gravel, Cinder Fragments | Petroleum odor |
| | - S | 4 12 | 15-8-9-7 | | | 8.0 | FILL: Black to red F/M SAND, little Fine Gravel, some Brick Fragments, trace Cinder and Concrete | |
| 10 | - S- | 5 12 | 4-4-5-5 | | F | | Fragments FILL: Black to dark gray Silty CLAY, some F/M Sand, trace Brick and Cinder Fragments | |
| | - | | | | | 13.0 | FILL: Dark gray Silty CLAY AND F/M SAND, some organic pieces of Wood, trace Cinder 2.5 | |
| | - S- | 6 12 | 3-2-3-2 | | | | FILL: Dark gray Fine SAND, Micaceous, some Silt | |
| | - | | | | | 18.0 | -2.5 | |
| 20 | s- | 7 24 | WOH/12"- 2-2 | | | 10.0 | Dark gray Silty CLAY, trace Fine Sand | |
| | - | | | | 1 | | | |
| | | | | | | 23.0 | -7.5 Gray F/M SAND AND brown SILT, little Organics | |
| 25 | S- | 8 12 | 1-1-1-1 | | • | | | |
| | $\left \right\rangle$ | | | _ | | 28.0 | -12.5 | |
| | - X s- | 9 20 | 5-6-4-7 | | 3 | | Gray to tan M/F SAND, trace Silt | Added mud |
| | | | | | - - - - | | | |
| 35 | S-1 | 0 18 | 4-6-9-9 | | | | | |
| <u>NOTE</u> | <u>S:</u> | _ | | _ | _ | _ | | |
| | | | | | | | | |

| Pe | nnoni |) | | • | BORING B-1 PAGE 2 OF 2 | | | | | | | |
|-----------------------|-----------------------|----------------|------------------------------|----------------|---------------------------|--|----------------|--|--|--|--|--|
| | Philadelph | | | | ty | PROJECT NAME _ PhilaPort Distribution Warehouse PROJECT LOCATION _ Philadelphia, PA | | | | | | |
| HLLAID DEPTH 35 | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | DESCRIPTION | REMARKS | | | | | |
| - 40 | S-11 | 12 | 8-9-13-15 12-26-20- 15 | | 3 | Gray to tan M/F SAND, trace Silt <i>(continued)</i> 38.0 -22.5 Brown to tan to gray F/C GRAVEL, some C/M/F Sand, trace Silt | Very wet | | | | | |
| | S-13 | 0 | 10-14-13-25 | | 4 | 48.0 -32.5 NO RECOVERY 53.0 -37.5 NO RECOVERY | Ducking angul | | | | | |
| | S-14 | 0 | | | | 58.0 -42.5 White C/F GRAVEL, little C/M/F Sand, trace Silt 60.0 -44.5 Boring terminated at 60.0 feet. | Pushing gravel | | | | | |
| | | | | | | Boring terminated at 60.0 feet. | | | | | | |
| <u>NOTE</u> | <u>S:</u> | | | | | | | | | | | |

| Pe | nnc | oni |) | | | Т | ES | ST BO | RING LOG | | BORING B-2 PAGE 1 OF 2 |
|--|-------------------|--------|----------------|----------------|------------------|--------------------------------------|------|--------------------------------|---|------------|---------------------------|
| CLIENT | Phila | adelph | ia Rec | nional Port A | Authori | tv | | | PROJECT NAME _ PhilaPort Distribution Wa | rehous | 9 |
| | | | | PAX17013.0 | | | | | | | <u> </u> |
| | | | - | | | | | | GROUND ELEVATION <u>16 +/- feet NAV</u> D88 | | <u> </u> |
| | | | | | | | | | | | |
| DRILLING CONTRACTOR CGC Geoservices, LLC WATER ENCOUNTERED: DRILLING METHOD Hollow Stem Auger \[\frac{10.00}{2} DURING DRILLING 10.00 / Elev 6.00 \] | | | | | | | | | | | |
| DRILLE | | | | | | | | | | | |
| | | | | | CHE | AT END OF DRILLING AFTER DRILLING | | | | | |
| | | | | | | | | | | | |
| o DEPTH (ft) | SAMPLE TYPE | NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | Dept | | | ev. | REMARKS |
| | | | | | | Р | 0.9 | | | 5.1 | |
| | X | S-1 | 10 | 15-22 | | | 2.0 | -\AND F/M SAN | F gravel size ROCK FRAGMENTS | 4.0 | |
| | - X = | S-2 | 20 | 14-27-22- | | | | | /M SAND, trace Silt | | |
| | $\left\{\right\}$ | | | | | | 4.0 | | /M SAND, little Fine Gravel, trace | 2.0 | |
| 5 | 1X : | S-3 | 12 | 6-6-7-7 | | | 6.0 | Silt Black to tan E/ | M SAND AND Fine GRAVEL | 0.0 | Petroleum odor |
| | M, | S-4 | 12 | 12-13-8-5 | | | 0.0 | <u> </u> | ND, little Fine Gravel, Organics | 0.0 | |
| | $\left\{\right\}$ | S-4 | 7 | 1-1-1-1 | | | 8.0 | Black M/C/F S | AND AND F/C gravel size ROCK | 8.0 | |
| <u> 10 </u> | | 00 | | | | F | | FRAGMENTS | , little Clay, little Organics, Debris | | Wet on spoon |
| | - | | | | | | 13.0 | | | F 3.0 | Petroleum odor 4' to 15' |
| _ <u>15</u> | | S-6 | 16 | 1-2-1-1 | | | | Dark gray F/M Brick Fragmer | | | |
| 20 | | S-7 | 24 | WOH/24" | | | 18.0 | Gray Silty CLA | Y, trace Fine Sand, trace Organics | <u>2.0</u> | Wet, Saturated |
| | | | | | | | 23.0 | | | 7.0 | |
| 25 | | S-8 | 24 | 1-1-2-2 | | 1 | | Gray Silty CLA | Y, trace Fine Sand, little Organics | | |
| | 1 | | | | | | 28.0 | | | 2.0 | |
| | | S-9 | 24 | 4-4-4-5 | | | 20.0 | Gray Silty CLA Micaceous | Y, little to some Fine Gravel, | | |
| | | | | | | | | | | | |
| 35 | - X s | 6-10 | 12 | 6-7-7-6 | | 3 | 33.0 | Tan to gray M/ | F SAND, trace Silt | 7.0 | |
| <u>NOTE</u> | <u> </u> | 1 | 1 | 1 | <u>p. 13 (5)</u> | 1 | 1 | | | I | |

(Continued Next Page)

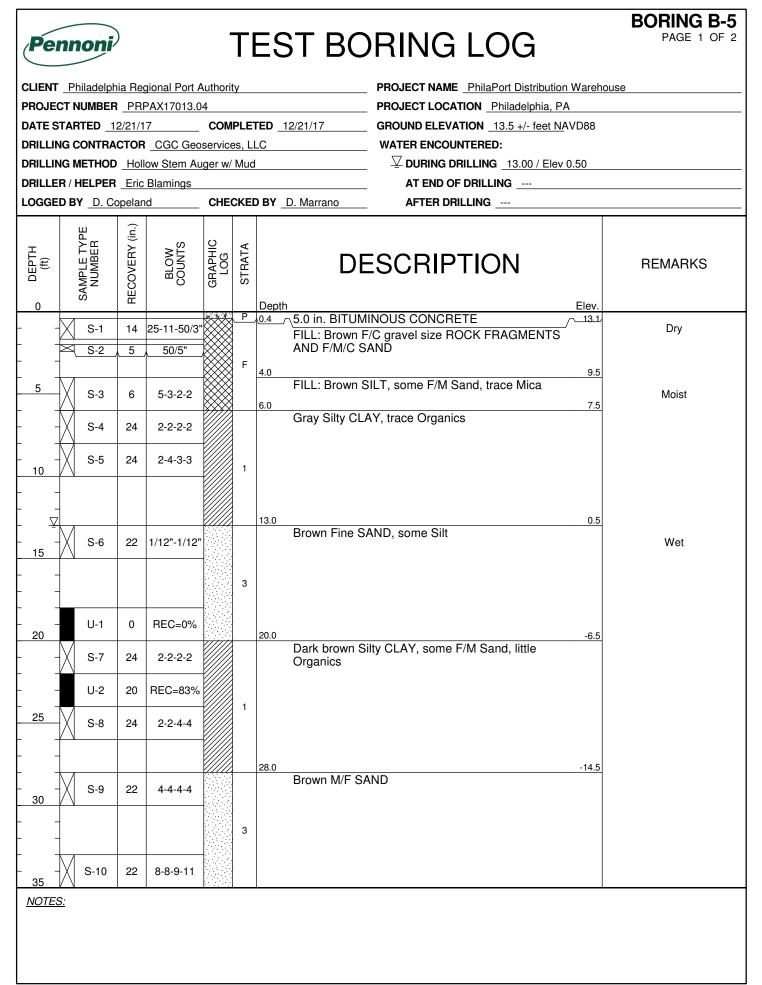


| Pe | Pennoni TEST BORING LOG | | | | | | | | | | |
|-------------------|-------------------------|----------------|--------------|----------------|-------------|------|-------------------|--|---------|--|--|
| | Philad | elnhia R | egional Port | Authori | itv | | | PROJECT NAME _ PhilaPort Distribution Wareho | | | |
| | | | RPAX17013.0 | | | | | | | | |
| | | | | | | | | GROUND ELEVATION <u>16 +/- feet NAV</u> D88 | | | |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| | | | ic Blemings | ugei | | | | AT END OF DRILLING | | | |
| | | | - | CHE | CKE | D RY | D. Marrano | | | | |
| 20002 | | | | | | | | | | | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW | GRAPHIC LOG | STRATA | Dep | | ESCRIPTION | REMARKS | | |
| Ŭ | | | | | Р | 0.4 | 5.0 in. BITUM | INOUS CONCRETE | | | |
| [] | S- | | | | 8 | 2.0 | FILL: Gray C/F | gravel size ROCK FRAGMENTS | | | |
| | S- | 2 5 | 50/5" | -1000 | | | AND M/F/C S/ | an F/M SAND, some F/C Gravel | | | |
| | | | | -888 | <pre></pre> | 4.0 | , | gray F/M SAND, some F/C Gravel, | | | |
| 5 | - X s- | 3 8 | 15-13-7-6 | | 8 | | trace Silt, trace | e Brick and Cinder Fragments | | | |
| - · | s- | 4 16 | 8-5-3-3 | | F | 6.0 | FILL: Black SI | LT, some F/M Sand | | | |
| | | | | -888 | <pre></pre> | 8.0 | FILL: Black C/ | F GRAVEL AND F/M/C SAND, little | | | |
| 10 | -X s- | 5 6 | 3-3-2-2 | | | | Silt | | Wet | | |
| - · | _ | | | | | 13.0 | | 3.0 | | | |
| - · · | | 6 14 | 2-1-1-1 | | | 10.0 | | ID F/M SAND, trace Organics | | | |
| | | | | | 2 | | | | | | |
| | | | | | | 18.0 | | -2.0 | | | |
| 20 | - X s- | 7 22 | WOH/24" | | | | Gray Silty CLA | AY, trace Fine Sand | Wet | | |
| | _ | | | | | | | | | | |
| | 1 | | | -{//// | 1 | 23.0 | Grav Silty CLA | -7.0 AY, trace Fine Sand, trace Organics | | | |
| 25 | - X s- | 8 24 | 1-1-1-1 | | | | | | | | |
| |] | | | | | 28.0 | | -12.0 | | | |
| - 30 | - S- | 9 12 | 5-5-5-9 | | | | Brown SILT A | ND ORGANICS, trace Fine Sand | | | |
| | - | | | | 2 | | | | | | |
| _ · | -X s-1 | 0 9 | 5-6-7-6 | | 3 | 33.0 | | /F/C SAND, trace Silt | | | |
| 35 <u>NOTE</u> | <u>v v</u> | | | <u>hodror</u> | 4 | 1 | | | | | |
| | <u>o.</u> | | | | | | | | | | |
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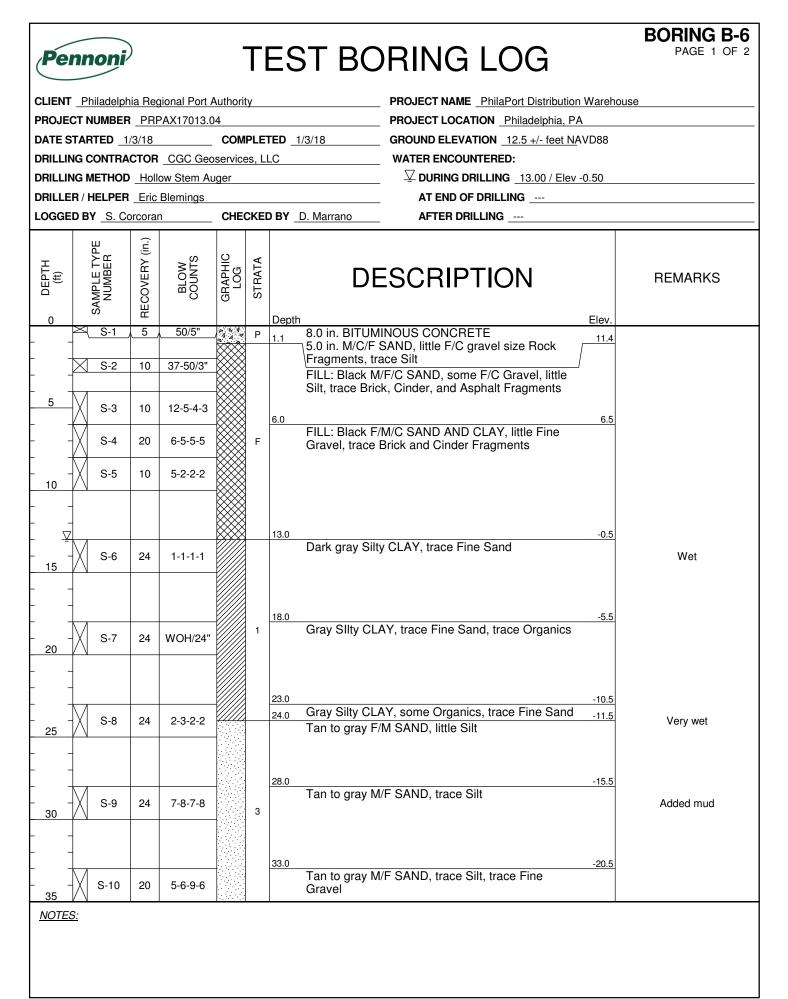
| Per | nnoni |) | | • | T | EST BORING LOG | BORING B-3 PAGE 2 OF 2 | | | | |
|-------------------|-----------------------|----------------|--------------------|----------------|------------|---|---------------------------|--|--|--|--|
| | Philadelph | | | | t y | PROJECT NAME _ PhilaPort Distribution Warehouse PROJECT LOCATION _ Philadelphia, PA | | | | | |
| DEPTH (ft) | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | DESCRIPTION | REMARKS | | | | |
| <u>35</u> | | | | | | Depth Elev. Gray to tan M/F/C SAND, trace Silt (continued) 38.0 38.0 -22.0 Gray to tan M/F/C SAND, little to some C/F | | | | | |
| | S-11 | 10 | 5-5-7-14 | | 3 | Gravel, trace Silt | | | | | |
| - 45 | S-12 | 12 | 6-7-13-36 | | | 43.0 -27.0 Gray to tan F/M/C SAND, trace Fine Gravel, trace 44.5 Silt -28.5 Gray to tan C/F GRAVEL, some C/M/F Sand, trace Silt | | | | | |
| - 50 | S-13 | 24 | 28-33-42- 50/3" | | | 49.0 -33.0 Gray to tan F/M/C SAND, trace Fine Gravel, trace Silt | | | | | |
| - 55 | S-14 | 16 | 50-40-9-13 | | 4 | 53.0 -37.0 Gray to tan C/F GRAVEL, some C/M/F Sand, trace Silt | | | | | |
| | S-15 | 18 | 8-20-7-34 | | | 58.0 -42.0 Gray to tan C/M/F SAND AND C/F GRAVEL, trace | | | | | |
| 60 | / \ | | | ÞÝC | | Boring terminated at 60.0 feet. | | | | | |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| | | | | | | | | | | | |
| NOTES | <u>5:</u> | | | | | | | | | | |
| | | | | | | | | | | | |

| Pe | nnon | | | | Т | ES | ST BC | RING LOG | | BORING B-4 PAGE 1 OF 2 |
|--------------------|-------------------------|----------------|----------------|----------------|-------------|----------|--------------------------------|--|-----------------|---------------------------|
| CLIENT | Philade | phia Re | gional Port / | Author | ity | | | PROJECT NAME _ PhilaPort Distributio | n Warehou | se |
| PROJE | CT NUMB | ER _ PR | PAX17013.0 |)4 | | | | PROJECT LOCATION _ Philadelphia, P | A | |
| DATE S | TARTED | 12/22/ | 17 | CON | IPLE | TED _ | 12/22/17 | GROUND ELEVATION 13.5 +/- feet N | AVD88 | |
| | | | | | | | | | | |
| | | | | uger w | / Muc | 1 | | · · · · · · · · · · · · · · · · · · · | | |
| | | | Blemings | | | | | AT END OF DRILLING | | |
| LOGGE | D BY _D. | Copela | nd | CHE | CKE | D BY _ | D. Marrano | AFTER DRILLING | I | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | | Depth | h | ESCRIPTION | Elev. | REMARKS |
| | | 10 | 00.00.50 | | P | 0.5 | | INOUS CONCRETE | 13.0 | Dry |
| | S-1 | 12 | 29-26-50 | -888 | 3 | | FILL: Brown C AND M/F SAN | C/F gravel size ROCK FRAGMENTS | | 5.7 |
| | - 3-2 | 4 | | -1000 | | | | | | |
| | S-3 | 16 | 5-8-9-6 | | F | 4.0 | FILL: Black S Incinerated M | ILT, some M/F Sand, trace aterial, trace Organics | 9.5 | |
| | S-4 | 16 | 6-6-6-7 | | | 8.0 | | | 5.5 | Moist |
| | S-5 | 18 | 7-9-8-7 | - | | | Gray Fine SA | ND, trace Silt | | |
| | | | | | 3 | 13.0 | Grov Silty CL | AY, trace Organics, trace Fine Sand | 0.5 | |
| 15 | S-6 | 24 | WOH/24" | | | | | Ar, frace Organics, frace rifle Sand | | |
| 20 | S-7 | 24 | 1/12"-1/12' | , | 1 | 18.0 | Gray Silty CL | AY, some Organics | -4.5 | |
| | | | | | | 23.0 | | | -9.5 | |
| 25 | S-8 | 24 | 2-2-2-2 | | | | Dark brown S | ILT AND ORGANICS | | |
| 30 | S-9 | 24 | 5-7-9-12 | | 2 | | | | | |
| | | | | | | 33.0 | | | -19.5 | |
| | S-10 | 22 | 4-7-7-9 | | 3 | | Brown M/F SA | AND, trace Silt | | |
| 35 <u>NOTES</u> | <u>V N</u> <u>S:</u> | | | | • | <u> </u> | | | | |

| Pennoni | | | | | | TEST BORING LOG | | | |
|---|-----------------------|----------------|-----------------|----------------|--------|---|---------------|--|--|
| CLIENT <u>Philadelphia Regional Port Authorit</u> PROJECT NUMBER PRPAX17013.04 | | | | | | PROJECT NAME _ PhilaPort Distribution Warehous | se | | |
| HLU DEPTH 32 | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | DESCRIPTION Elev. | REMARKS | | |
| - 40 | S-11 | 22 | 4-6-7-5 | | 3 | Brown M/F SAND, trace Silt <i>(continued)</i> 38.0 -24.5 Brown M/C/F SAND, trace Silt | | | |
| - 45 | S-12 | 10 | 43-45-45- 45 | | | 43.0 -29.5 Brown M/F/C SAND, some C/F Gravel, trace Silt | Auger Chatter | | |
| <u>50</u> | S-13 | 22 | 19-20-24- 19 | | | | | | |
| - <u>55</u> | S-14 | 2 | 15-15-15- 16 | | | | | | |
| 60 | S-15 | 20 | 6-10-11-12 | | | 60.0 -46.5 | | | |
| NOTES | ç. | | | | | Boring terminated at 60.0 feet. | | | |
| | <u></u> | | | | | | | | |



| Pe | nnonj |) | | • | T | EST BORING LOG | BORING B-5 PAGE 2 OF 2 | | |
|---|-----------------------|----------------|-----------------|----------------|--------|---|---------------------------|--|--|
| CLIENT _Philadelphia Regional Port Authority PROJECT NUMBER _PRPAX17013.04 | | | | | | | | | |
| 25 DEPTH 29 | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | DESCRIPTION | REMARKS | | |
| 40 | S-11 | 22 | 10-11-14- 16 | | | Brown M/F SAND <i>(continued)</i> <u>38.0</u> Brown C/F GRAVEL AND M/F SAND | | | |
| - 45 | S-12 | 22 | 5-6-6-5 | | | 43.0 -29.5 Brown M/F SAND, trace Fine Gravel | | | |
| - 50 | S-13 | 16 | 7-8-10-11 | | 3 | 48.0 -34.5 Brown F/C GRAVEL AND M/C/F SAND 53.0 -39.5 | | | |
| <u>55</u> | S-14 | 18 | 12-11-10- 12 | | | Brown C/M/F SAND | | | |
| 60 | S-15 | 18 | 4-6-8-8 | | | 60.0 -46.5 Boring terminated at 60.0 feet. | | | |
| | | | | | | | | | |
| <u>NOTES</u> | <u></u> | | | | | | | | |





TEST BORING LOG

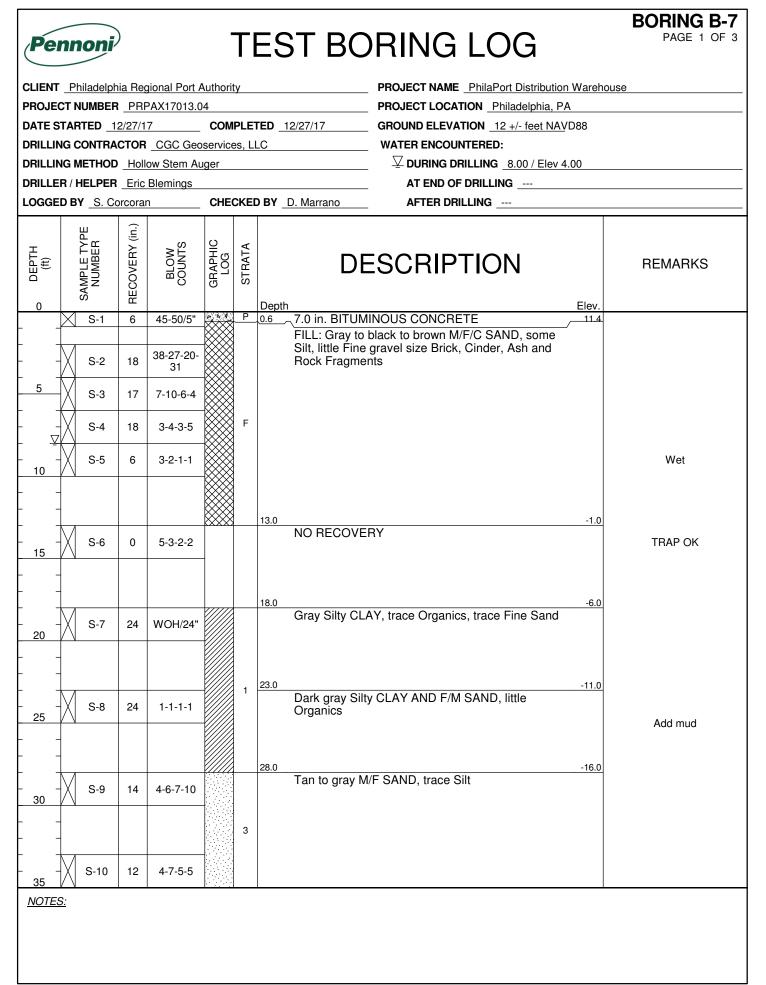
CLIENT Philadelphia Regional Port Authority

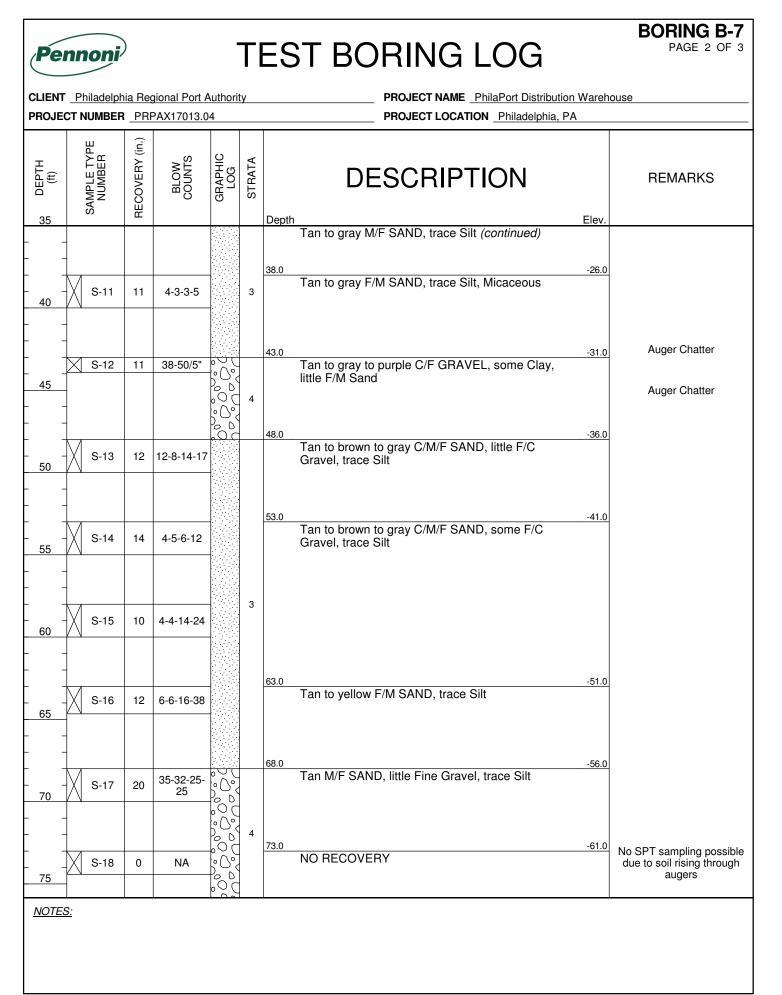
PROJECT NAME PhilaPort Distribution Warehouse

PROJECT NUMBER PRPAX17013.04

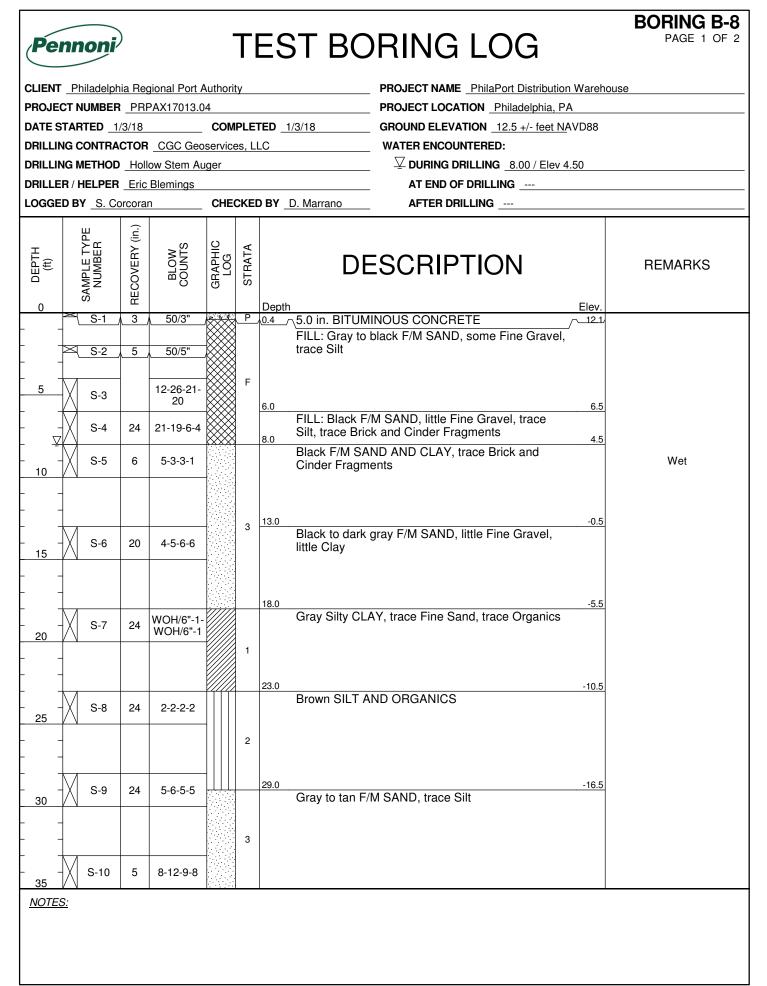
PROJECT LOCATION Philadelphia, PA

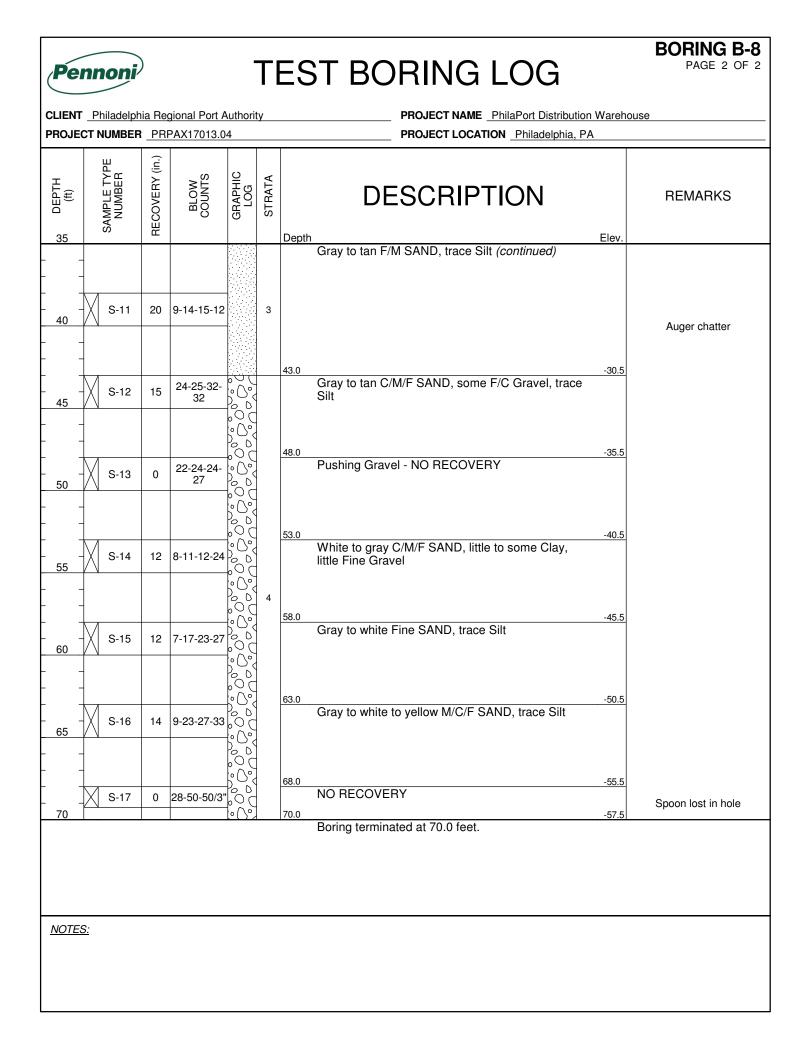
| G DEPTH | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | Depth | DESCRIPTION | Elev. | REMARKS |
|---------|-----------------------|----------------|-----------------|----------------|--------|--------------|---|------------------------|---------|
| | - | | | | 3 | | Tan to gray M/F SAND, trace Silt, trace Fine Gravel (continued) | | |
| | - | | | | 3 | 38.0 | | -25.5 | |
| | S-11 | 12 | 13-18-10-7 | 000 | | | Tan to gray M/F/C SAND, little Fine Gravel, trace Silt | | |
| 40 | / N | | | | | | | | |
| | - | | | [00] | | | | | |
| | | | 20 12 16 | | | 43.0 | Gray to tan C/M/F SAND, little Fine Gravel, trace | -30.5 | |
| 45 | S-12 | 7 | 20-13-16- 14 | | | | Silt | | |
| | - | | | 000 | | | | | |
| | - | | | | | 48.0 | | -35.5 | |
| | S-13 | 10 | 4-10-10-11 | | | 40.0 | Gray to tan C/M/F SAND, some F/C Gravel, trace | 00.0 | |
| 50 | | | | | | | Silt | | |
| | - | | | 000 | | | | | |
| | | _ | 50/01 | | | 53.0 | | -40.5 | |
| | ≊{ <u>S-14</u> | _2_ | 50/3" | | 4 | | Gray C/F GRAVEL, little C/M/F Sand | | |
| 55 | | | | 0° | | | | | |
| | | | | 000 | | | | | |
| | | | 24-38-42- | 000 | | 58.0 | Yellow to white to tan F/M SAND, trace Fine | -45.5 | |
| 60 | S-15 | 12 | 44 | 000 | | | Gravel, trace Silt, mottled | | |
| | - | | | | | | | | |
| | - | | | 0° | | 63.0 | | -50.5 | |
| | S-16 | 24 | 12-16-19- | | | | Yellow to white to tan F/M SAND, little Clay, trace Fine Gravel, trace Silt, mottled | | |
| 65 | <u> </u> | | 21 | 000 | | | The Gravel, trace Silt, mottled | | |
| | | | | 000 | | | | | |
| | | | | | | 68.0 | White to gray Fine SAND, little Silt | -55.5 | |
| 70 | S-17 | 24 | 17-12-15- 13 | | 5 | 69.0 70.0 | White to gray CLAY, some to little Fine Sand | - <u>56.5</u> -57.5 | |
| 10 | | | 1 | 0.0.0.0 | | 70.0 | Boring terminated at 70.0 feet. | 07.0 | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| NOTE | S: | | | | | | | | |
| <u></u> | <u></u> | | | | | | | | |
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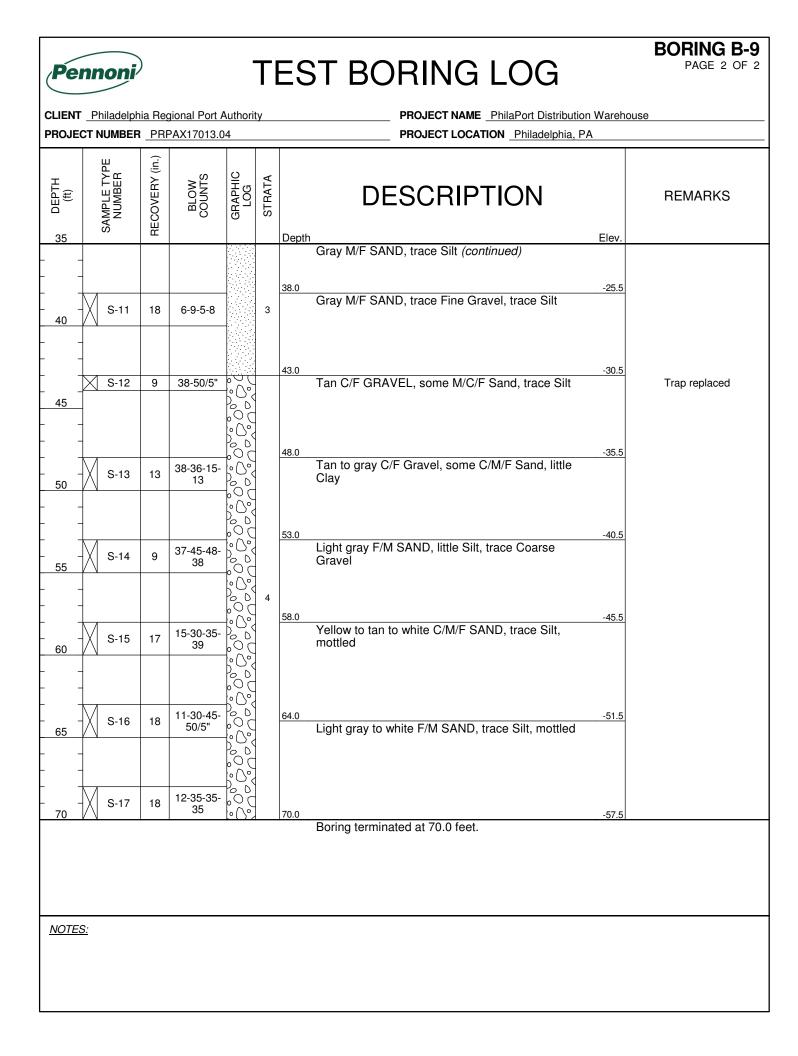


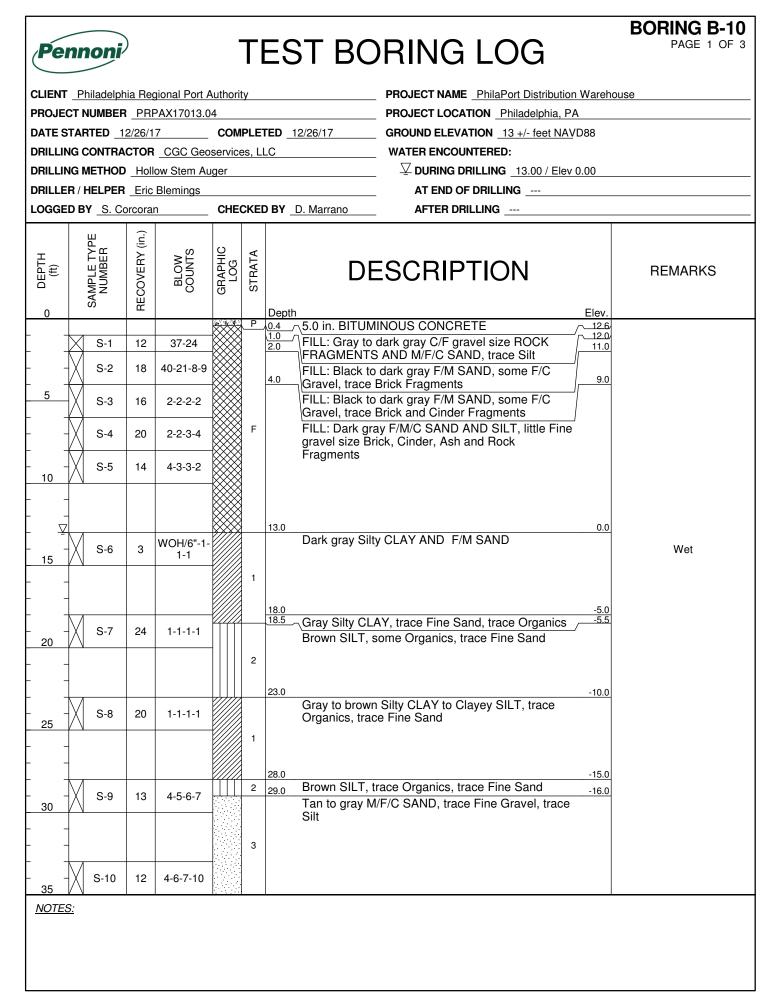
| Per | nnoni |) | | - | ΤI | EST BORING LOG | BORING B-7 PAGE 3 OF 3 |
|----------------|-----------------------|----------------|----------------|----------------|--------|---|--|
| | Philadelph | | | | y | PROJECT NAME PhilaPort Distribution Wareh | ouse |
| DEPTH (ft) | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | DESCRIPTION | REMARKS |
| 80 | S-19 | 0 | NA | | 4 | NO RECOVERY (continued) -66.0 78.0 -66.0 NO RECOVERY -68.0 80.0 -68.0 Boring terminated at 80.0 feet. -68.0 | No SPT sampling possible due to soil rising through augers |
| | | | | | | | |
| | | | | | | | |
| | | | | | | | |
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| | | | | | | | |
| <u>NOTES</u> | <u>5:</u> | | | | | | |

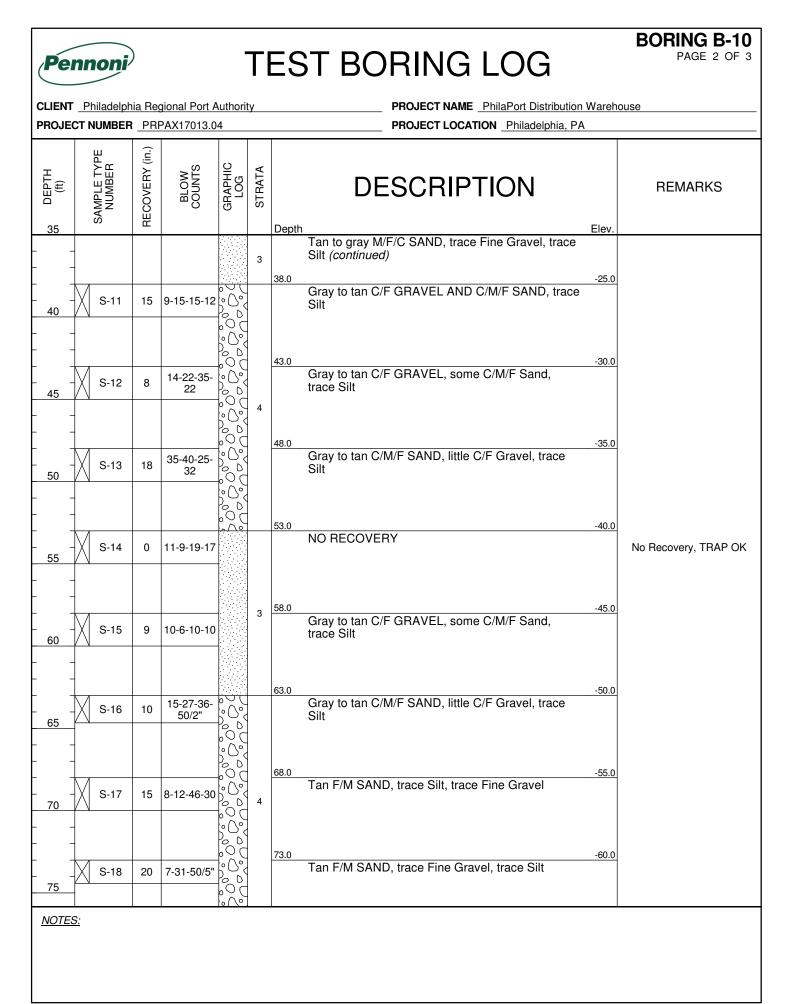




| Pe | Pennoni TEST BORING LOG | | | | | | | | | | | | | |
|-------------------|---|-----------------------|----------------|----------------|----------------|--------|------------|---|-------------------|--------------|--|--|--|--|
| | CLIENT _Philadelphia Regional Port Authority PROJECT NAME _PhilaPort Distribution Warehou | | | | | | | | | | | | | |
| | | | | PAX17013.0 | | | | PROJECT LOCATION Philadelphia, PA | | | | | | |
| | | | | | | | | 12/29/17 GROUND ELEVATION 12.5 +/- feet NAVD | 88 | | | | | |
| | | | | | | | | WATER ENCOUNTERED: | 00 | | | | | |
| | | | | | | | | $ \qquad \qquad$ | | | | | | |
| | | | | Blemings | igei | | | AT END OF DRILLING | | | | | | |
| | | | | - | | | | D. Marrano AFTER DRILLING | | | | | | |
| Loadi | | | | | | | | | | | | | | |
| o DEPTH (ft) | | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | Dept | | lev. | REMARKS | | | | |
| _ | | | | | | Р | 0.8 | 6.0 in. BITUMINOUS CONCRETE | 11.7 | | | | | |
| | M | S-1 | 10 | 22-18 | | | 2.0 | 4.0 in. Gray C/F gravel size ROCK FRAGMENTS | 10.5 | | | | | |
| _ · | \mathbb{N} | S-2 | 14 | 24-14-7-8 | | | 4.0 | Gray F/M/C SAND, some Fine gravel size Rock | 8.5 | | | | | |
| 5 | $\overline{\mathcal{N}}$ | S-3 | 18 | 16-10-7-6 | | | 5.0 | Black to dark gray F/M SAND, little Fine gravel | 7.5 | | | | | |
| | \mathbb{N} | S-4 | 20 | 9-6-5-7 | | F | 7.0 8.0 | Fragments Black to dark gray F/M SAND, little Fine gravel | <u>5.5</u> 4.5 | Wet on spoon | | | | |
| - 10 | \mathbb{N} | S-5 | 24 | 7-8-7-4 | | | | size Rock Fragments, trace Brick, Asphalt, Cinder, and Concrete Fragments | | | | | | |
| | | | | | | | | Black F/M SAND, little Silt, trace Glass Black SILT, some F/M Sand, trace Organics, trace Brick Fragmente | | | | | | |
| _ · | | | | | | | 13.0 | Brick Fragments Black C/M/F SAND AND F/C GRAVEL, Debris, | -0.5 | | | | | |
| 15 | | S-6 | 24 | 1-2-1-1 | | | | Organics, Brick, Concrete, little Clay | | Very soft | | | | |
| - · | | | | | | 1 | | | | | | | | |
| 20 | М | S-7 | 24 | WOH/24" | | | | | | Very soft | | | | |
| - · | | | | | | | | | | | | | | |
| | | 0.0 | | | | 2 | 23.0 | Brown to gray SILT, Organics, trace F/M Sand | 10.5 | | | | | |
| 25 | \mathbb{N} | S-8 | 24 | 2-4-4-2 | | _ | 24.5 | | 12.0 | Added mud | | | | |
| | | | | | | | 28.0 | - | 15.5 | | | | | |
| - - 30 | | S-9 | 12 | 5-7-9-7 | | 3 | | Tan to gray M/F SAND, little Silt | | | | | | |
| | | | | | | 5 | 33.0 | | 20.5 | | | | | |
| | | S-10 | 10 | 6-7-7-7 | | | 00.0 | Gray M/F SAND, trace Silt | <u>20.5</u> | | | | | |
| 35 <u>NOTE</u> | <u>v</u> V S· | | I | 1 | <u> </u> | I | 1 | | | | | | | |
| <u></u> | <u>.</u> | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |









TEST BORING LOG

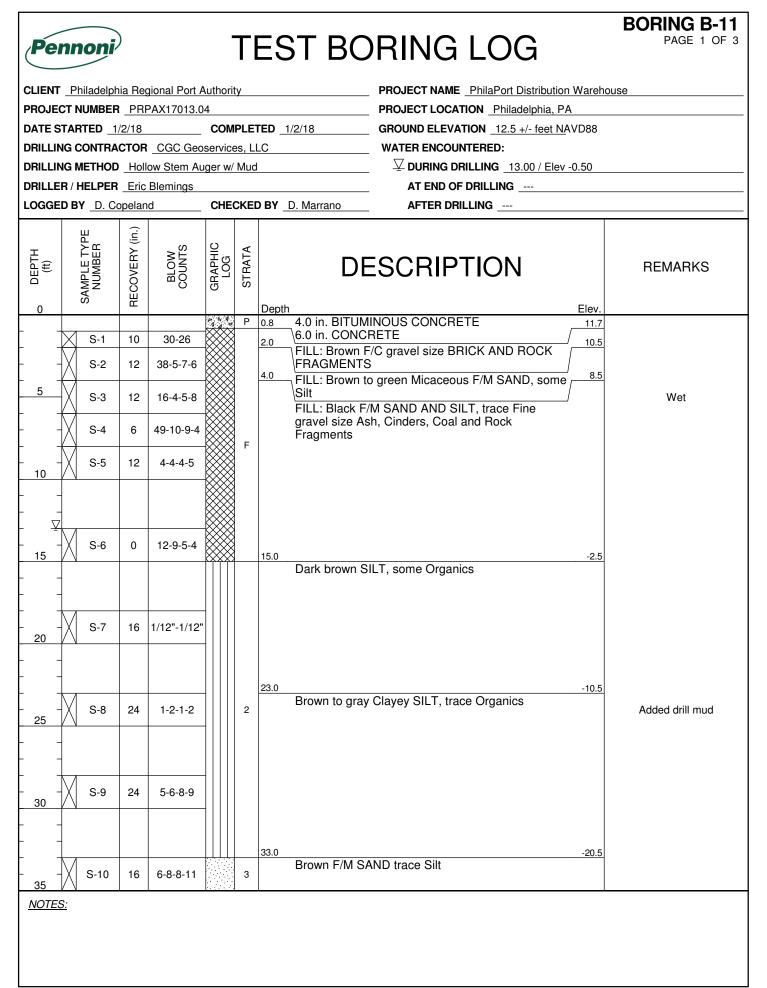
CLIENT Philadelphia Regional Port Authority

PROJECT NAME PhilaPort Distribution Warehouse

PROJECT NUMBER PRPAX17013.04

PROJECT LOCATION Philadelphia, PA

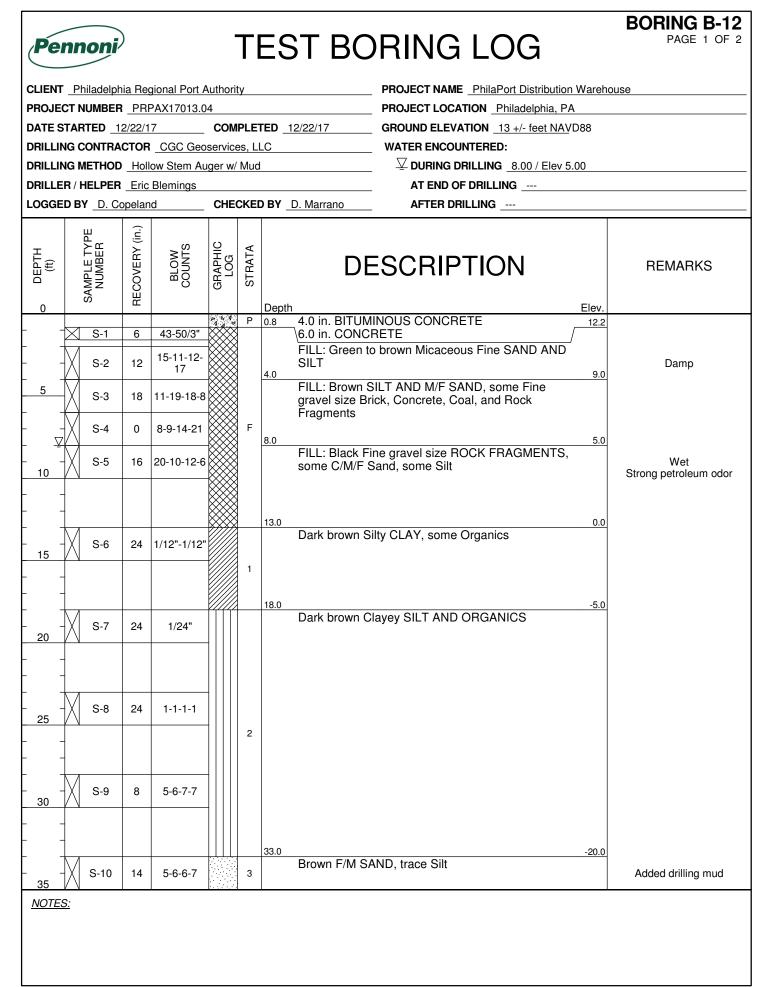
| DEPTH (ft) | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | DESCRIPTION | | REMARKS |
|---------------|-----------------------|----------------|----------------|----------------|--------|---|----------------|---------|
| - | S-19 | 18 | 5-6-7-7 | | 4 | Depth Tan F/M SAND, trace Fine Gravel, trace Silt (continued) Red to white to purple Silty CLAY, trace Fine Sand | Elev. -65.0 | |
| 80 | | 10 | 5077 | | | 80.0 Boring terminated at 80.0 feet. | -67.0 | |
| | | | | | | | | |
| | | | | | | | | |
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| IOTES | <u>5:</u> | | | | | | | |
| | | | | | | | | |

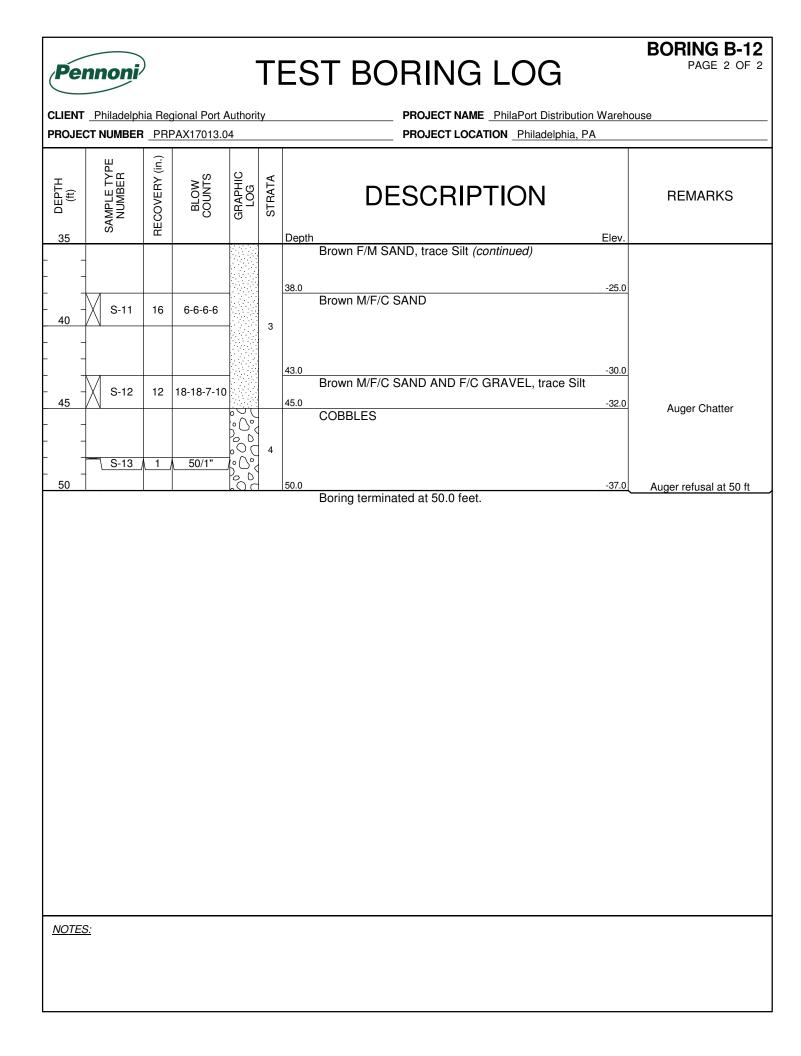


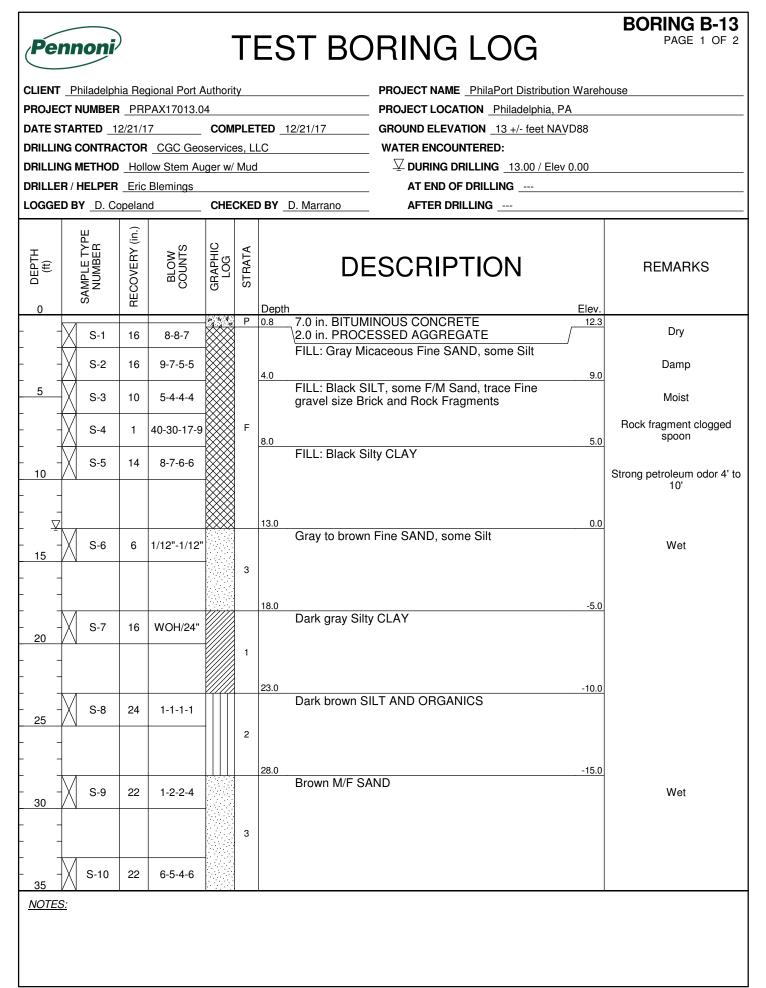
⁽Continued Next Page)

| Pe | nnoni |) | | • | T | EST BORING LOG | BORING B-11 PAGE 2 OF 3 |
|--------------------------|-----------------------|----------------|------------------------------------|----------------|--------|--|----------------------------|
| | Philadelph | | | | ty | PROJECT NAME PhilaPort Distribution Wa | rehouse |
| PROJE | | PRF | PAX17013.0 | 4 | | PROJECT LOCATION Philadelphia, PA | |
| (tt) (tt) 35 | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | | REMARKS |
| - 40 | S-11 | 16 | 8-9-8-9 | | 3 | Brown F/M SAND trace Silt <i>(continued)</i> | |
| 45 | S-12 | 18 | 42-37-27- 38 | | | 43.0 -3 Brown F/C GRAVEL, some M/C/F Sand, trace Silt | <u>0.5</u> |
| - 50 | S-13 | 18 | 17-12-15- 21 14-28-32- 24 | | 4 | | |
| - 60 | S-15 | 18 | 12-14-14- 18 | | | 63.0 -5 Tan C/M/F SAND, some F/C Gravel, trace Silt | <u>0.5</u> |
| <u>65</u> | S-16 | 0 | 5-6-7-6 | | 3 | | |
| - 70 | S-17 | 20 | 10-13-20- 14 | | 4 | Brown F/C GRAVEL, some M/C/F Sand, trace Silt | <u>5.5</u> |
| _ 75 | S-18 | 24 | 8-8-10-17 | | 5 | 73.0 -6 Red to gray CLAY | 0.5 |
| <u>NOTES</u> | <u>S:</u> | | | | | | |

| Pennoni |) | | - | TE | EST BORING LOG | BORING B-11 PAGE 3 OF 3 |
|-----------------------|----------------|----------------|----------------|--------|---|----------------------------|
| IENT Philadelph | | | | ty | PROJECT NAME PhilaPort Distribution Wareh | ouse |
| | | AX17013.0 | 94 | | PROJECT LOCATION _ Philadelphia, PA | |
| SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | DESCRIPTION | REMARKS |
| - | | | | 5 | Red to gray CLAY (continued) | |
| 80 - S-19 | 24 | 6-6-9-14 | | | 80.0 -67.5 | |
| | | | | | Boring terminated at 80.0 feet. | |
| | | | | | | |
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| | | | | | | |
| | | | | | | |
| <u>DTES:</u> | | | | | | |

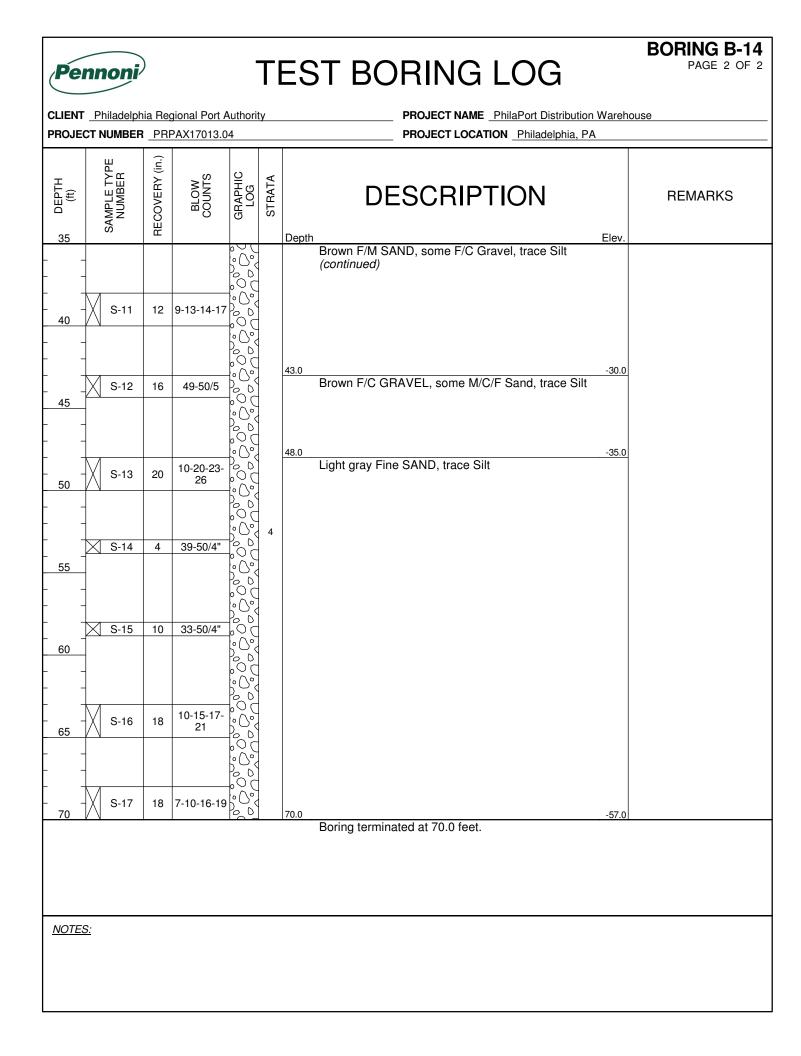




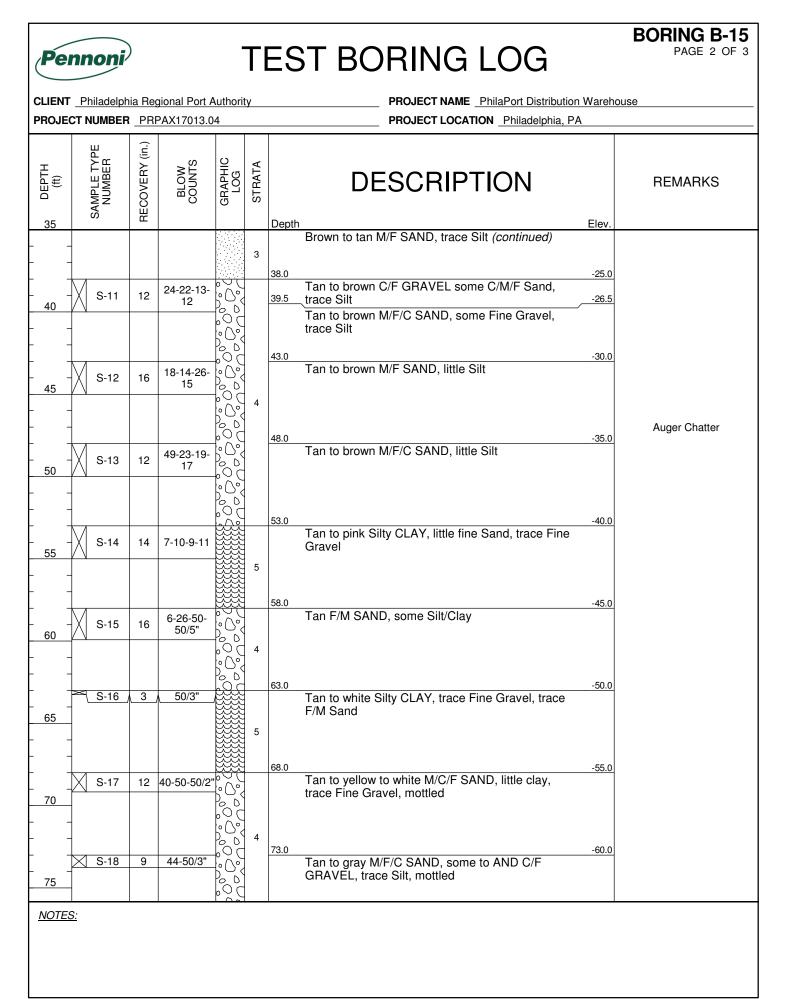


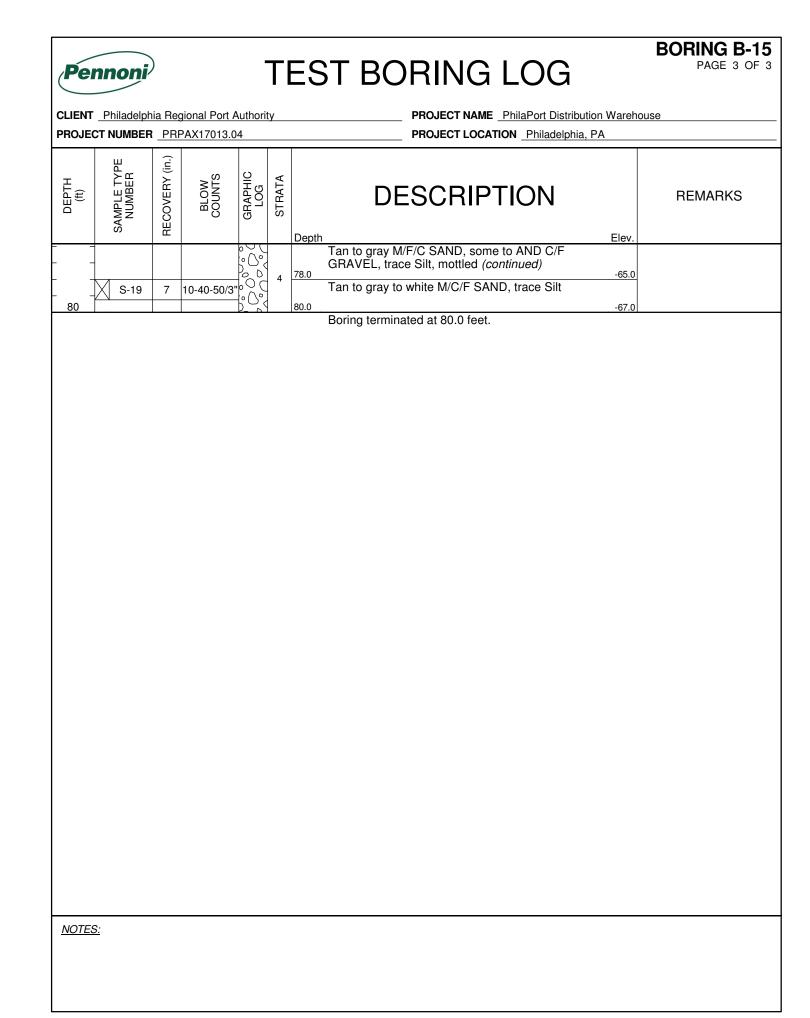
| <form><form></form></form> | Pe | nnoni |) | | • | Т | EST BORING LOG | BORING B-13 PAGE 2 OF 2 |
|--|-------------------|-----------|----|-----------------|---|--------|--|----------------------------|
| Hand Image: State Image: State <thimage: state<="" th=""> Image: State</thimage:> | | | | | | ty | | ouse |
| -40 - S.11 22 3-6-5-5 -40 - S.11 22 3-6-5-5 -45 - S.12 22 10-5-6-6 -45 - S.12 22 10-5-6-6 -50 - S.13 20 8-12-13-25 -55 - S.14 22 6-8-10-14 -55 - S.14 22 6-8-10-14 -60 - S.15 22 10-13-15-17 -60 - S.15 22 10-13-15-17 | DEPTH (ft) | | 1 | | | STRATA | DESCRIPTION | REMARKS |
| 45 S-12 22 10-5-6-6 45 S-12 22 10-5-6-6 50 S-13 20 8-12-13-25 50 S-13 20 8-12-13-25 50 S-14 22 6-8-10-14 55 S-14 22 6-8-10-14 60 S-15 22 10-13-15- 17 60 S-15 22 10-13-15- 17 | | S-11 | 22 | 3-6-5-5 | | | Brown M/F SAND <i>(continued)</i> 38.0 -25.0 | |
| S-13 20 8-12-13-25 50 S-13 20 8-12-13-25 60 S-14 22 6-8-10-14 55 S-14 22 6-8-10-14 55 S-14 22 6-8-10-14 55 S-15 22 10-13-15- 17 60 S-15 22 10-13-15- 17 | - - - 45 | S-12 | 22 | 10-5-6-6 | | | 43.0 -30.0 Brown Fine GRAVEL AND C/M/F SAND | |
| S-14 22 6-8-10-14 55 - - - | - - - 50 | S-13 | 20 | 8-12-13-25 | | 3 | | |
| | - - 55 - | S-14 | 22 | 6-8-10-14 | | | 53.0 -40.0 Brown C/M//F SAND, trace Fine Gravel | |
| | - - 60 | S-15 | 22 | 10-13-15- 17 | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| <u>NOTES:</u> | NOTES | <u>S:</u> | | | | | | |

| Pen | nonj |) | | | T | EST BO | RING LOG | | PAGE 1 OI |
|-----------------|-------------------------|----------------|-----------------|----------------|--------|------------------------|---|-------------|-----------------|
| | Philadolph | nia Po | gional Port / | | | | | ion Warobou | 50 |
| | | | PAX17013.0 | | | | PROJECT NAME <u>PrilaPort Distribut</u> PROJECT LOCATION Philadelphia, | | 56 |
| | | | | | | | GROUND ELEVATION <u>13 +/- feet N</u> | | |
| | | | | | | | | AVD66 | |
| | | | | | | | | av 0.00 | |
| | | | Blemings | | | <u> </u> | | | |
| | | | - | | | DBY _D. Marrano | | | |
| | BT _ <u>D.</u> C | upeiai T | | | | | AFTER DRILLING | | |
| (tt) | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | Depth | SCRIPTION | Elev. | REMARKS |
| | S-1 | 24 | 34-6-5-7 | | Р | 1.0 12.0 in. PROC | ESSED AGGREGATE | 12.0 | |
| 1/ | 5-1 | 24 | 34-0-5-1 | | 8 | 2.0 | icaceous Fine SAND AND SILT | 11.0 | |
| | S-2 | 4 | 5-7-8-7 | | 8 | FILL: Brown M | icaceous Fine SAND | | Damp |
| + | | | | | - | 4.0 | caceous Fine SAND AND SILT | 9.0 | |
| $ \rightarrow $ | (S-3 | 22 | 4-4-4-5 | | F | | LALEUUS FILLE SAIND AIND SILL | | |
| + | S-4 | 4 | 5-5-3-3 | | | Cinder | T, some Fine Sand, trace Ash, | 7.0 | Wet |
| , -> | S-5 | 24 | 2-2-2-2 | | | B.0 Dark brown SII | T, trace Organics | 5.0 | |
| _ | S-6 | 0 | 1/24" | - | 2 | | | | |
| <u> </u> | S-7 | 24 | 1/12"-1/12" | - | | | | | |
| + | / | | | | | 23.0 Gray Silty CLA | V | -10.0 | |
| 5 | S-8 | 24 | 1/12"-1/12" | | 1 | | , | | |
| + | / | | | <i>\////</i> | | 28.0 Brown F/M SAI | ND, trace Silt | -15.0 | |
| , -/ - - | S-9 | 18 | 5-5-8-10 | | 3 | | | | Added drill mud |
| . +> | S-10 | 18 | 10-15-15- 15 | 000 | 4 | 33.0 Brown F/M SA | ND, some F/C Gravel, trace Silt | -20.0 | |
| 5 / | N | 1 | 1 10 | KO D | 1 | | | | |



| Pe | nnc | BORING B-15 PAGE 1 OF 3 | | | | | | | | | |
|-----------------|--------------|----------------------------|----------------|----------------|----------------|--------|-------------------|-----------------------------------|---|--------------|-----------------------------------|
| CLIENT | Phil: | ouse | | | | | | | | | |
| | | | | PAX17013.0 | | | | | PROJECT NAME <u>PhilaPort Distribution</u> PROJECT LOCATION Philadelphia, PA | | |
| | | | | | | PLE | TED _ | 12/27/17 | GROUND ELEVATION _13 +/- feet NAVE | 88 | |
| DRILLI | NG CO | NTRA | CTOR | CGC Geo | service | es, Ll | LC | | WATER ENCOUNTERED: | | |
| DRILLI | NG ME | THOD | Holl | ow Stem Au | iger | | | | $\overline{\mathbf{\nabla}}$ during drilling 13.00 / Elev 0 | .00 | |
| DRILLE | R / HE | | | | | | | | | | |
| LOGGE | DBY | | | | | | | | | | |
| o DEPTH (ft) | SAMPLE TYPE | NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | Dept | h | SCRIPTION | Elev. | REMARKS |
| | \mathbb{N} | S-1 | 18 | 9-8-7-7 | | | <u>0.7</u> 2.0 | FRAGMENTS | y to black F/C gravel size ROCK AND F/M/C SAND, trace Silt | 12.3 11.0 | |
| | \mathbb{A} | S-2 | 24 | 16-11-5-3 | | | 4.0 | Silt, little Fine | black Micaceous F/M SAND, some | 9.0 | |
| 5 | | S-3 | 24 | 3-4-3-4 | | | 6.5 | Organics, Deb Micaceous | ris, some Fine Gravel, little Silt, | 0 F | Dry |
| | | S-4 | 20 | 8-7-13-17 | | F | 8.0 | Micaceous | tan F/M SAND, some to AND SILT, | 6.5 5.0 | Petroleum odor |
| | | S-5 | 18 | 8-14-13-10 | | | | FILL: Black to | M SAND, little Sitl, Organics / tan F/M SAND, some gravel size ts, Cinders, Brick, trace Silt | | Brick and cinder fragments Dry |
| | _ | | | | | | | | | | |
| _ ⊻ | Λ | S-6 | 24 | 3-2-2-2 | | | 13.0 14.0 | FILL: Black to \Sand, trace Or | dark gray Silty CLAY, trace Fine ganics, trace Fine Gravel | 0.0 -1.0 | Observed soil heaving at surface |
| | | S-7 | 24 | 1-2-1-2 | | 1 | | Gray Silty CLA | Y, trace Fine Sand | | |
| _ <u>25</u> | | S-8 | 20 | 1-2-1-2 | | | 23.0 | Gray Silty CLA | Y, trace Fine SAND, trace Organics | -10.0 | Petroleum odor Mud added |
| | | | | | | | 28.0 | Brown to tan M | I/F SAND, trace Silt | -15.0 | |
| - <u>30</u> | | S-9 | 15 | 7-7-8-12 | | 3 | | | | | |
| 35 | 1 | S-10 | 12 | 7-8-9-13 | | | | | | | |
| <u>NOTE</u> | <u>S:</u> | | | | | | | | | | |

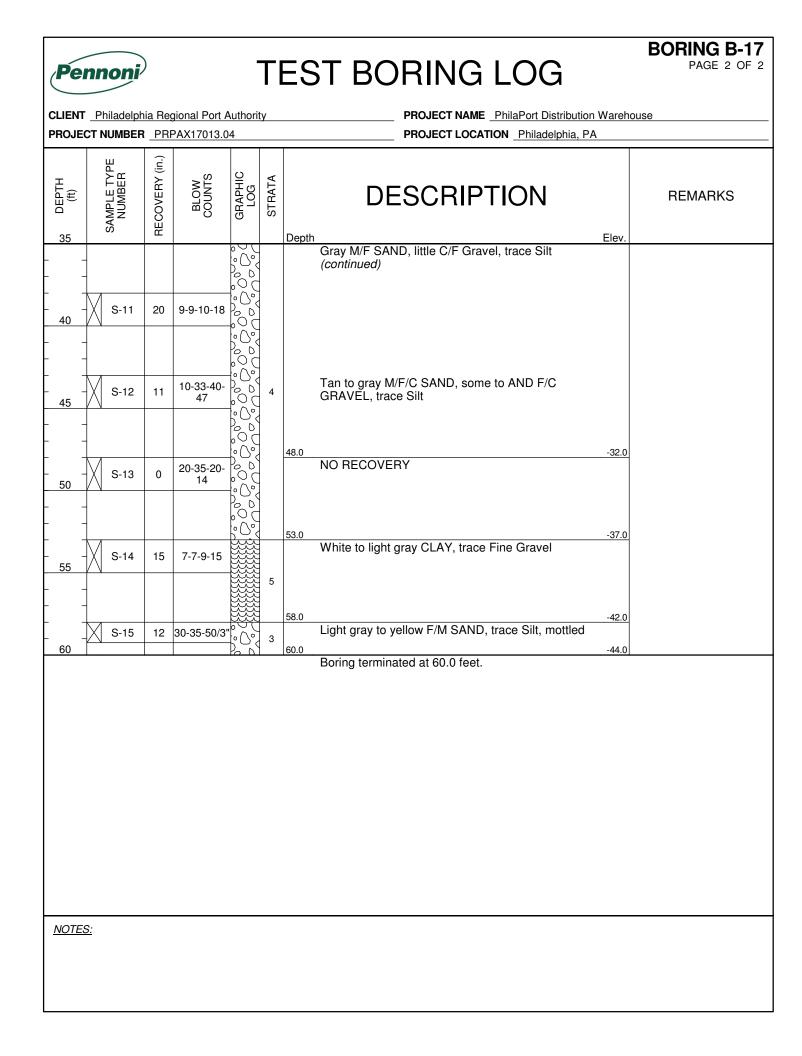




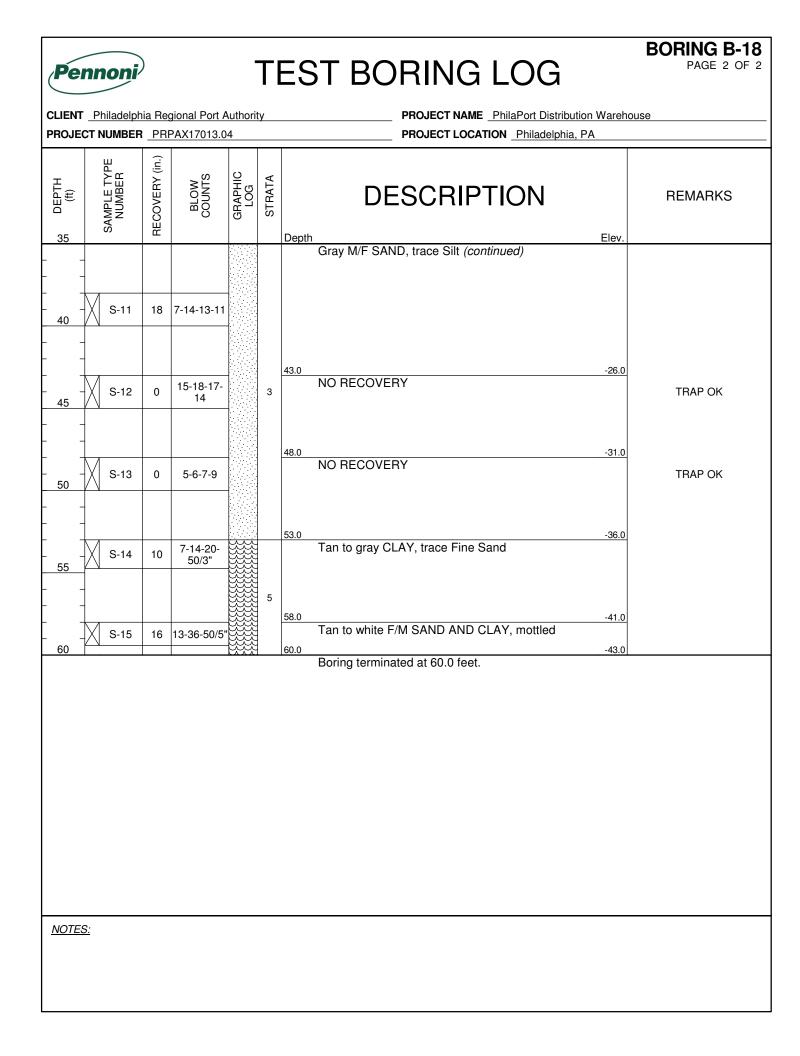
| Pe | Pennoni TEST BORING LOG | | | | | | | | | | | |
|-------------------|-------------------------|----------|----------------|----------------|----------------|---|-------|-------------------------------------|---|-------|---------|--|
| CLIENT | se | | | | | | | | | | | |
| | | | | PAX17013.0 | | | | | PROJECT NAME <u>PhilaPort Distribution</u> PROJECT LOCATION <u>Philadelphia</u> , PA | | | |
| | | | | | | IPLE | TED _ | 1/3/18 | GROUND ELEVATION 16 +/- feet NAV | D88 | | |
| DRILLI | NG CC | NTRA | CTOR | CGC Geo | service | es, L | LC | | WATER ENCOUNTERED: | | | |
| DRILLI | NG ME | THOD | Hol | ow Stem Au | ıger | $\overline{\mathcal{V}}$ DURING DRILLING 13.00 / Elev 3 | 3.00 | | | | | |
| DRILLE | | | | | | | | | | | | |
| LOGGE | DBY | | | | | | | | | | | |
| o DEPTH (ft) | SAMPLE TYPE | NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | Dept | | SCRIPTION | Elev. | REMARKS | |
| | M | S-1 | 24 | 47-20-10-9 | | | | FILL: Tan to gi little F/C Grave | ray to black F/M SAND, some to | | | |
| | $\left\{\right\}$ | | | | | | 2.0 | | ack F/M SAND AND Fine GRAVEL. | 14.0 | | |
| | \mathbb{N} | S-2 | 12 | 12-14-9-7 | | | 4.0 | | ce Brick Fragments | 12.0 | | |
| _ 5 | M | S-3 | 12 | 8-9-10-20 | | | | | M SAND, some Fine Gravel, trace | | | |
| | \square | S-4 | 0 | 50/5" | | | 6.0 | Cinders, Brick | | 10.0 | TRAP OK | |
| | | <u> </u> | | | | > | 8.0 | NO RECOVER | 1 | 8.0 | | |
| <u>10</u> | | S-5 | 7 | 2-4-4-3 | | F | 0.0 | FILL: Red C/F some F/M San | gravel size BRICK FRAGMENTS, d | 0.0 | | |
| | - - , | | | | | | 13.0 | | | 3.0 | | |
| 15 | | S-6 | 5 | 1-1-1-1 | | | | FILL: Black F/0 some F/M/C S | C gravel size ROCK FRAGMENTS, and, trace Silt | | Wet | |
| | | | | | | | 18.0 | NO RECOVER | Υ. | -2.0 | | |
| 20 | | S-7 | 0 | 1-1-1-1 | | | | | | | TRAP OK | |
| | - | | | | | | 23.0 | | | -7.0 | | |
| | М | S-8 | 24 | 2-2-2-2 | | 1 | | Gray Silty CLA | Y, trace Fine Sand, trace Organics | | | |
| | | | | | | | 24.5 | Tan to gray F/I | M SAND, trace Silt | -8.5 | | |
| [- | M | S-9 | 10 | 3-4-6-9 | 1 | | | | | | | |
| | / \ - - | | | | | 3 | 33.0 | | | -17.0 | | |
| [- | \mathbb{M} | S-10 | 10 | 16-11-20- |] | | | Gray F/M SAN | D, little Fine Gravel, little Clay | | | |
| 35 | $\langle \rangle$ | | | 17 | | | | | | | | |
| <u>NOTE</u> | <u>5:</u> | | | | | | | | | | | |
| | | | | | | | | | | | | |
| | | | | | | | | | | | | |

| Per | nnoni |) | | • | TI | EST BORING LOG | BORING B-16 PAGE 2 OF 2 |
|-------------------|-----------------------|----------------|--------------------|----------------|--------|---|----------------------------|
| | Philadelph | | | | ty | PROJECT NAME PhilaPort Distribution Wareh | ouse |
| PROJEC | | | PAX17013.0 | 4 | | PROJECT LOCATION Philadelphia, PA | |
| HTH (ff) 22 | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | DESCRIPTION | REMARKS |
| | | | | | | Gray F/M SAND, little Fine Gravel, little Clay (continued) | |
| 40 | S-11 | 12 | 5-6-7-7 | | 3 | 38.0 -22.0 Gray F/M SAND, trace Silt | |
| | S-12 | | 29-33-36- 28 | | | 43.0 -27.0 Tan to gray to red F/M SAND AND F/C GRAVEL, trace Silt | |
| 50 | S-13 | 0 | 21-11-18- 19 | | 4 | 48.0 -32.0 NO RECOVERY | TRAP OK |
| | S-14 | 24 | 7-7-10-11 | | | 53.0 -37.0 Tan to gray to white CLAY, little F/M Sand | |
| <u>55</u> | S-15 | 12 | 14-22-47- 50/3" | | 5 | 58.0 -42.0 Gray Fine SAND, trace Silt | |
| 60 | A 3-15 | 12 | 50/3" | | 4 | 60.0 -44.0 | |
| | | | | | | Boring terminated at 60.0 feet. | |
| <u>NOTES</u> | <u>5:</u> | | | | | | |

| Pe | G | BORING B-17 PAGE 1 OF 2 | | | | | | |
|--|---|----------------------------|------------------------|----------------|--------|---|-------|-----------------------|
| PROJEC DATE S DRILLIN DRILLIN DRILLE | <u>Philadelph</u> CT NUMBEF TARTED <u>1</u> NG CONTRA NG METHOE R / HELPER D BY <u>S. C</u> | JSE | | | | | | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | | Elev. | REMARKS |
| | S-1 S-2 | 12 24 | 12-10-10-5 10-7-8-5 | | | Dark gray F/M SAND AND F/C GRAVEL, 1 Tan to yellow F/M SAND, little Silt, Micace | | |
| | S-3 S-4 | 16 17 | 4-4-4-5 5-6-12-18 | | | Black to brown F/M SAND, little Silt, trace Gravel, trace Brick, Cinders Black to tan F/M SAND, little Fine Gravel, | | |
| | S-5 | 17 | 15-6-8-20 | | F | Micaceous | | Strong petroleum odor |
| _ <u>15</u> | S-6 | 12 | 10-3-2-2 | | | Gray Silty CLAY, Organics, some F/M San | d | |
| _ ⊻ | S-7 | 10 | 2-1-2-1 | | 1 | 18.0 Gray Silty CLAY, trace Fine Sand | -2.0 | Wet |
| _ <u>25</u> | U-1 | 23 | REC=95% 8-5-6-6 | | | 25.0 Gray M/F SAND, trace Silt | -9.0 | |
| <u>- 30</u> | S-9 | 20 | 5-5-5-7 | | 3 | Gray M/F SAND, trace Silt, trace Fine Grav | vel | |
| 35 | S-10 | 24 | 20-32-13- 11 | | 4 | Gray M/F SAND, little C/F Gravel, trace Sil | lt | |
| <u>NOTES</u> | <u>5:</u> | | | | | | | |

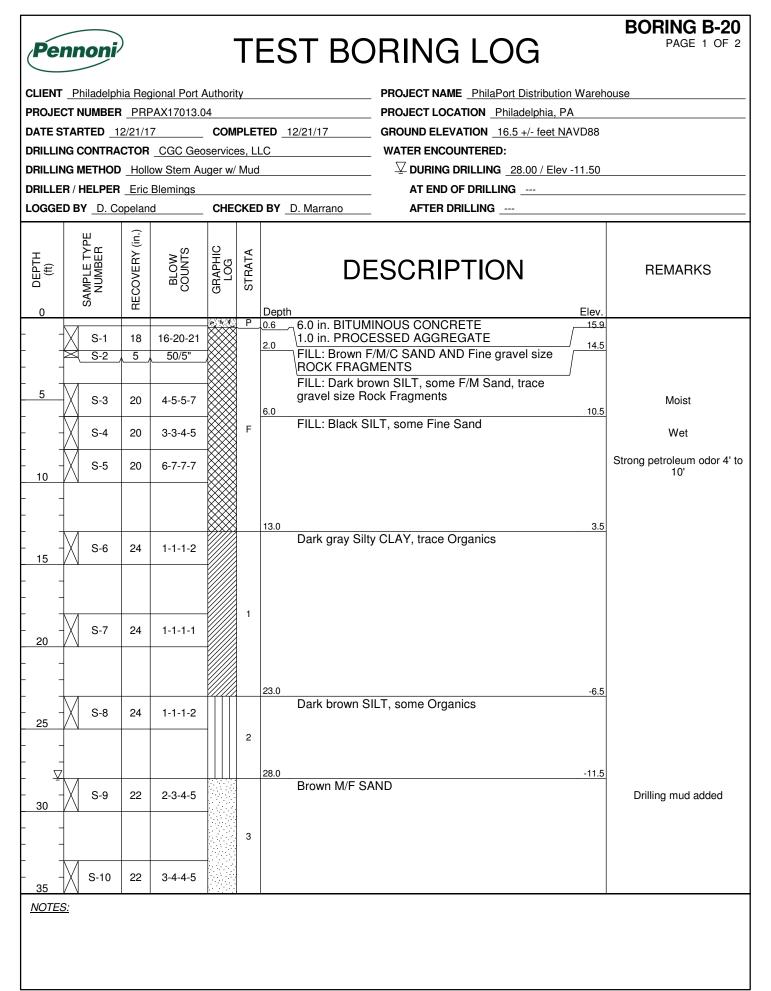


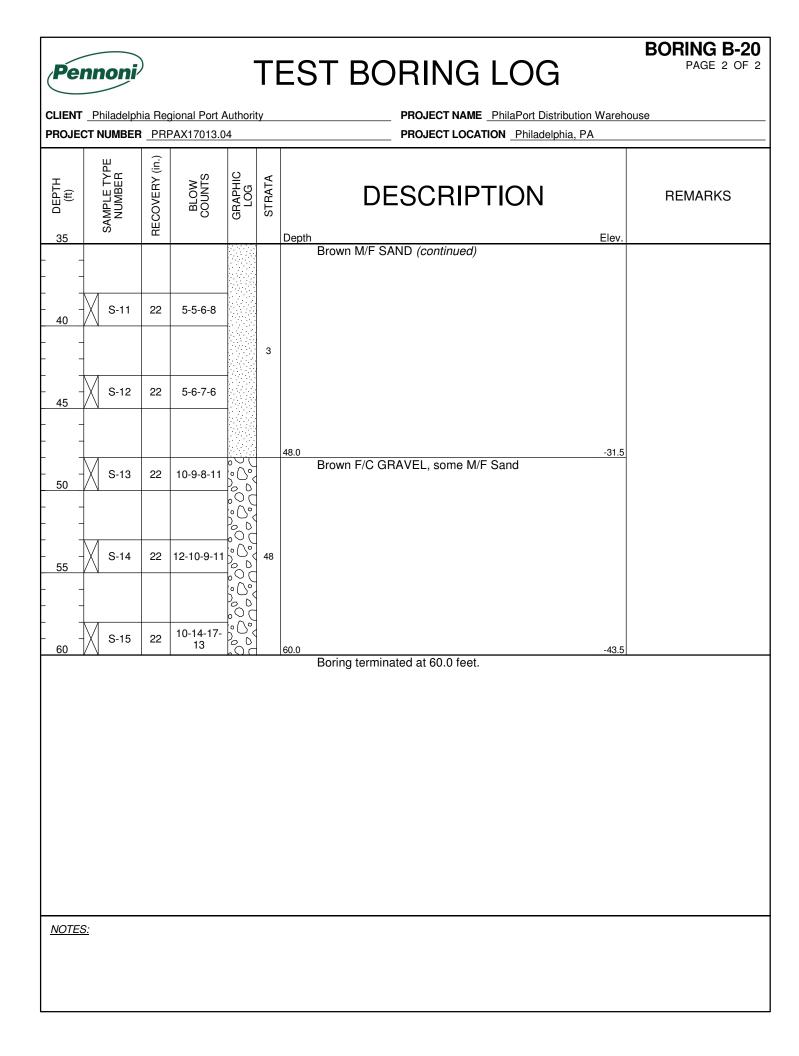
| Pe | nnoni |) | | • | T | ES | Т ВС | RING LOG | | BORING B-18 PAGE 1 OF 2 |
|------------------------------|--------------------------------------|----------------|-----------------------------------|-----------------|--------|-------|-------------------------------|--|--------------|----------------------------|
| | Philadelph | | | | | | | PROJECT NAME _ PhilaPort Distribution PROJECT LOCATION _ Philadelphia, PA | | use |
| DRILLII DRILLII DRILLE | NG CONTRA NG METHOD R / HELPER | CTOR | CGC Geo ow Stem Au Blemings | service Iger | es, L | LC | | | 11.00 | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | Depth | | ESCRIPTION | Elev. | REMARKS |
| | S-1 | 14 | 5-10-13-15 | | | | FILL: Black to little Silt | tan F/M/C SAND, some F/C Gravel, | 15.0 | |
| | S-2 | 16 | 16-4-5-3 | | | | FILL: Brown to Micaceous | o tan F/M SAND, little Silt, | 13.0 | |
| 5 | S-3 | 5 | 4-13-7-7 | | | | FILL: Brown to trace Silt | o tan F/M SAND AND C/F GRAVEL, | 11.0 | |
| | S-4 | 6 | 18-14-7-7 | | F | | FILL: Black to some Silt | brown F/M SAND, little F/C Gravel, | 9.0 | |
| 10 | S-5 | 15 | 5-5-20-22 | | | | | M SAND AND SILT, trace Fine Brick and Cinder Fragments | | |
| | | | | | | 13.0 | | | 4.0 | |
| | S-6 | 16 | 2-1-1-1 | | 1 | | Dark gray Silt | y CLAY, trace Fine Sand | | |
| 20 | S-7 | 24 | WOH/6"-1- 2-2 | | | | Dark gray to b | brown Clayey SILT, trace Fine Sand | -2.0 | |
| 25 | S-8 | 24 | 1-1-1-1 | | 2 | | | SILT, Organics, trace Fine Sand ND F/M SAND | -6.0 -7.0 | |
| - - <u>30</u> | S-9 | 8 | 4-6-7-8 | | 3 | 28.0 | Tan to gray M | /F SAND, trace Silt | -11.0 | Wet on spoon |
| 35 | S-10 | 14 | 4-6-7-9 | | | 33.0 | Gray M/F SAN | ND, trace Silt | -16.0 | |
| NOTES | <u>S:</u> | | | | | | | | | |



| Per | nor | į | | | T | ES | PAGE 1 OF 2 | | | |
|---------------------|-----------------------|----------------|----------------|----------------|-------------|------|---------------------|---|-------|--------------------|
| PROJEC | T NUMB | ER PR | PAX17013.0 |)4 | | | | PROJECT LOCATION Philadelphia, P | A | USE |
| | | | | | | | 12/22/17 | GROUND ELEVATION <u>16.5 +/- feet N</u> WATER ENCOUNTERED: | AVD88 | |
| | | | low Stem Au | | | | | ∇ | 3.50 | |
| | | | Blemings | | | - | | AT END OF DRILLING | | |
| LOGGE | DBY D. | Copela | nd | CHE | CKE | DBY | D. Marrano | AFTER DRILLING | | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | Dept | | ESCRIPTION | Elev. | REMARKS |
| | S-1 | 18 | 1-10-5-5 | | P | | $_{-1}6.0$ in. PROC | ESSED AGGREGATE Fine SAND AND Fine gravel size | | |
| | x s-2 | 6 | 8-7-10-11 | | | | ROCK FRAG | MENTS, trace Silt | | |
| | X s-3 | 8 | 6-8-7-9 | | | 4.0 | FILL: Brown M | licaceous Fine SAND AND SILT | 12.5 | Moist |
| | / X | . 3 | 15-8-6-6 | | F | | | | | |
| _ ⊻ | X S-5 | 18 | 8-6-6-5 | | | 8.0 | FILL: Black S | ILT, some F/M Sand size Incinerate | 8.5 | Wet |
| | | | | | | 13.0 | Material, trace | organics | 3.5 | |
| _ <u>15</u> / | S-6 | 24 | 1/12"-1/12" | | | | Brown to gray | v Silty CLAY, trace Organics | | |
| _ <u>20</u> | S-7 | 24 | WOH/24" | | 1 | 18.0 | Brown to gray | Silty CLAY, some Organics | -1.5 | |
| | | | | | | | | | | |
| 25 / | S-8 | 24 | 1-1-1-1 | - | 2 | 23.0 | Dark brown S | ILT AND ORGANICS | -6.5 | |
| | | | | | | 28.0 | | | -11.5 | |
| _ 30 | S-9 | 18 | 7-9-12-13 | | · · · | | Brown M/F S/ | AND, trace Silt | | Added drilling mud |
| | | | | | 3 | | | | | |
| 35 | S-10 | 18 | 6-8-7-5 | | | | | | | |
| NOTES | <u>.</u> | | | | | | | | | |
| | | | | | | | | | | |

| Pe | nnoņi |) | | | Т | EST BORING LOG | BORING B-19 PAGE 2 OF 2 |
|---------------------|-----------------------|----------------|-----------------------------|----------------|--------|---|----------------------------|
| | | | gional Port A PAX17013.0 | Authori | | PROJECT NAME PhilaPort Distribution Wareh PROJECT LOCATION Philadelphia, PA | ouse |
| DEPTH (ft) 22 | SAMPLE TYPE NUMBER | RECOVERY (in.) | BLOW COUNTS | GRAPHIC LOG | STRATA | DESCRIPTION | REMARKS |
| | - | | | | | Brown M/F SAND, trace Silt <i>(continued)</i> | |
| - 40 | S-11 | 18 | 5-5-7-6 | | 3 | | |
| <u>45</u> | S-12 | 16 | 22-29-6-9 | | | 43.0 -26.5 Brown F/C GRAVEL AND M/F SAND, trace Silt | |
| _ 50 | S-13 | 16 | 10-13-15- 18 | | 4 | | |
| <u>55</u> | S-14 | 16 | 10-11-12- 15 | | | | |
| <u>60</u> | S-15 | 16 | 10-10-8-13 | | | 60.0 -43.5 Boring terminated at 60.0 feet. | |
| | | | | | | bonng terminated at 60.0 reet. | |
| NOTES | <u>S:</u> | | | | | | |





| Pen | noni |) | | | TEST | PIT LOG | Test Pit TP-1 PAGE 1 OF 1 |
|-----------------|-------------------------|----------------|--------|---------|---|--|------------------------------|
| | Philadelph | ia Regi | onall | Port Au | thority | PROJECT NAME _ PhilaPort Distribution Warehouse | |
| | T NUMBER | | | | | PROJECT LOCATION Philadelphia, PA | |
| | ARTED 4 | | | | | | |
| | | | | | nt Group, LLC | | |
| | TION METI OR / HELPI | | | er Tire | Backnoe | | |
| | BY <u>N. Di</u> | | | | CHECKED BY _D. Marano | AT END OF EXCAVATION Ψ 0 HRS AFTER EXCAVATION $8.0'$ / Elev $0.5'$ | |
| LOGGED | | 00330 | | | | | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | GRAPHIC LOG | STRATA | Depth | DESC | | REMARKS |
| Ŭ | | | | 0.3 | ASPHALT | 8.3 | |
| | | 60% | Р | 1.0 | Processed Aggregate similar to | 9 3A 7.5 | |
| | | | | | FILL: Gray F/M/C SAND and F trace Silt | GRAVEL and BRICK FRAGMENTS, | |
| | | | F | 4.0 | FILL: Black SILT, some F/M Sa | and, trace F/C Gravel | Trace Timber |
| | | | | | | | Asphalt Odor |
| | | | | 9.0 | Test Pit terminated at 9.0 feet. | -0.5 | |
| | | | | | | | |
| <u>NOTES:</u> | | | | | | | |

| Per | noni |) | | | TEST | PIT LOG | Test Pit TP-2 PAGE 1 OF 1 |
|---------------|-----------------------|----------------|--------|---------------|----------------------------------|--|------------------------------|
| CLIENT | Philadelph | nia Regi | onal I | Port Au | thority | PROJECT NAME _ PhilaPort Distribution Warehouse | |
| | T NUMBER | | | | | PROJECT LOCATION Philadelphia, PA | |
| | | | | | COMPLETED <u>4/18/19</u> | | |
| | | | | | nt Group, LLC | | |
| | ATION MET | | | er Tire i | Васкпое | DURING EXCAVATION AT END OF EXCAVATION | |
| | D BY <u>N. D</u> | | | | CHECKED BY D. Marano | Ψ 0 HRS AFTER EXCAVATION _9.0' / Elev -0.5' | |
| | | | | | | | |
| DEPTH (ft) | SAMPLE TYPE NUMBER | GRAPHIC LOG | STRATA | Doubh | DESC | RIPTION | REMARKS |
| 0 | | | | Depth 0.3_ | ASPHALT | Elev | |
| | | 000 | Р | 1.0 | Processed Aggregate similar to | 3A 7.5 | |
| | | | | | FILL: Red-Brown F SAND and | SILT | |
| | | | | | | | |
| | | | | | | | |
| | | | | 3.0 | FILL: Green micaceous F SAN | 5.5 D and SILT_trace E/C Gravel | |
| | | | | 10 | | | |
| | | | | 4.0 | FILL: Black F SAND, some SIL | 4.5 T and F/C Gravel | |
| 5 | | | F | | | | |
| | | | | | | | |
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| | | | | | | | |
| | | | | | | | |
| <u> </u> | | | | 9.0 | | -0.5 | Oily water surface |
| | | | | | Test Pit terminated at 9.0 feet. | | |
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| NOTES | <u>):</u> | | | | | | |
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| Per | nnoni |) | | | TEST | PIT LOG | Test Pit TP-3 PAGE 1 OF 1 | | | |
|---------------|---|----------------|--------|--------------|----------------------------------|--|------------------------------|--|--|--|
| CLIENT | CLIENT Philadelphia Regional Port Authority PROJECT NAME PhilaPort Distribution Warehouse | | | | | | | | | |
| PROJEC | PROJECT NUMBER PRPAX17013 PROJECT LOCATION Philadelphia, PA | | | | | | | | | |
| | | | | | COMPLETED <u>4/18/19</u> | | | | | |
| | | | | | nt Group, LLC | | | | | |
| | ATION METI | | | er Tire | Backhoe | | | | | |
| | | | | | CHECKED BY _D. Marano | AT END OF EXCAVATION AFTER EXCAVATION | | | | |
| LUGGE | | | | | | | | | | |
| DEPTH (ft) | SAMPLE TYPE NUMBER | GRAPHIC LOG | STRATA | Dereth | | RIPTION | REMARKS | | | |
| 0 | | | | Depth 0.3 | ASPHALT | Elev | | | | |
| | | | Р | 1.0 | Processed Aggregate similar to | o 3A 7.0 | | | | |
| | | | | 1.0 | FILL: Tan F/M SAND, some C | | | | | |
| | | | | 4.0 | FILL: Black F/M SAND, some | 4.0 C/F Gravel, trace Silt | | | | |
| | | | F | 6.0 | FILL: Black F/M SAND, some | 2.0 to little Silt, little F Gravel | | | | |
| | | | | 11.0 | | -3.0 | | | | |
| | | | | | Test Pit terminated at 11.0 feet | i. | | | | |
| | | | | | | | | | | |
| NOTES | <u>5'</u> | | | | | | | | | |

| Per | nnoni |) | | | TES | Γ PIT LOG | Test Pit TP-4 PAGE 1 OF 1 | | | |
|-----------------|---|----------------|--------|---------|---|---|------------------------------|--|--|--|
| CLIENT | CLIENT Philadelphia Regional Port Authority PROJECT NAME PhilaPort Distribution Warehouse | | | | | | | | | |
| PROJEC | ROJECT NUMBER PRPAX17013 PROJECT LOCATION Philadelphia, PA | | | | | | | | | |
| DATE S | | 4/18/19 | | | COMPLETED <u>4/18/19</u> | _ GROUND ELEVATION _8.0' | | | | |
| EXCAVA | XCAVATION CONTRACTOR Ambient Group, LLC WATER ENCOUNTERED: | | | | | | | | | |
| | TION MET | | | er Tire | Backhoe | | | | | |
| | FOR / HELF | | | | | AT END OF EXCAVATION | | | | |
| LOGGE | D BY <u>N. C</u> | i Sessa | T | | CHECKED BY D. Marano | _ Ψ 0 HRS AFTER EXCAVATION _9.0' / Ele | ev -1.0' | | | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | GRAPHIC LOG | STRATA | Depth | | | REMARKS | | | |
| | | | | 0.3 | ASPHALT | | 7.7 | | | |
| | | 600 | P | 1.0 | Processed Aggregate similar | to 3A | 7.0 | | | |
| | | | > | | | Gravel, some Clay, trace Brick | | | | |
| | | | F | 4.0 | Fragments FILL: Black F/M SAND, some Silt | F Gravel, trace Brick Fragments and | 4.0 | | | |
| _ <u>v</u> | | | | | | | | | | |
| | | | 2 | 9.5 | Test Pit terminated at 9.5 feet. | | 1.5 | | | |
| NOTES | | | | | | | | | | |
| NOTES | <u>.</u> | | | | | | | | | |

| Per | nnoni |) | | TEST PIT LOG | | Test Pit TP-5 PAGE 1 OF 1 | | | |
|-----------------|---|----------------|--------|---|-------------|------------------------------|--|--|--|
| CLIENT | CLIENT _ Philadelphia Regional Port Authority PROJECT NAME _ PhilaPort Distribution Warehouse | | | | | | | | |
| PROJEC | PROJECT NUMBER PRPAX17013 PROJECT LOCATION Philadelphia, PA | | | | | | | | |
| DATE S | DATE STARTED 4/18/19 COMPLETED 4/18/19 GROUND ELEVATION 10.0' | | | | | | | | |
| EXCAV | ATION CON | TRACT | OR | mbient Group, LLC WATER ENCOUNTERED: | | | | | |
| EXCAV | ATION MET | HOD _ | Rubb | Tire Backhoe DURING EXCAVATION | | | | | |
| OPERAT | TOR / HELP | PER Vi | ictor | AT END OF EXCAVATION | | | | | |
| LOGGE | D BY <u>N. D</u> | i Sessa | 1 | CHECKED BY D. Marano I O HRS AFTER EXCAVATION 9.0' | / Elev 1.0' | | | | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | GRAPHIC LOG | STRATA | | Elev. | REMARKS | | | |
| | | | | 0.3 ASPHALT | 9.7 | | | | |
| | | 600 | P | Processed Aggregate similar to 3A | 9.0 | | | | |
| | | | | FILL: Brown C/F gravel size ROCK FRAGMENTS and F/M SAND, | 8.5 | | | | |
| | | | | trace Silt | | | | | |
| | | | | FILL: Tan F/M SAND, little F Gravel, trace Silt and Brick Fragments | | Rebar Encountered | | | |
| | | | | 3.0 | 7.0 | | | | |
| | | | | FILL: Black F/M SAND, some Brick Fragments, little F Gravel, trace | 1.0 | | | | |
| | | | | Cinder Fragments, glass | | | | | |
| | | | | | | | | | |
| 5 | | | | 5.0 | 5.0 | | | | |
| | | | F | FILL: Brown-Orange-Gray F/M/C SAND, some F/C Gravel, some Silt | 0.0 | | | | |
| | | | | | | | | | |
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| | | | Š. | | | | | | |
| | | | | | | | | | |
| | | | | 9.0 | 1.0 | | | | |
| <u> </u> | | | 1 | Test Pit terminated at 9.0 feet. | 1.0 | | | | |
| NOTES | <u>5:</u> | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |

| Per | nnoni |) | | TES | T PIT LOG | Test Pit TP-6 PAGE 1 OF 1 | | | | |
|-----------------|---|----------------|--------|--|---|------------------------------|--|--|--|--|
| CLIENT | CLIENT _ Philadelphia Regional Port Authority PROJECT NAME _ PhilaPort Distribution Warehouse | | | | | | | | | |
| | PROJECT NUMBER PRPAX17013 PROJECT LOCATION Philadelphia, PA | | | | | | | | | |
| DATE S | DATE STARTED _4/18/19 COMPLETED _4/18/19 GROUND ELEVATION _12.0' | | | | | | | | | |
| EXCAV | EXCAVATION CONTRACTOR Ambient Group, LLC WATER ENCOUNTERED: | | | | | | | | | |
| EXCAV | ATION MET | HOD _ | Rubb | ber Tire Backhoe | DURING EXCAVATION | | | | | |
| | TOR / HELF | | | | AT END OF EXCAVATION | | | | | |
| LOGGE | D BY <u>N. D</u> | i Sessa | 1 | CHECKED BY D. Marano | | 5' | | | | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | GRAPHIC LOG | STRATA | DES | | REMARKS | | | | |
| 0 | | 00(| | | | | | | | |
| | | 00 | P | Processed Aggregate simila | ar to 3A 11.0 | | | | | |
| | | | > | FILL: Brown F/M SAND, so | | | | | | |
| | | | > | 2.0 | 10.0 | | | | | |
| | | | > | FILL: Brown to Tan F/M SA | ND, little F Gravel, trace Silt | | | | | |
| | | | > | 3.0 | 9.0 | | | | | |
| | | | | FILL: Brown to Black F/M S Fragments and Silt | SAND, little F Gravel, trace Cinder | | | | | |
| | | | > | | | | | | | |
| | | | > | | | | | | | |
| 5 | | | > | 5.0 FILL: Black E/M SAND, son | 7.0 ne Silt, some to little F/C Gravel and Brick | | | | | |
| | | | F | Fragments | | | | | | |
| | - | | | | | | | | | |
| | | | | | | | | | | |
| | - | | | | | Telphone poles | | | | |
| | | | | | | | | | | |
| | | | > | | | Hole collapsed | | | | |
| | | | > | | | | | | | |
| | | | > | | | | | | | |
| 10 | | | > | | | | | | | |
| y | , | | > | 10.5 | 1.5 | | | | | |
| | | | | Test Pit terminated at 10.5 f | reet. | | | | | |
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| NOTES | S: | | | | | | | | | |
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| Penn | oni | | | TEST | F PIT LOG | Test Pit TP-7 PAGE 1 OF 1 | | | | |
|--------------------------------------|---|-----------------------------------|-------|---------------------------------|---|------------------------------|--|--|--|--|
| CLIENT P | CLIENT Philadelphia Regional Port Authority PROJECT NAME PhilaPort Distribution Warehou | | | | | | | | | |
| PROJECT N | IUMBER _ PR | PROJECT LOCATION Philadelphia, PA | | | | | | | | |
| DATE STAF | RTED _4/19/1 | 9 | | COMPLETED <u>4/19/19</u> | GROUND ELEVATION 10.0' | | | | | |
| | | | | nt Group, LLC | | | | | | |
| | ON METHOD | | | Backhoe | | | | | | |
| | | | | | _ AT END OF EXCAVATION | | | | | |
| | | sa | | CHECKED BY D. Marano | AFTER EXCAVATION | - | | | | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER GRAPHIC | STRATA | Depth | DESC | | REMARKS | | | | |
| Ŭ | | | 0.5 | ASPHALT | 9.5 | | | | | |
| | | | 1.0 | Processed Aggregate similar t | o 3A 9.0 | | | | | |
| | | F | 6.0 | FILL: Tan to Brown F/M SANE | 4.0 F/C GRAVEL and BRICK organics, debris, wood | | | | | |
| | KXX | <u> </u> | 11.0 | Test Pit terminated at 11.0 fee | | | | | | |
| <u>NOTES:</u> | | | | | | | | | | |

| Per | nnoni |) | | | TEST | PIT LOG | Test Pit TP-8 PAGE 1 OF 1 |
|----------------------------------|--------------------------|----------------|--------|--------------|----------------------------------|--|------------------------------|
| CLIENT | Philadelph | ia Regi | onal I | Port Au | thority | PROJECT NAME _ PhilaPort Distribution Wareho | use |
| | T NUMBER | | | | | PROJECT LOCATION Philadelphia, PA | |
| DATE S | TARTED _4 | /19/19 | | | COMPLETED _4/19/19 | GROUND ELEVATION 10.0' | |
| EXCAV | | TRACT | OR | Ambie | nt Group, LLC | WATER ENCOUNTERED: | |
| EXCAV | ATION MET | HOD _ | Rubb | er Tire | Backhoe | DURING EXCAVATION | |
| | TOR / HELP | | | | | AT END OF EXCAVATION | |
| LOGGE | D BY <u>N. Di</u> | Sessa | | | CHECKED BY D. Marano | AFTER EXCAVATION | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | GRAPHIC LOG | STRATA | Donth | DESC | | REMARKS |
| | | | | Depth 0.3 | ASPHALT | Elev. 9.7 | |
| | | 000 | Р | 1.0 | Processed Aggregate similar to | 9.0 3A | |
| | | | | 1.0 | FILL: Tan to Brown F/M SAND | | - |
| | | | F | 4.0 | | 6.0 F/C BRICK FRAGMENTS, little Clay, | |
| | | | | 11.0 | Test Pit terminated at 11.0 feel | -1.0 | |
| NOTES | <u>S:</u> | | | | | | |
| | | | | | | | |

| Per | nnoni |) | | | TEST | F PIT LOG | Test Pit TP-9 PAGE 1 OF 1 |
|---------------|-----------------------|----------------|--------|--------------|---------------------------------|---|------------------------------|
| CLIENT | Philadelph | nia Regi | onal I | Port Au | thority | PROJECT NAME _ PhilaPort Distribution Warehouse | |
| | | | | | | PROJECT LOCATION Philadelphia, PA | |
| | | | | | COMPLETED _4/19/19 | | |
| | | | | | nt Group, LLC | | |
| | ATION MET | | - | | | | |
| | FOR / HELP | | | | | AT END OF EXCAVATION | |
| | | | | | CHECKED BY D. Marano | | |
| DEPTH (ft) | SAMPLE TYPE NUMBER | GRAPHIC LOG | STRATA | Death | DESC | RIPTION | REMARKS |
| 0 | | | | Depth 0.3 | ASPHALT | Elev. 8.7 | |
| | | | | | Processed Aggregate similar to | o 3A | |
| | | | | 1.0 | FILL: Black F/C GRAVEL and | 8.0 F/M/C SAND, little Silt | |
| | | | | 4.0 | FILL: Brown SILT, some F/M S | 5.0 | |
| 1 | | | | | FILL: Brown SILT, some F/M | SAND, trace F Graver | |
| 5 | | | | | | | |
| | | | | | | | |
| | | | F | 6.0 | | 3.0 | |
| - ⊻ | | | | | FILL: Black Silty Clay, some F | | |
| | | | | 11.0 | Test Pit terminated at 11.0 fee | 2.0 | |
| NOTES | <u>.</u> | | | | | | |

| Pennoni | | TEST | PIT LOG | Test Pit TP-10 PAGE 1 OF 1 |
|--|--------------|---|--|-------------------------------|
| CLIENT Philadelphia Regi | onal Port A | uthority | PROJECT NAME _ PhilaPort Distribution Warehous | e |
| PROJECT NUMBER PRP | | | PROJECT LOCATION Philadelphia, PA | |
| | | _ COMPLETED _4/19/19 | | _ |
| EXCAVATION CONTRACT | | ent Group, LLC | DURING EXCAVATION | |
| OPERATOR / HELPER _Vi | | | AT END OF EXCAVATION | |
| LOGGED BY <u>N. Di Sessa</u> | | CHECKED BY _D. Marano | $\underline{\Psi}$ 0 HRS AFTER EXCAVATION <u>9.0' / Elev 0.0</u> | |
| | | | | |
| o DEPTH (ft) SAMPLE TYPE NUMBER CRAPHIC LOG | STRATA | | RIPTION | REMARKS |
| | Deptl 0.3 | | Elev. 8.8 | |
| | P 1.0 | Processed Aggregate similar to | 3 3A 8.0 | |
| | | FILL: Black F/C GRAVEL and | | |
| | <u>4.0</u> | FILL: Brown F/M SAND, some Fragments, trace Clay | 5.0 Silt, little F/C Gravel and Brick | |
| <u> </u> | 9.0 | Test Pit terminated at 9.0 feet. | 0.0 | |
| <u>NOTES:</u> | | | | |

| Per | nnoni |) | | | TEST | F PIT LOG | Test Pit P-1 PAGE 1 OF 1 |
|-----------------|-----------------------|----------------|--------|-----------|--|---|-----------------------------|
| CLIENT | Philadelph | ia Regi | onal | Port Au | thority | PROJECT NAME PhilaPort Distribution Warehouse | |
| PROJE | | R PRP | AX17 | 013 | | PROJECT LOCATION Philadelphia, PA | |
| DATE S | | /18/19 | | | COMPLETED <u>4/18/19</u> | GROUND ELEVATION 8.0' | |
| | | | | | nt Group, LLC | WATER ENCOUNTERED: | |
| | ATION MET | | | er Tire I | Backhoe | DURING EXCAVATION | |
| | TOR / HELP | | | | | AT END OF EXCAVATION | |
| | DBY <u>E. la</u> | nnetti | | | CHECKED BY D. Marano | _ AFTER EXCAVATION | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | GRAPHIC LOG | STRATA | Depth | DESC | | REMARKS |
| | | | | 0.5 | 6" ASPHALT | 7.5 | |
| | | \sim | Р | 1.0 | 6" Processed Aggregate simila | | |
| | | | | 1.3 | Tan F/M/C SAND Test Pit terminated at 1.3 feet. | 6.7 | |
| | | | | | | | |
| NOTES | <u>S:</u> | | | | | | |

| Per | nnoni |) | | | TES | F PIT LOG | Test Pit P-2 PAGE 1 OF 1 |
|-----------------|-----------------------|----------------|--------|------------|-------------------------------|---|-----------------------------|
| CLIENT | Philadelph | nia Regi | onal | Port Au | ithority | PROJECT NAME PhilaPort Distribution Warehouse | |
| PROJEC | | | AX17 | 013 | | PROJECT LOCATION Philadelphia, PA | |
| DATE S | | 4/18/19 | | | COMPLETED 4/18/19 | GROUND ELEVATION 12.0' | |
| EXCAV | ATION CON | TRACT | OR | Ambie | nt Group, LLC | WATER ENCOUNTERED: | |
| EXCAV | ATION MET | HOD _ | Rubb | er Tire | Backhoe | DURING EXCAVATION | |
| | FOR / HELP | | ctor | | | AT END OF EXCAVATION | |
| LOGGE | DBY <u>E. la</u> | nnetti | 1 | | CHECKED BY D. Marano | AFTER EXCAVATION | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | GRAPHIC LOG | STRATA | Depth | | | REMARKS |
| 0 | | | | 0.4 | 5" ASPHALT | 11.6 | |
| | | 0 | Р | | 9" Processed Aggregate simila | ar to 3A | |
| | | | | 1.2 1.5 | _ Tan F/M/C SAND | <u> </u> | |
| | | | | | | | |
| NOTES | <u>S:</u> | | | | | | |

| Per | nnoni |) | | | TES | ST | PIT LOG | | Test Pit P-3 PAGE 1 OF 1 |
|-----------------|--------------------------|----------------|--------|---------|---|-----|--|---------|-----------------------------|
| CLIENT | Philadelph | nia Regi | ional | Port Au | ithority | | PROJECT NAME PhilaPort Distribution Wa | rehouse | |
| | | | | | | | PROJECT LOCATION _ Philadelphia, PA | | |
| DATE S | | 4/18/19 | | | COMPLETED <u>4/18/19</u> | | GROUND ELEVATION 12.0' | | |
| EXCAV | ATION CON | TRACI | OR | Ambie | nt Group, LLC | | WATER ENCOUNTERED: | | |
| EXCAV | ATION MET | HOD _ | Rubb | er Tire | Backhoe | | DURING EXCAVATION | | |
| | TOR / HELP | | | | | | AT END OF EXCAVATION | | |
| LOGGE | D BY <u>E. la</u> | nnetti | | | CHECKED BY D. Marano | | AFTER EXCAVATION | | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | GRAPHIC LOG | STRATA | Depth | | SCI | RIPTION | Elev. | REMARKS |
| | | | Б | 0.4 | 5" ASPHALT | | | 11.6 | |
| | | | ч 1 | 1.1 | 8" Processed Aggregate sin Test Pit terminated at 1.1 fe | | to 3A | 10.9 | |
| | | | | | | | | | |
| NOTES | <u>S:</u> | | | | | | | | |

| Pennoni | TEST | PIT LOG | Test Pit P-4 PAGE 1 OF 1 |
|---|----------------------------------|---|------------------------------|
| CLIENT _ Philadelphia Regional Port Au | uthority | PROJECT NAME _ PhilaPort Distribution Warehou | ISE |
| PROJECT NUMBER PRPAX17013 | | PROJECT LOCATION Philadelphia, PA | |
| DATE STARTED 4/18/19 | COMPLETED 4/18/19 | | |
| EXCAVATION CONTRACTOR Ambie | ent Group, LLC | WATER ENCOUNTERED: | |
| EXCAVATION METHOD Rubber Tire | Backhoe | DURING EXCAVATION | |
| OPERATOR / HELPER Victor | | AT END OF EXCAVATION | |
| LOGGED BY E. lannetti | CHECKED BY D. Marano | AFTER EXCAVATION | |
| DEPTH (ft) (ft) (ft) (ft) (ft) (ft) (ft) (ft) | | RIPTION | REMARKS |
| 0 Depth 0.3 | _ 4" ASPHALT | Elev. 8.7 | Concrete slab encountered on |
| P | 11" Processed Aggregate simila | | one side of test pit |
| | Test Pit terminated at 1.3 feet. | 7.8 | |
| | | | |
| <u>NOTES:</u> | | | |

| Pennoni | TEST | PIT LOG | Test Pit P-5 PAGE 1 OF 1 |
|---|--|---|-----------------------------|
| CLIENT _ Philadelphia Regional Port A | uthority | PROJECT NAME _ PhilaPort Distribution Warehouse | |
| PROJECT NUMBER PRPAX17013 | | PROJECT LOCATION Philadelphia, PA | |
| DATE STARTED 4/18/19 | COMPLETED 4/18/19 | | |
| EXCAVATION CONTRACTOR _ Ambie | | | |
| EXCAVATION METHOD Rubber Tire | | DURING EXCAVATION | |
| OPERATOR / HELPER Victor | | AT END OF EXCAVATION | |
| LOGGED BY E. lannetti | CHECKED BY D. Marano | AFTER EXCAVATION | |
| o DEPTH (ft) (ft) (ft) (ft) (ft) (ft) (ft) (ft) | | | REMARKS |
| 0.3 | _4" ASPHALT | 8.7 | |
| 007 1.0 | 8" Processed Aggregate similar Test Pit terminated at 1.0 feet. | to 3A 8.0 | |
| | | | |
| <u>NOTES:</u> | | | |

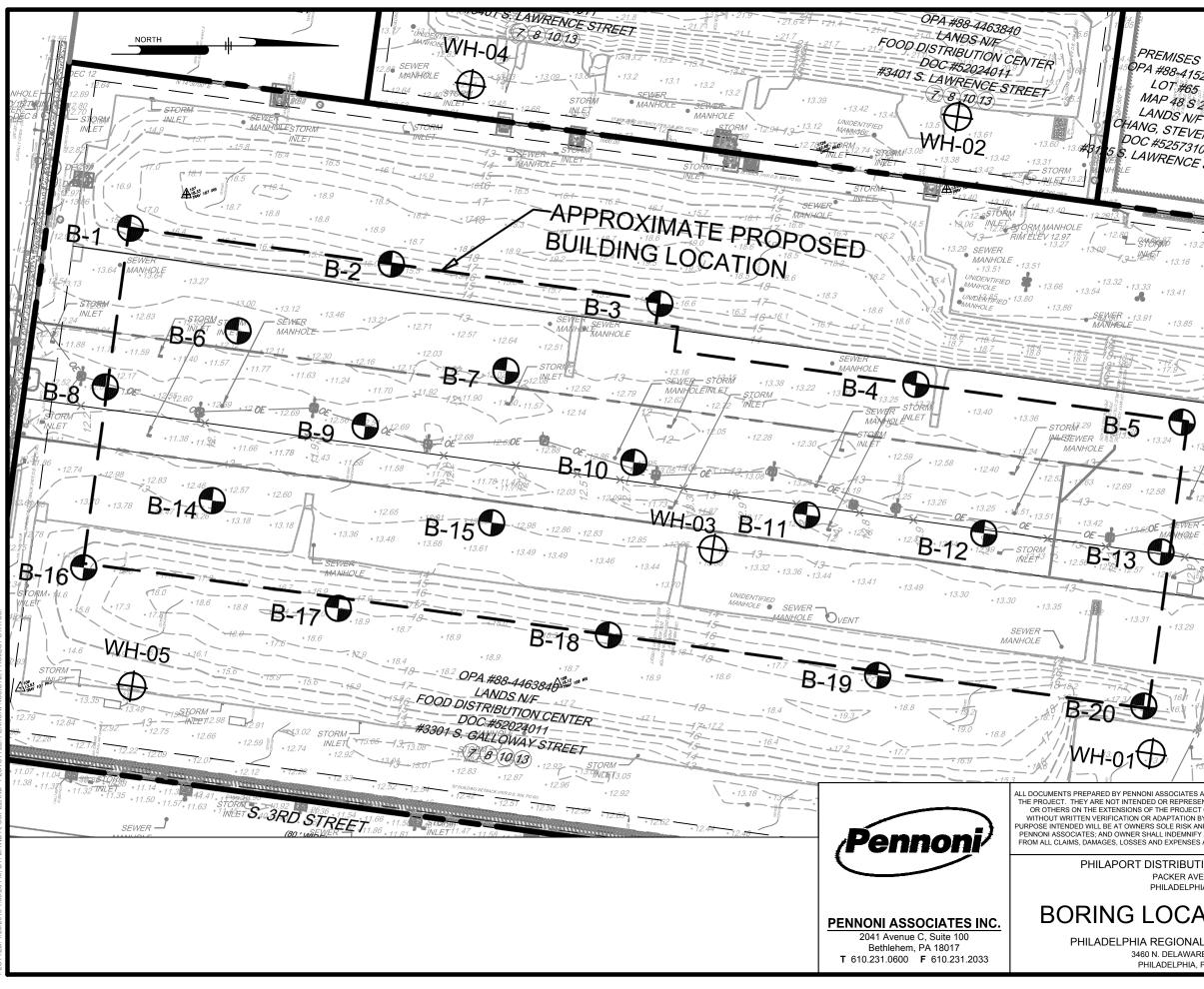
| Pennoni | TEST | PIT LOG | Test Pit P-6 PAGE 1 OF 1 |
|--|--|---|-----------------------------|
| CLIENT Philadelphia Regiona | l Port Authority | PROJECT NAME _ PhilaPort Distribution Warehouse | |
| PROJECT NUMBER PRPAX | | | |
| | COMPLETED _4/18/19 | | |
| | Ambient Group, LLC | | |
| | ber Tire Backhoe | DURING EXCAVATION | |
| OPERATOR / HELPER Victor | | AT END OF EXCAVATION | |
| LOGGED BY E. lannetti | CHECKED BY D. Marano | AFTER EXCAVATION | |
| o DEPTH (ft) SAMPLE TYPE NUMBER NUMBER CRAPHIC LOG | Depth | | REMARKS |
| POLP | 0.3 4" ASPHALT | 10.7 | |
| | 1.1 | • to 3A 9.9 | |
| | Tan F/M/C SAND Test Pit terminated at 1.2 feet. | <u>9.8</u> / | |
| | | | |
| <u>NOTES:</u> | | | |

| Pennoni | TEST | PIT LOG | Test Pit P-7 PAGE 1 OF 1 |
|---|----------------------------------|---|-----------------------------|
| CLIENT _ Philadelphia Regional Port Au | thority | PROJECT NAME _ PhilaPort Distribution Warehouse | |
| PROJECT NUMBER PRPAX17013 | | PROJECT LOCATION Philadelphia, PA | |
| DATE STARTED 4/18/19 | COMPLETED 4/18/19 | GROUND ELEVATION 12.5' | |
| EXCAVATION CONTRACTOR _Ambie | nt Group, LLC | WATER ENCOUNTERED: | |
| EXCAVATION METHOD Rubber Tire | Backhoe | DURING EXCAVATION | |
| OPERATOR / HELPER Victor | | AT END OF EXCAVATION | |
| LOGGED BY E. lannetti | CHECKED BY D. Marano | AFTER EXCAVATION | |
| 0 DEPTH (ft) (ft) (ft) (ft) SAMPLE TYPE NUMBER NUMBER LOG STRATA STRATA | | | REMARKS |
| 0.3 | _4" ASPHALT | 12.2 | |
| | 10" Processed Aggregate simila | | |
| <u> 1.2</u> | Test Pit terminated at 1.2 feet. | 11.3 | |
| | | | |
| <u>NOTES:</u> | | | |

| Pennoni | TEST | PIT LOG | Test Pit P-8 PAGE 1 OF 1 |
|---|----------------------------------|---|-----------------------------|
| CLIENT _ Philadelphia Regional Port Au | uthority | PROJECT NAME _ PhilaPort Distribution Warehouse | |
| PROJECT NUMBER PRPAX17013 | | PROJECT LOCATION Philadelphia, PA | |
| DATE STARTED 4/18/19 | COMPLETED <u>4/18/19</u> | GROUND ELEVATION 9.0' | |
| EXCAVATION CONTRACTOR Ambie | ent Group, LLC | WATER ENCOUNTERED: | |
| EXCAVATION METHOD Rubber Tire | Backhoe | DURING EXCAVATION | |
| | | | |
| LOGGED BY E. lannetti | CHECKED BY D. Marano | AFTER EXCAVATION | |
| o DEPTH (ft) (ft) (ft) (ft) (ft) (ft) (ft) (ft) | | | REMARKS |
| 0.3 | _4" ASPHALT | 8.7 | |
| P C P | 10" Processed Aggregate simila | | |
| | Test Pit terminated at 1.2 feet. | 7.8 | |
| | | | |
| <u>NOTES:</u> | | | |

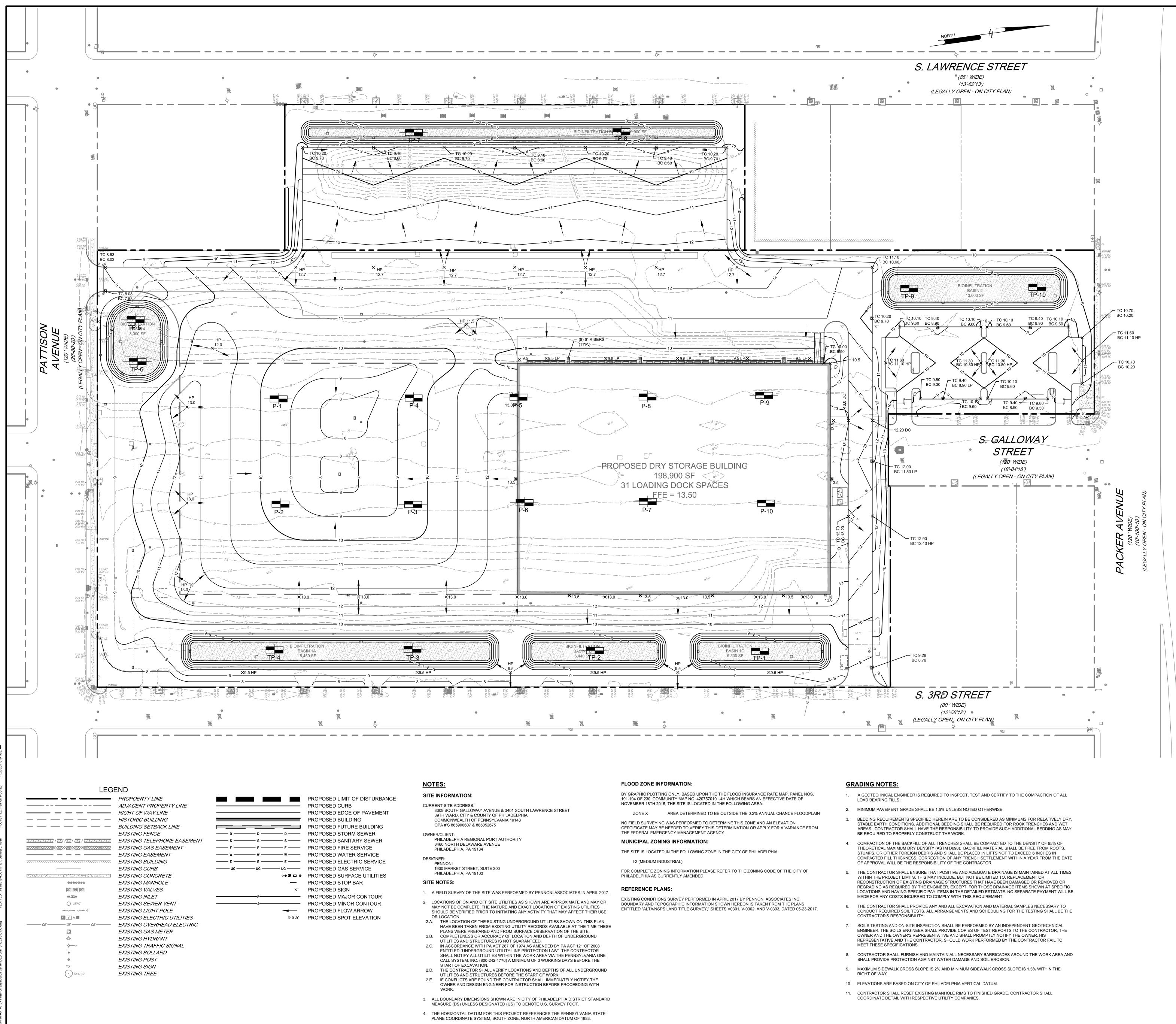
| Pennoni TEST PIT LOG | Test Pit P-9 PAGE 1 OF 1 |
|--|-----------------------------|
| CLIENT _ Philadelphia Regional Port Authority PROJECT NAME _ PhilaPort Distribution Warehouse | |
| PROJECT NUMBER PRPAX17013 PROJECT LOCATION Philadelphia, PA | |
| DATE STARTED _4/18/19 COMPLETED _4/18/19 GROUND ELEVATION _9.0' | |
| EXCAVATION CONTRACTOR Ambient Group, LLC WATER ENCOUNTERED: | |
| EXCAVATION METHOD Rubber Tire Backhoe DURING EXCAVATION | |
| OPERATOR / HELPER _Victor AT END OF EXCAVATION LOGGED BY _E. lannetti CHECKED BY _D. Marano AFTER EXCAVATION | |
| | |
| HLdag Baker Algebra DESCRIPTION 0 Depth Elev. | REMARKS |
| 7" ASPHALT | |
| P 0.6 8.4 6" Processed Aggregate similar to 3A 7.9 Test Pit terminated at 1.1 feet. | |
| | |
| NOTES: | |

| Per | nnoni |) | | | TES | T PIT LOG | | Test Pit P-10 PAGE 1 OF 1 |
|-----------------|-----------------------|----------------|---------|------------------------------|---------------------|---|--------------|------------------------------|
| CLIENT | Philadelph | nia Regi | ional I | Port Authority | | PROJECT NAME _ PhilaPort Distribution W | /arehouse | |
| PROJE | | R PRP | AX17 | /013 | | PROJECT LOCATION Philadelphia, PA | | |
| | | | | | | GROUND ELEVATION _13.0' | | |
| | | | | | | WATER ENCOUNTERED: | | |
| | | | | | | | | |
| | | | | | DBY_D. Marano | AT END OF EXCAVATION | | |
| LUGGE | | | | | | AFTER EXCAVATION | | |
| o DEPTH (ft) | SAMPLE TYPE NUMBER | GRAPHIC LOG | STRATA | Depth | DESC | CRIPTION | Elev. | REMARKS |
| | | | | _0.34" ASPH | | | 12.7 | |
| | | 000 | P | | cessed Aggregate si | nilar to 3A | | |
| | | <u>o 0</u> |] | 1.2 1.5 , Tan F/M/ | /C SAND | | 11.8 11.5 | |
| | | | | | | | | |
| NOTES | <u>S:</u> | | | | | | | |



| | | REVISIONS | | |
|----|-----------|----------------------------|---------|-----|
| NC |). | DESCRIPTION | DATE | BY |
| # | # | | # | # |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| | | LEGEND | | |
| | B-1 | INDICATES APPROXIMATE | · · | |
| | \bullet | BORING LOCATION AND ID | | |
| | • | NUMBER FOR THE CURREI | NISIUL | JY. |
| | | INDICATES APPROXIMATE | TEST | |
| | WH-01 | BORING LOCATION AND | | |
| | \oplus | IDENTIFYING NUMBER | | |
| | Ψ | CONDUCTED BY OTHERS F | FOR THE | Ξ |
| | | PRELIMINARY STUDY. | | |
| | | | | |
| | | | | |
| | | | | |
| | NOT | -0 | | |
| | NOTE | <u>=5</u> | | |
| | WAT | ER LEVELS, WHERE SHOWN, | ARE | |
| | | SE OBSERVED AT THE TIME N | | |
| | | MAY NOT REFLECT DAILY OF | | |
| | | SONAL VARIATIONS IN THE GI | ROUND | |
| | WAI | ER LEVEL. | | |
| | THE | SUBSURFACE CONDITIONS | | |
| | | EALED BY THIS STUDY REPRE | ESENT | |
| | | RENT CONDITIONS AT THE | | |
| | | CIFIED TEST LOCATIONS ONL | | |
| | | NOT BE INDICATIVE OF CONE | DITIONS | |
| | ALO | THER LOCATIONS. | | |
| | | | | |
| | | | | |
| | | | | |
| ĺ | | | | |

| | 100' 200' |
|--|-----------------------|
| ARE INSTRUMENTS OF SERVICE IN RESPECT OF NTED TO BE SUITABLE FOR REUSE BY OWNER | PROJECT PRPAX 17013 |
| OR ON ANY OTHER PROJECT. ANY REUSE Y PENNONI ASSOCIATES FOR THE SPECIFIC ID WITHOUT LIABILITY OR LEGAL EXPOSURE TO | DATE 2018-01-23 |
| AND HOLD HARMLESS PENNONI ASSOCIATES ARISING OUT OF OR RESULTING THEREFROM. | DRAWING SCALE 1"=100' |
| ION WAREHOUSE | DRAWN BY DAC |
| IA, PA | APPROVED BY DPM |
| TION PLAN | DRAWING NO. |
| L PORT AUTHORITY E AVENUE PA 19134 | SHEET 1 OF 1 |



- 5. THE VERTICAL DATUM FOR THIS PROJECT REFERENCES THE VERTICAL DATUM OF THE CITY OF PHILADELPHIA (CITY).





120

TEST BORING/TEST PIT/AUGER PROBE LOG KEY SHEET

| COLUMN | DESCRIPTION |
|-------------|--|
| Depth | Depth in feet below ground surface |
| Description | Description of sample including color, texture, and classification of subsurface material as applicable. Estimated depths to bottom of strata as interpolated from the boring are also shown. |
| Stratum | Strata numbers as assigned by the geotechnical engineer |
| Sample No. | Split barrel sample and sample number (S-x) Undisturbed Tube sample and sample number (U-x) Rock core run and core number (R-x) NR indicates no recovery |
| Blow Counts | For soils sample (ASTM D 1586): indicates number of blows obtained for each 6 inches penetration of the standard split-barrel sampler. |
| | For rock coring (ASTM D 2113): indicates percent recovery (REC) per run and rock quality designation (RQD). RQD is the sum of rock pieces that are 4 inches or longer in length in one core run divided by the total core run. |
| Recovery | For soil samples indicates the length of recovery in the sample spoon |
| Remarks | Special conditions or test data as noted during drilling |

Ground Water: Free water level as shown ()*; * Free water level as noted may not be indicative of daily, seasonal, or long term fluctuations.

DESCRIPTIVE TERMS

| 1 to 10 |
|----------|
| |
| 10 to 20 |
| 20 to 35 |
| 35 to 50 |
| |

| GRADATION OF COARSE | GRAINED COMPONENTS | 8 |
|---------------------|---|---|
| Size Range | Particle Size | |
| | Maximum | Minimum |
| | | 12" |
| | 12" | 3" |
| Coarse | 3" | 3/4" |
| Fine | 3/4" | #4 Sieve |
| Coarse | #4 Sieve | #10 Sieve |
| Medium | #10 Sieve | #40 Sieve |
| Fine | #40 Sieve | #200 Sieve |
| | #200 Sieve | .005 mm |
| | .005 mm | - |
| | <u>Size Range</u> Coarse Fine Coarse Medium | Maximum12"Coarse3"Fine34"Coarse#4 SieveMedium#10 SieveFine#40 Sieve#200 Sieve |

COMPOSITION OF COARSE-GRAINED COMPONENTS

| Gradation Designation | <u>Symbol</u> | Defining Proportions |
|-----------------------|---------------|---|
| Coarse to Fine | CF | All fractions greater than 10% of the component |
| Coarse to Medium | CM | Less than 10% Fine |
| Medium to Fine | MF | Less than 10% Coarse |
| Coarse | С | Less than 10% Fine and Medium |
| Medium | Μ | Less than 10% Coarse and Fine |
| Fine | F | Less than 10% Coarse and Medium |



| Boring WH-01 ECMS District:County: Philadelphia SRSection Baseline: FDC Site - Port Authority StaOffset SegmentOffset Coordinates: LatLong 219498.7770 E 2696490.0640 N Ground Elev. 14.0 ft Water Level Elev./Elapsed Time: $ age Initial -6.4 \text{ ft. }Elapsed 0.0 \text{ hr.} \\ Final -7.8 \text{ ft. }Elapsed 96.0 \text{ hr.} \\ Driller: Gary B. \\ Company: Allied Well Drilling \\ $ | Drilling Complete Grouting Complete Rig: <u>Acker XLS</u> Hammer Type: <u>Assumed 0.8</u> Hammer Calibrate Hole Type: <u>HS</u> Casing Type: <u>HS</u> Casing I.D.: <u>3.25</u> Rock Core Method Inspector: <u>Jeren</u> | e: 07/28 ote: 08/0 <u>Frack Rin</u> Automat ciency: <u></u> tion Dat <u></u> <u>SA/FJC -</u> <u>in</u> Cas od: ny Booze | /2017 2/201 g ic easurec e: Spun ing De er | 1:05 7 8:45 | 5 am | Final Lo By: <u>Ca</u> Date: _ | Seal, Si og Chu nrie N 9/21/2 Lab Tu on Sa S: N va | eckeo licho 2017 esting mple lues a | and Approved Ison |
|---|---|--|--|-----------------------|---|--------------------------------------|--|--|----------------------|
| HOBEOBEC - A HA HA MATERIAL DESC COMMENTS - OBSE | | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ 0.5ft) | 8 N ₆₀ RQD % | REC (ft.) | REC (%) | |
| Sta. Offset Segment Offset Coordinates: Lat. Lat. Long. 219498.7770 E 2696490.0640 N Ground Elev. 14.0 ft. Water Level Elev./Elapsed Time: Initial -6.4 ft. Elapsed 0.0 hr. Final -7.8 ft. Driller: Gary B. Company: Allied Well Drilling MATERIAL DESC Commany: Allied Well Drilling Matterial Desc Company: Allied Well Drilling Subbase. Subase. Subase. Subase. Subase. Subase. Subase. Subase. | between two 0.8'/El. 13.2 1.0'/El. 13.0 Silt, medium bus, well graded, in-plastic, gray to a in S-3. | a-2-4 / sm | - 1.0 - - 2.0 - - 4.0 - - 6.0 - | S-1 - S-2 - S-3 | 20-14 15-13-19-2 15-4-4-11 37-15-10-1 | 1 11 | 1.0 1.6 2.0 0.5 | 100 80 100 25 | |
| SILT and CLAY, some Sar soft, wet, heterogeneous, prounded to sub-angular, lo black, fill, - tar odor. | poorly graded, | a-2-4 / ml | - 0.0 - | - S-5 | 2-2-1-4 Pen=0.50 t | sf ⁴ | 2.0 | 100 | |
| CLAY and SILT, little Sand heterogeneous, poorly gra medium plastic fines, black alluvium, Class. on jar samples colle & SB-7T A-7-5(16)/ML | d, very soft, wet, ded, rounded, k to dark gray, | A-7-5 / ML | | S-6 | 2-1-1-2 Pen=0.25 t WOH-WOI WOH-4 Pen=0.25 t | H- 0 | 2.0 | 100 | |
| N.M.C.=62.4%. | 13.5'/El. 0.5 | A-4 / ML | - 14.0- | | 1-3-2-3 | | | | |



Boring WH-01

ENGINEER'S LOG

District: _____ County: <u>Philadelphia</u> SR ______ Section _____

Sta. _____ Offset _____

Sheet <u>2</u> of <u>5</u>

<u>NOTE</u>: N values and all graphical plots are for information only.

Lab Testing Performed on Sample

| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ 0.5ft) | N ₆₀ RQD % | REC (ft.) | REC (%) | ⊙ So 20 | il/Ro 40 . SP1 | Γ (N ₆₀ | ec.% ₀) ▲ | |
|-------|---------|--|------------------|-----------------|---------------|-------------------------------------|---------------------------------|--------------|------------|------------|----------------------|--|-----------------------------|-----------------|
| | | SILT and CLAY , some Sand, very soft, wet, lensed, poorly graded, rounded, non-plastic, brown, alluvium, | | - 16.0- | | Pen=0.25 tsf | 7 | 1.6 | 80 | | | | 40 / / () | 7 |
| | | Class. on jar samples collected from S-9 & S-10 A-4(0)/ML N.M.C.=52.9%. | | | S-9 | WOH-WOH- WOH-3 Pen=0.25 tsf | 0 | 1.6 | 80 | | | | | |
| -5 - | | (Layer continued from the previous page.) | A-4 / ML | - 18.0- | S-10 | WOH-WOH- WOH-WOH Pen=0.25 tsf | 0 | 2.0 | 100 | | | | | ! |
| 7 | | - pocket penetrometer readings are from clay seams; soil is lensed. | | - 20.0- | | | | | | | | | | |
| | | | | | | | | | | | | | | í |
| -10 - | | 24.0'/EI10.0 CLAY and SILT, some Sand, very soft, wet, | | - 24.0- | | | | | | | | | 1/ ! | |
| | | homogeneous, poorly graded, rounded, medium plastic fines, black to dark gray, alluvium. | | - 26.0- | S-11 | WOH-2-3-3 Pen=0.25 tsf | 7 | 1.1 | 55 | | | | | |
| | | | a-6 / cl | | | | | | | | | - <u> </u> <u> </u> | | |
| -15 - | | 29.0'/EI15.0 | | - 29.0- | | | | | | | | | V I | |
| -10 | | SAND , little Silt, little Gravel, medium dense, wet, heterogeneous, poorly graded, sub-rounded to sub-angular, non-plastic, brown, alluvium. | | | S-12 | 6-7-6-6 | 17 | 1.6 | 80 | | | | | |
| | | | a-3 / | - 31.0- | | | | | | | | | | |
| | | | sp | | | | | | | | | | | |
| -20 - | | | | - 34.0- | | | | | | | | | | |



Boring WH-01

ENGINEER'S LOG

District: _____ County: Philadelphia

SR _____ Section _____

Sta. _____ Offset _____

Sheet <u>3</u> of <u>5</u>

<u>NOTE</u>: N values and all graphical plots are for information only.

Lab Testing Performed on Sample

| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ | N ₆₀ RQD | REC (ft.) | REC (%) | ⊙ Soil/ | | Rec.% |
|-------|---|---|---------------------|-----------------|---------------|---------------------------|----------------------------|--------------|------------|------------|--------|---------------------------------------|
| ш | GR | | , 0000 | DI | SA | 0.5ft) | % | (10.) | (,,,) | ▲ \$ 10 | SPT (N | $I_{60}) \blacktriangle_{40}$ |
| - | | SAND , little Silt, little Gravel, medium dense, wet, heterogeneous, poorly graded, sub-rounded to sub-angular, non-plastic, brown, alluvium. (<i>Layer continued from the previous page.</i>) | | - 36.0- | S-13 | 6-7-7-8 | 19 | 1.6 | 80 | | | · · · · · · · · · · · · · · · · · · · |
| -25 - | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | | | | • S-14 | 5-5-8-6 | 17 | 1.4 | 70 | | | |
| -30 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | - hard to very hard, coarse gravel caused drill rig to abnormally vibrate when boring was advanced with tri-cone roller bit while applying downward pressure between 41.0' and 44.0'. | a-3 / sp | | • S-15 | 17-7-8-6 | 20 | 1.0 | 50 | | | |
| - | | 49.0'/El35.0 | | - 46.0- | | | | | | | | |
| -35 - | | SAND and GRAVEL, trace Silt, medium dense, wet, heterogeneous, well graded, sub-angular to angular, non-plastic, brown, | | - 49.0- | S-16 | 20-19-16-16 | 47 | 0.8 | 40 | | | |
| | | alluvium, Class. on jar samples collected from S-16 to S-19 A-1-b/SP-SM N.M.C.=10.5%. | A-1-b / SP-SM | - 51.0- | | | | | | | | |
| -40 - | | | | - 54.0- | | | | | | | | |



Boring WH-01

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Sheet <u>4</u> of <u>5</u>

<u>NOTE</u>: N values and all graphical plots are for information only.

| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ | N ₆₀ RQD | REC (ft.) | REC (%) | ⊙ Soil/ 20 | | | ;.% 80 |
|-------|---------|--|------------------|-----------------|---------------|---------------------------|----------------------------|--------------|------------|---------------|-------------|-------------------------|------------|
| ш | | | | D S/ | | 0.5ft) | % | | | 10 | SPT (20 | N ₆₀) 30 | 4 0 |
| | | SAND and GRAVEL , trace Silt, medium dense, wet, heterogeneous, well graded, sub-angular to angular, non-plastic, brown, alluvium, | | - 56.0- | S-17 | 14-12-10-11 | 29 | 1.5 | 75 | | | | D |
| -45 - | | Class. on jar samples collected from S-16 to S-19 A-1-b/SP-SM N.M.C.=10.5%. (Layer continued from the previous page.) | | | | | | | | | | | |
| | | | A-1-b | - 61.0- | S-18 | 10-9-8-7 | 23 | 1.2 | 60 | | | | |
| | | | SP-SM | | | | | | | | | | |
| -50 - | | | | - 64.0 - | S-19 | 11-7-6-7 | 17 | 1.5 | 75 | | | | |
| | | | | | | | | | | | | | |
| -55 - | | 69.0'/EI55.0 GRAVEL and SAND, little Clay, dense to very dense, wet, heterogeneous, poorly graded, sub-angular to angular, medium plastic fines, tan to light brown, alluvium. | | - 69.0- | S-20 | 9-11-14-17 | 33 | 2.0 | 100 | | | | |
| | | | a-1-b / gp | - 71.0- | | | | | | | | | |
| -60 - | | | | | S-21 | 32-33-50/.4' | 111 | 1.4 | 100 | | | | A |



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<u>NOTE</u>: N values and all graphical plots are for information only.

| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ 0.5ft) | N ₆₀ RQD % | REC (ft.) | REC (%) | ◇ RQD % ◇ ○ Soil/Rock Rec.% △ SPT (N₆₀) ▲ 10 20 30 40 |
|-------|---------|---|------------------|-----------------|---------------|-------------------------------------|---------------------------------|--------------|------------|---|
| | | 75.4'/El61.4 | | | | | | | | |
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| DEPARTMENT OF TRANSPORTATION |

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|-------------|---|-----------------------|------------------|---------|---------------|--------------------------|-----------------|--------------|----------|----------------------|----------------|---------------------|
| Boring W | H-02 ECMS | | | | | | / | III O | NWE | A | 7 | |
| District: _ | County: Philadelphia | Drilling Start: _07 | 7/25/201 | 7 12:5 | 8 pm | | H | T RI | GISTER | ED | A | |
| SR | Section | Drilling Complet | e: <u>07/26</u> | 2017 | 11:55 | i am | | PRO | FESSI | ONAL A | FA | |
| Baseline: | FDC Site - Port Authority | Grouting Comple | ete: <u>08/0</u> | 1/201 | 7 2:40 |) pm | | DON | 1 hu | Lill | tel | 1 |
| Sta | Offset | Rig: Acker XLS | Track Rig | g | | | | 19 | | 9/21/1 | 17 | |
| Segment | Offset | Hammer Type: | Automat | ic | | | H-1 | K/1 | NGINE | | | |
| Coordinat | | | | | | | Ĥ | A A | -053530 | | ×J) | |
| | Long | Assumed 0.8 | Me | easured | | | | | SYL | | | |
| 219294. | 3170 E 2695829.6000 N | Hammer Calibra | | | | | PG/PE | Seal, S | ignature | e and Dat | te | |
| Ground E | lev. <u>13.9 ft.</u> vel Elev./Elapsed Time: | Hole Type: | | | | F | inal Lo | og Ch | ecke | d and | naaA | roved |
| Vater Lev | vel Elev./Elapsed Time: | Casing Type: <u>H</u> | <u>SA/FJC -</u> | Spun | | B | | | | lson | | |
| | 0.1 ft. Elapsed 0.0 hr. | | | | | <u>20.0 π.</u> Γ |)ate: _ | | | | | |
| | 3.9 ft Elapsed _24.0 hr | | | | | | | Lab T | esting | Perfor | med | |
| | Bary B. | | | | | | | on Sa | mple | | | - l |
| Company | Allied Well Drilling | Inspector Cert. N | lo. <u>410-</u> | 17 | | | plots | are fo | r infor | nd all gi rmation | i only. | ai |
| . <u>⊇</u> | | | | 빅ェ | щ | BLOW | N ₆₀ | | | \$ | RQD | % 🛇 |
| ELEV. | MATERIAL DESCR COMMENTS - OBSER | | AASHTO / USCS | | SAMPLE No. | COUNTS (Blows/ | RQD | REC (ft.) | REC (%) | ● Soil/ | | |
| GR E | | VALIONO | , 0000 | SA | SA | 0.5ft) | % | (11.) | (/0) | ▲ S | SPT (N 20 3 | J ₆₀) ▲ |
| | | | | | | | | | | | | |
| | | 0.3'/El. 13.6/ | | | | | | | | | | |
| | Subbase. | | | - 1.0 - | | | | | | 1 ! ! ! | | |
| | | 1.0'/El. 12.9/ | | | S-1 | 9-8 | 11 | 0.8 | 80 | | | |
| | Coarse SAND , trace Gravel, | loose, moist, | a-3 / | - 2.0 - | | | | | | [i † i | İİ | i i₽ |
| | homogeneous, poorly grade | d, sub-rounded, | sp | | | | | | | | | |
| | non-plastic, light brown, fill. | | | | S-2 | 6-4-4-6 | 11 | 1.2 | 60 | | 11 | . / . . / . |
| | 2 | 3.7'/El. 10.2 | | | | | | | | | | 1/1 ;/ ; ; ; |
| 10 | SLAG, ASPHALT MILLINGS | | | - 4.0 - | | | | | | ¦ ∱ ¦ | | |
| | | 4.0'/EI. 9.9/ | | | | 4101 | | | | ! /: ! | | N I |
| | SAND and SILT, very loose | | | | S-3 | 4-1-2-1 Pen=0.50 ts | f ⁴ | 1.5 | 75 | | ···!··!··! | !!. \ |
| | lensed, well graded, sub-rou fines, dark gray to black, allu | inded, low plastic | | | | | | | | <u> </u> | İİ | i A i |
| | - clay and silt seams from 4. | 2' to 4.5' and 7.5' | | - 6.0 - | | | | | | :∦ : : | | Q |
| • • | to 8.0'. | | | | | | | | | i i i | įį | i i N |
| | | | a-2-4 | | S-4 | 1-1-1-1 Pen=0.25 ts | f ³ | 2.0 | 100 | | | |
| | - pocket penetrometer readi | ngs are from clay | / sm | | | | | | | | | |
| | seams. | | | - 8.0 - | | | | | | ≜ | | |
| • • | | | | | | | | | | | | |
| 5 - | • | | | | S-5 | WOH-2-5-7 Pen=0.25 ts | f 9 | 0.3 | 15 | <u>\</u> i i | 11/ | Í Í |
| | | | | | | | | | | | | |
| | | | | - 10.0- | | | | | | | ··· | - - |
| | • | 10.8'/EI. 3.1 | | | | | | | | ` | N. I | |
| | CLAY and SILT, some Sand | | | | S-6 | 4-4-5-5 Pen=0.25 ts | f 12 | 1.8 | 90 | | ÌN, | |
| 0_0 | homogeneous, poorly grade | d, rounded, | | | | | | | | | | |
| | medium plastic fines, dark g | ray to black, | | - 12.0- | | | | | | | | ! ! `\ |
| | alluvium. | | a-6 / | | | | | | | <u>i</u> i i | İİ | İİİ |
| | | | | | S-7 | 3-4-6-7 Pen=0.25 ts | 1 3 | 2.0 | 100 | | | |
| | 0 | | | | | | 1 | | | | | |
| 0 - 0 0 | 0 | 14.0'/EI0.1 | | - 14.0- | | | | | | | | |
| 0 0 | 0 | | a-3 / | | | | | | | T | | |
| 00 | 0 | | sp | | | | | | | <u> ; ; ;</u> | | |
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Boring WH-02

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Sta. _____ Offset _____

Sheet <u>2</u> of <u>4</u>

<u>NOTE</u>: N values and all graphical plots are for information only.

Lab Testing Performed on Sample

| S.GPJ | U | | | 111 | 111 | BLOW | N | | | ♦ RQD | % ♦ |
|---------------------------|---------|---|---------------------|-----------------|---------------|--------------------------------|---------------------------------|--------------|------------|--|--|
| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | COUNTS (Blows/ 0.5ft) | N ₆₀ RQD % | REC (ft.) | REC (%) | Soil/Rock ▲ SPT (1) 10 | Rec.% ⊙ |
| HOUSE/PORT | | SAND and GRAVEL , some Silt, loose, wet, heterogeneous, well graded, angular, non-plastic, dark gray, alluvium, | | - 16.0- | S-8 | WOH-2-4-2 | 8 | 1.5 | 75 | | |
| | | - tan, coarse gravel-sized pieces of angular, very hard, quartz frequent in samples S-8 and S-9. (Layer continued from the previous page.) | a-3 / sp | | S-9 | 2-1-1-1 | 3 | 1.8 | 90 | | · · · · · · · · · · · · · · · · · · · |
| | | 18.9'/El5.0 | | | S-10 | 2-2-3-4 | 7 | 1.6 | 80 | | |
| | | CLAY and SILT , trace Sand, trace Gravel, soft, wet, homogeneous, poorly graded, rounded, high plastic fines, dark gray, alluvium, | | - 20.0- | 3-10 | Pen=0.50 tsf | | 1.0 | 00 | | |
| | | Class. on jar samples collected from S-10B to S-11 A-7-5(31)/MH N.M.C.=57.7%. | | | | | | | | | |
| - (M) MUNICIPALIM1700 | | | A-7-5 / MH | - 24.0- | · S-11 | WOH-WOH- WOH-2 | 0 | 2.0 | 100 | | |
| 0T - 9/21/17 08:55 - P:\6 | | | | - 26.0- | | Pen=0.25 tsf | | | | | |
| | | | | | | | | | | | |
| | | 30.2'/El16.3 | | | S-12 | 3-4-4-6 Pen=0.25 tsf | 11 | 1.2 | 60 | | |
| - PENNDOI_GINI_ | | SAND , some Gravel, trace Silt, medium dense to very dense, wet, heterogeneous, poorly graded, sub-rounded, non-plastic, red gray, alluvium. | A 4 h | - 31.0- | | | | | | | $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ |
| | | | A-1-b / SW-SM | | | | | | | | |
| DENNDOT | | | | 54.0 | | | | | | | |



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Sheet <u>3</u> of <u>4</u>

<u>NOTE</u>: N values and all graphical plots are for information only.

Lab Testing Performed on Sample

| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ | N ₆₀ RQD | REC (ft.) | REC (%) | ◇ RQD % Soil/Rock Re 20 40 60 | |
|-------|---|--|---------------------|---------------------|---------------|---------------------------|----------------------------|--------------|------------|----------------------------------|-----------|
| Ξ | GR/ | COMMENTS - OBSERVATIONS | / 0303 | SAI | SAI | 0.5ft) | % | (11.) | (70) | ▲ SPT (N ₆₀ |) ▲ 40 |
| | | SAND , some Gravel, trace Silt, medium dense to very dense, wet, heterogeneous, poorly graded, sub-rounded, non-plastic, red gray, alluvium. <i>(Layer continued from the previous page.)</i> | | - 36.0- | S-13 | 7-7-10-11 | 23 | 1.3 | 65 | | |
| -25 - | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | - tan, coarse gravel-sized pieces of angular, very hard, quartz frequent in samples S-13, S-14, and S-15 | | - 39.0 <i>-</i> | - S-14 | 7-8-10-13 | 24 | 1.4 | 70 | | |
| | | Class. on jar samples collected from S-14 to S-16 A-1-b/SW-SM N.M.C.=13.4%. | | - 41.0- | | | | | | | |
| -30 - | | | A-1-b / SW-SM | - 44.0- | S-15 | 6-7-8-18 | 20 | 1.5 | 75 | | |
| -35 - | | - brown, gray, white, green, red and purple, coarse gravel, subrounded to rounded, | | | | | | | | | |
| - | | medium hard to very hard with frequent minerals in alluvial deposit in bottom 6" of S-16. | | - 51.0- | S-16 | 17-35-49-42 | 112 | 1.9 | 95 | | |
| -40 - | | 54.0'/El40.1 | A-1-a | - 54.0- | | | | | | | |
| | 0 0 0 | | / SP | | | | | | | | |



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Sheet <u>4</u> of <u>4</u>

<u>NOTE</u>: N values and all graphical plots are for information only.

| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ 0.5ft) | N ₆₀ RQD % | REC (ft.) | REC (%) | ▲ SP1 (N ₆₀) ▲ |
|-------|---------|--|------------------|-----------------|---------------|-------------------------------------|---------------------------------|--------------|------------|----------------------------|
| | | GRAVEL and SAND , trace Silt, medium dense to dense, wet, heterogeneous, poorly graded, angular, non-plastic, brown, alluvium, <i>Class. on jar samples collected from S-17 to</i> <i>S-18</i> <i>A-1-a/SP</i> | | - 56.0- | S-17 | 5-12-12-13 | 32 | 1.5 | 75 | |
| 45 | | N.M.C.=17.6%. (Layer continued from the previous page.) - low recovery in S-18 due to coarse gravel in shoe and broken basket. | A-1-a / SP | - 59.0- | - S-18 | 6-6-7-9 | 17 | 1.0 | 50 | |
| | | | | - 61.0- | - | | | | | |
| 50 | | 64.0'/El50.1 GRAVEL and SAND, little Clay, medium | | | - | | | | | |
| · - | | dense to dense, wet, heterogeneous, poorly graded, sub-angular to angular, medium plastic fines, tan to light brown, alluvium, - heaving sand and gravel clogged tri-cone bit and AWS rod, required tool cleaning and hole reaming. | a-1-b / gp | - 66.0- | S-19 | 4-7-12-16 | 25 | 1.3 | 65 | |
| 55 | | 71.0'/El57.1 | | - 69.0- | - S-20 | 3-5-18-49 | 31 | 2.0 | 100 | |
| | | Abandoned hole due to heaving sands. Ran casing advancer down to 74.0' twice; the first time it caved at 48.0' and the second time it caved at 54.0' when trying to sample. Bottom of boring. | | | - | | | 1 | 1 | |
| 60 | | | | | - | | | | | |

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| DEPARTMENT OF TRANSPORTATION |

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| Boring W | H-03 ECMS | _ | | | | | | III O | NWE | ALT |
| District: _ | County: Philadelphia | _ Drilling Start: <u>07</u> | 7/31/201 | 7 2:05 | pm | | <u> </u> | T RI | EGISTER | |
| | Section | | | | | | | PRO | FESSI | ONAL |
| Baseline: | FDC Site - Port Authority | _ Grouting Comple | ete: <u>08/0</u> | 2/201 | 7 11:4 | 15 am | | nite | 1/K | filleta |
| Sta | Offset | _ Rig: <u>Acker XLS</u> | Track Ri | g | | | | | | 9/21/17 |
| Segment . | Offset | _ Hammer Type: _ | Automat | ic | | | H- | K 1 - | NGINEE - 053530 | |
| Coordinat | es: | SPT Hammer Effi | ciency: | | | | Ĥ | | -000000 | S-EP |
| | Long | Assumed0.8 | | | | | | | SY L | TITLE |
| | 6650 E 2696277.2210 N | | | | | | PG/PE | Seal, S | ignature | e and Date |
| | lev. <u>13.1 ft.</u> | | | 0 | | I | - inal Lo | og Ch | ecke | d and Approved |
| | vel Elev./Elapsed Time: | | | | | | | | | lson |
| | <u>B.7 ft.</u> Elapsed <u>0.0 hr.</u> | | | | | <u>30.0 ft.</u> | , Date: _ | | | |
| | 0 ft. Elapsed <u>23.0 hr.</u> | | | | | | | Lab T | esting | Performed |
| | Bary B. | | | | | | NOT | on Sa | | nd all graphical |
| Company | Allied Well Drilling | Inspector Cert. N | lo. <u>410-</u> | 17 | | | plots | are fo | r infor | mation only. |
| <u> </u> | | | | Щт | щ | BLOW | N ₆₀ | | | \diamond RQD % \diamond |
| ELEV. GRAPHIC | MATERIAL DESC COMMENTS - OBSE | | AASHTO / USCS | MPL | SAMPLE No. | COUNTS (Blows/ | RQD | REC (ft.) | REC (%) | Soil/Rock Rec. % 20 40 60 80 |
| GR/ EI | COMMENTS - OBSE | RVATIONS | / 0505 | SAI | SAI | 0.5ft) | % | (11.) | (%) | ▲ SPT (N ₆₀) ▲ |
| | | | | | | | | | | |
| | | 0.4'/El. 12.8 | | | | | | | | |
| | Subbase, coarse cobble-si | zed limestone | | - 1.0 - | | | | | | |
| 0 0 | o] \pieces. | | a-2-4 | | S-1 | 16-12 | 16 | 1.0 | 100 | |
| -00 | • | 1.0'/El. 12.1 | / sm | - 2.0 - | | | | | | ∱ |
| 00 | SAND and GRAVEL, some | Silt, medium | | | | 0 5 7 40 | | | | |
| | o dense, wet, heterogeneous | , well graded, | 0.1 | | S-2 | 8-5-7-10 Pen=3.00 ts | of 16 | 1.0 | 50 | |
| | sub-rounded to sub-angula fines, brown and red black, | | a-6 / | | | | | | | |
| | | 3.0'/EI. 10.1/ _[| | - 4.0 - | | | | | | ▲ ∲ |
| | CLAY and SILT, some Gra | vel. verv stiff. | | | | | | | | |
| | wet, heterogeneous, poorly | graded, | | | S-3 | 7-4-3-3 | 9 | 0.3 | 15 | |
| | sub-rounded to sub-angula | r, medium plastic | | | | | | | | |
| ••• | - trace pyrite in S-2. | ay, III, | | - 6.0 - | | | | | | |
| | | 4.0'/El. 9.1 | | | | | | | | |
| V | SAND and SILT, some Gra | vel, loose, wet, | | | S-4 | 2-1-2-3 | 4 | 2.0 | 100 | |
| | lensed, well graded, rounde | | | | | Pen=0.25 ts | sf . | | | |
| | plastic fines, dark brown to | DIACK, TIII. | | - 8.0 - | | | | | | |
| - 5 - | | | a-2-4 / sm | 0.0 | | | | | | |
| | | | | | 0.5 | 1-1-2-1 | 4 | 20 | 100 | |
| | | | | Г ⁻ | S-5 | Pen=0.25 ts | sf ⁴ | 2.0 | 100 | |
| | | | | | | | | | | |
| | - tar odor in S-5 and S-6. | | | - 10.0- | 1 | | | | | |
| ••• | | | | | | 1-1-1-1 | | | | |
| | | | | | S-6 | Pen=0.25 ts | sf ³ | 1.7 | 85 | |
| | | | | | | | | | | |
| | | 12.5'/El. 0.6 | | - 12.0- | | | | | | • • • • • • • • • • • • |
| | | 12.3/EI. U.0 | | | | | | | | |
| - 0 - | | | | | S-7 | WOH-1-8-8 | 3 12 | 0.6 | 30 | |
| 0°0 | 0 | | A-2-4 | | | | | | | |
| | 0 | | / SM | - 14.0- | | | | | | |
| 0 0 | 0 | | | | | | | | | |
| | 0 | | | | | | | | | liilii`xiii |



Boring WH-03

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Sheet <u>2</u> of <u>5</u>

<u>NOTE</u>: N values and all graphical plots are for information only.

Lab Testing Performed on Sample

| | OHIC | MATERIAL DESCRIPTION | AASHTO | PLE TH | PLE 0. | BLOW COUNTS | N ₆₀ | REC | REC | | RQD % |
|--|---------|---|----------------|-----------------|---------------|-------------------------|-----------------|-------|------|-----|--|
| ELEV. | GRAPHIC | COMMENTS - OBSERVATIONS | / USCS | SAMPLE DEPTH | SAMPLE No. | (Blows/ 0.5ft) | RQD % | (ft.) | (70) | ▲ S | $\begin{array}{ccc} 40 & 60 & 80 \\ \hline & & \\ 5 \text{PT} (\text{N}_{60}) \\ 20 & 30 & 40 \end{array}$ |
| | | SAND , little Silt, trace Gravel, medium dense, wet, heterogeneous, poorly graded, sub-rounded to sub-angular, non-plastic, | | - 16.0- | S-8 | 2-3-7-7 | 13 | 1.6 | 80 | | |
| | | brown, fill, Class. on jar samples collected from S-8 to S-9 A-2-4(0)/SM | A-2-4 / SM | | S-9 | 5-4-3-3 | 9 | 2.0 | 100 | | |
| 5 | | N.M.C.=19.8%. (Layer continued from the previous page.) 19.2'/El6.1 | | - 18.0- | S-10 | 2-2-2-3 Pen=1.00 tsf | 5 | 2.0 | 100 | | |
| | | CLAY and SILT , trace Sand, stiff, wet, homogeneous, poorly graded, rounded, medium plastic fines, dark gray, fill. | | - 20.0- | | | | | | | |
| | | | | | | | | | | | |
| 10 | | | a-6 / cl | | | | | | | | |
| | | - organics/weeds in sample from 25.2' to 26.0'. | | - 24.0- | S-11 | WOH-2-2-4 | 5 | 2.0 | 100 | | |
| | | 26.0'/EI12.9 | | - 26.0- | | Pen=2.00 tsf | | | | | |
| 5 - 5 - | | SAND , trace Silt, trace Gravel, medium dense to dense, wet, heterogeneous, poorly graded, sub-rounded to angular, non-plastic, brown, alluvium, | | | | | | | | | |
| | | Class. on jar samples collected from S-12 to S-13 A-3/SP-SM N.M.C.=22.3%. | | | | | | | | | |
| 20 | | N.W.O22.376. | A-3 / SP-SM | | S-12 | 3-4-5-5 | 12 | 1.6 | 80 | | |
| | | | | - 31.0- | | | | | | | |
| 20 | | | | | | | | | | | |
| | | | | - 34.0- | | | | | | | |



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<u>NOTE</u>: N values and all graphical plots are for information only.

| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ | N ₆₀ RQD | REC (ft.) | REC (%) | |
|--------|---------|--|------------------|------------------------|-----------------------|---------------------------|----------------------------|--------------|------------|---|
| ш - | | SAND , trace Silt, trace Gravel, medium dense to dense, wet, heterogeneous, poorly | | - 36.0- | ທີ S-13 | 0.5ft) 4-7-5-6 | % 16 | 1.9 | 95 | ▲ SPT (N ₆₀) ▲ 10 20 30 40 |
| -25 - | | graded, sub-rounded to angular, non-plastic, brown, alluvium, <i>Class. on jar samples collected from S-12 to</i> <i>S-13</i> <i>A-3/SP-SM</i> <i>N.M.C.=22.3%.</i> <i>(Layer continued from the previous page.)</i> | | | | | | | | |
| - | | | A-3 / SP-SM | - 39.0- - 41.0- | - S-14 | 6-7-19-24 | 35 | 1.4 | 70 | |
| -30 - | | 44.0'/EI30.9 | | | | | | | | |
| - | | GRAVEL and SAND , trace Clay, dense to very dense, wet, heterogeneous, poorly graded, sub-angular to angular, medium plastic fines, brown, alluvium, - gravel stuck in S-15 shoe. | | | · S-15 | 10-14-11-9 | 33 | 0.1 | 5 | |
| -35 - | | | | | | | | | | |
| - | | | a-1-b / gp | - 49.0- | · S-16 | 20-40-46- 50/.4' | >115 | 1.8 | 95 | |
| - | | | | _ 50.9_ | | | | | | |
| -40 - | | 54.0'/El40.9 | | - 54.0- | | | | | | |
| | 0 0 0 | | a-3 / sp | | | | | | | |



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<u>NOTE</u>: N values and all graphical plots are for information only.

Lab Testing Performed on Sample

| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ | N ₆₀ RQD | REC (ft.) | REC (%) | ⊙ Soil 20 | /Rock | $0 \% \diamondsuit$ | .% • |
|-------|---------|--|------------------|-----------------|---------------|---------------------------|----------------------------|--------------|------------|--------------|-------|--|------|
| | | SAND and GRAVEL , little Silt, dense, wet, heterogeneous, gap graded, angular, non-plastic, brown, alluvium. <i>(Layer continued from the previous page.)</i> | a-3 / sp | - 56.0- | | 0.5ft) 19-20-16-17 | % 48 | 2.0 | 100 | | | (N ₆₀) 4 30 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | |
| 45 | | 59.0'/El45.9 GRAVEL and SAND, trace Silt, dense to | | | - | | | | | | | | |
| | | very dense, wet, heterogeneous, poorly graded, non-plastic, brown, alluvium. | | - 61.0- | • S-18 | 10-12-12-11 | 32 | 2.0 | 100 | | | | |
| 50 | | | | | - | | | | | | | | |
| | | | | - 64.0 - | • S-19 | 13-20-22-33 | 56 | 1.0 | 50 | | | | |
| · · | | | a-1-b / gp | | - | | | | | | | | |
| 55 | | | | - 69.0- | S-20 | 9-26-50/.4' | 101 | 1.4 | 100 | | | | |
| | | | | 70.4 | | | | | | | | | |
| 60 | | 74.0'/El60.9 | | | - | | | | | | | | |
| | | | A-7-6 / CL | - 74.0- | | 9-12-13-16 | | | | | | | |



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<u>NOTE</u>: N values and all graphical plots are for information only.

| ELEV. | GRAPHIC | COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ 0.5ft) | N ₆₀ RQD % | REC (ft.) | (70) | |
|--|---------|---|------------------|-----------------|---------------|-------------------------------------|-----------------------------|--------------|------|---------------------|
| | | CLAY and SILT , trace Sand, trace Gravel, stiff, wet, heterogeneous, poorly graded, high | A-7-6 / CL | | S-21 | Pen=1.50 tsf | 33 | 2.0 | 100 | |
| PENNDOT ENGINEER'S LOG - PENNDOT_GINT_VERSION_12.2.3_9-21-2016.GDT - 9/21/17 08:55 - P:/6 - (M) MUNICIPALIM17001-13 PRPA PORT DEVELOPMENT/GEOTECHUDRILLING/LOGS/WAREHOUSE/PORT AUTH LOGS.GPJ - | | stiff, wet, heterogeneous, poorly graded, high plastic fines, red and white, alluvium, Class. on jar samples collected from S-21 A-7-6(30)/CL N.M.C.=22.2%. (Layer continued from the previous page.) 76.0'/EL62.9 Bottom of boring. | | | | | | | | |
| | - | | | | | | | | | |



| Boring WH-04 ECMS District: County: Philadelphia SR Section Baseline: FDC Site - Port Authority Sta Offset Segment Offset Coordinates: Lat Long 218778.3140 E 2695791.4020 N Ground Elev12.9 ft. | Drilling Complete Grouting Comple Rig: <u>Acker XLS</u> Hammer Type: <u>A</u> | e: <u>07/27</u> , te: <u>08/0</u> <u>Frack Rig</u> Automat ciency: M ion Date | /2017 1/201 g ic easurec e: | 4:10 7 3:48 | <u>5 pm</u> | PG/PE | PROI | N W E EGISTER FESSI MGINEE S Y L S Y L | 0NAL 1 9/21/17 FR |
|--|--|---|--|-------------------|-------------------------------------|---------------------------------|--|---|---|
| Water Level Elev./Elapsed Time: ↓ Initial <u>-4.0 ft.</u> Elapsed <u>0.0 hr.</u> ↓ Final <u>-0.1 ft.</u> Elapsed <u>24.0 hr.</u> Driller: <u>Gary B.</u> Company: <u>Allied Well Drilling</u> | Casing Type: <u>HS</u> Casing I.D.: <u>3.25</u> Rock Core Metho Inspector: <u>Jeren</u> | A/FJC - in_Cas od: ny Booze | Spun ing De er | epth: | 35.0 ft. | By: <u>Ca</u> Date: <u></u> | Arrie N 9/21/2 Lab T on Sa E: N va | licho 2017 esting mple lues a | Performed nd all graphical rmation only. |
| OI OI OI MATERIAL DESCR OI MATERIAL DESCR OI COMMENTS - OBSER OI OI | | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ 0.5ft) | N ₆₀ RQD % | REC (ft.) | REC (%) | ◇ RQD % ◇ ③ Soil/Rock Rec.% ⊙ △ SPT (N₆₀) ▲ 10 20 30 40 |
| Sta. Offset Segment Offset Coordinates: Lat. Lat. Long. 218778.3140 E 2695791.4020 N Ground Elev. 12.9 ft. Water Level Elev./Elapsed Time: ♀ Initial -4.0 ft. Elapsed On hr. ♥ Final -0.1 ft. Driller: Gary B. Company: Allied Well Drilling MATERIAL DESCR COMMENTS - OBSER BITUMINOUS CONCRETE. Subbase. ● ● ● ● ● ● ● ● BITUMINOUS CONCRETE. Subbase. ● ● ● ● ● ● ● ● ● ● ○ ● ● ● BITUMINOUS CONCRETE. SLAG, ASPHALT MILLINGS fill. ● | gap graded, ay, fill. 4.5'/El. 8.4 5, AND TAR , | a-1-b /gp | - 1.0 - - 2.0 - - 4.0 - | S-1 S-2 S-3 | 19-12 5-6-5-6 8-5-6-8 | 16 15 15 | 0.2 | 20 50 80 | |
| GRAVEL and SAND, some S to medium dense, moist, hei well graded, sub-angular, no gray to black, fill, - brick, wood, and asphalt from - piece of wood stuck in S-6 | terogeneous, on-plastic, dark | a-2-4 / gm | - 6.0 - - 8.0 - | S-4 | 9-10-9-9 WOH-WOH 2-2 | 25 | 1.6 | 80 50 | |
| - piece of wood stuck in S-6 | shoe. 12.0'/El. 0.9 | | - 10.0- | S-6 | 2-WOH- WOH-3 | 0 | 0.3 | 15 | |
| Coarse SAND , little Silt, little to medium dense, wet, homo graded, sub-rounded to sub- non-plastic, dark gray, alluvi | ogeneous, poorly -angular, | a-3 / sp | | · S-7 | 4-5-7-5 | 16 | 2.0 | 100 | |



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<u>NOTE</u>: N values and all graphical plots are for information only.

Lab Testing Performed on Sample

| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ 0.5ft) | N ₆₀ RQD % | REC (ft.) | REC (%) | ⊙ Soil/I | RQD % | |
|--|---------|--|------------------|----------------------------|---------------|-------------------------------------|---------------------------------|--------------|------------|----------|-------|--|
| | | | a-3 / sp | - 16.0- | S-8 | 2-2-2-2 | 5 | 0.8 | 40 | | | |
| ⊻ 5 - | | 16.5'/El3.6 CLAY and SILT, trace Sand, very soft to soft, wet, homogeneous, poorly graded, rounded, medium plastic fines, dark gray, alluvium. | | | S-9 | WOH-WOH- WOH-WOH Pen=0.25 tsf | 0 | 1.7 | 85 | | | |
| - | | | | - 18.0 | | 2-1-1-2 Pen=0.50 tsf | 3 | 2.0 | 100 | | | |
| - <u>-</u> -5 - 5 - 10 - 10 - | | | | - 20.0 - | | | | | | | | |
| 10 - - | | | a-6 / cl | | | | | | | | | |
| - | | | | | - 26.0- | S-11 | WOH-2-2-4 Pen=0.25 tsf | 5 | 1.2 | 60 | | |
| - 15 - | | | | | | | | | | | | |
| - - 20 - | | 29.0'/El16.1 SAND and GRAVEL, trace Silt, medium dense, wet, heterogeneous, gap graded, sub-rounded, non-plastic, red gray, alluvium. | | - 29.0- | 6.40 | 5400 | 10 | 1.0 | 50 | | | |
| - | | sub-rounded, non-plastic, red gray, alluvium. | | - 31.0- | S-12 | 5-4-6-6 | 13 | 1.0 | 50 | | | |
| - 20 - | | | a-3 / sp | | | | | | | | | |
| - | | | | - 34.0- | | | | | | | | |



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<u>NOTE</u>: N values and all graphical plots are for information only.

Lab Testing Performed on Sample

| ELEV. GRAPHIC | MATERIAL DESCRIPTION | AASHTO | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS | N ₆₀ | REC | REC | ◇ RC ③ Soil/Ro 20 40 | QD % | | |
|------------------|--|---------------------|-----------------|---------------|-------------------|-----------------|-------|-----|----------------------------|----------------------------|--|--|
| EL GRA | COMMENTS - OBSERVATIONS | / USCS | SAN DEF | SAN | (Blows/ 0.5ft) | RQD % | (ft.) | (%) | | ▲ SPT (N ₆₀) ▲ | | |
| | SAND and GRAVEL , trace Silt, medium dense, wet, heterogeneous, gap graded, sub-rounded, non-plastic, red gray, alluvium. (Layer continued from the previous page.) | | - 36.0- | S-13 | 6-8-7-9 | 20 | 1.8 | 90 | | | | |
| | | a-3 / | | | | | | | | | | |
| | | sp | | S-14 | 12-14-7-16 | 28 | 1.6 | 80 | | | | |
| | 44.0'/EI31.1 | | | | | | | | | | | |
| | GRAVEL and SAND , some Clay, dense, wet, heterogeneous, well graded, sub-angular to angular, medium plastic fines, gray to brown, alluvium. | | | S-15 | 10-12-11-13 | 31 | 1.8 | 90 | | | | |
| -35 | | a-2-6 / gc | | | | | | | | | | |
| | 49.0'/EI36.1 | | - 49.0- | | | | | | | | | |
| | GRAVEL , some Sand, trace Silt, medium dense to very dense, wet, heterogeneous, poorly graded, angular, non-plastic, brown, alluvium, | | | S-16 | 7-19-47-47 | 88 | 2.0 | 100 | | | | |
| | Class. on jar samples collected from S-17 to S-18 A-1-a/SW-SM N.M.C.=17.2%. | A-1-a / SW-SM | - 51.0- | | | | | | | | | |
| | | | | | | | | | | | | |



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<u>NOTE</u>: N values and all graphical plots are for information only.

| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS | N ₆₀ RQD | REC | REC | ♦ ⊙ Soil | RQD /Rock | | |
|-------|---------|--|---------------------|-----------------|---------------|----------------------------------|----------------------------|-------|-----|-------------|--------------|-------------------------|----|
| Ξ | GR | GOIVIVILINTS - ODSERVATIONS | 10505 | SAI | SAI | (Blows/ 0.5ft) | % | (ft.) | (%) | | SPT (I | N ₆₀) 🖌 | |
| - | | GRAVEL , some Sand, trace Silt, medium dense to very dense, wet, heterogeneous, poorly graded, angular, non-plastic, brown, alluvium, | | - 56.0- | S-17 | 6-9-18-16 | 36 | 1.2 | 60 | | | + /! !/! !/ ! | |
| -45 - | | Class. on jar samples collected from S-17 to S-18 A-1-a/SW-SM N.M.C.=17.2%. (Layer continued from the previous page.) | | | | | | | | | | | |
| - | | | A-1-a / SW-SM | - 61.0- | · S-18 | 14-11-7-8 | 24 | 2.0 | 100 | | | | |
| -50 - | | | | | | | | | | | | | |
| - | | 65.0'/EI52.1 CLAY and SILT, some Sand, very stiff, wet, | | - 64.0- | S-19 | 6-7-10-14 Pen=3.50 tsf | 23 | 2.0 | 100 | | | | |
| - | | homogeneous, poorly graded, rounded, medium plastic fines, gray to tan, alluvium. | a-6 / cl | - 66.0- | | | | | | | | | |
| -55 | | 69.0'/El56.1 | | - 69.0- | | | | | | | | | |
| - | | SAND and SILT , some Clay, very dense, wet, homogeneous, gap graded, sub-rounded to sub-angular, low plastic fines, tan to light brown, alluvium. | | | S-20 | 16-26-32-42 | 77 | 2.0 | 100 | | | | |
| - | | | a-3 / sw | | | | _ | | | | | | |
| -60 | | | | | | | | | | | | | |
| - | | 75.0'/El62.1 | | | | | | | | | | 11 | ľ. |



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|-------|---------|--|------------------|-----------------|---------------|-------------------------------------|---------------------------------|--------------|------|---|
| | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ 0.5ft) | N ₆₀ RQD % | REC (ft.) | (70) | ◇ RQD % ◇ ③ Soil/Rock Rec.% ⊙ ▲ SPT (N₆₀) ▲ 10 20 30 40 |
| | | CLAY and SILT, little Sand, stiff, wet, homogeneous, poorly graded, rounded, | a-6 / cl | | S-21 | 18-12-9-16 | 28 | 2.0 | 100 | |
| | | (Layer continued from the previous page.) 76.0'/El63.1 | | | | | | | | |
| 65 - | | <i>Hole collapsed between 10.0' and 11.0' as noticed on 8/1/17 when attempting to grout.</i> Bottom of boring. | | | | | | | | |
| | - | | | | | | | | | |
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| N (M) | | | | | - | | | | | |
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| 80 - | | | | | | | | | | |
| | | | | | | | | | | |
| | | | | | 7 – | | | | | |



| District: SR Baseline: FC | -05 ECMS _ County: Philadelphia Section | Drilling Complete Grouting Complete Rig: <u>Acker XLS</u> Hammer Type: <u>A</u> SPT Hammer Effi Assumed <u>0.8</u> Hammer Calibrat Hole Type: <u>Casing Type</u> : <u>HS</u> Casing I.D.: <u>3.25</u> Rock Core Metho Inspector: <u>Carm</u> | e: 07/30. ete: 08/0 <u>Frack Rig</u> <u>Automat</u> ciency: <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> <u>Case</u> | 2/2017 2/201 c c easured e: Spun ing De o | 12:46 7 10:3 | 30 am F F B D | inal Lo y: <u>Ca</u> ate: _ NOTI | Seal, S og Chi arrie N 9/21/2 Lab Ti on Sa E: N va | eckeo <u>lichol</u> 2017 esting mple lues ar | and Date | |
|--|--|--|--|---|--------------------------|--|---|--|---|--|---------|
| ELEV. GRAPHIC | MATERIAL DESCR COMMENTS - OBSER | | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ 0.5ft) | N ₆₀ RQD % | REC (ft.) | REC (%) | ◇ RQD % ⊘ Soil/Rock R0 ▲ SPT (N₆₀ 10 20 30 | ec.% ⊙ |
| StaS | BITUMINOUS CONCRETE. Subbase (pulled from hole v SAND and CLAY, medium d heterogeneous, gap graded, fines, dark gray, fill, - brick, mica and asphalt mil - burnt shale waste from 4.0 SILT and CLAY, some Sand soft, wet, heterogeneous, por rounded to sub-angular, low | <u>1.0'/El. 12.1</u> / lense, moist, , medium plastic <i>llings in S-2</i> l'-6.0'. 7.0'/El. 6.1 l, trace Gravel, porly graded, | a-2-4 / sm a-4 / ml | - 1.0 - - 2.0 - - 4.0 - - 6.0 - | S-1 S-2 S-3 S-3 | 6-6 5-5-6-10 8-11-12-13 6-6-8-9 | 8 15 31 19 | 1.0 2.0 2.0 2.0 | 100 100 100 100 | | i i i l |
| | black, fill, - burnt shale waste in S-4. SAND and SILT , very loose dense, wet, heterogeneous, sub-angular to sub-rounded black, fill, - tar odor and black liquid th | 8.5'/El. 4.6 to medium poorly graded, , non-plastic, | a-2-4 / sm | - 10.0 - - 12.0 - | S-5 S-6 S-7 | 2-1-2-1 2-8-2-1 1-WOH-1-1 | 4 | 1.0 1.6 0.4 | 50 80 20 | | |



ECMS

Boring WH-05

ENGINEER'S LOG

District: _____ County: <u>Philadelphia</u> SR _____ Section _____

Sta. _____ Offset _____

Sheet <u>2</u> of <u>4</u>

<u>NOTE</u>: N values and all graphical plots are for information only.

Lab Testing Performed on Sample

| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ | N ₆₀ RQD | REC (ft.) | REC (%) | ⊙ Soi | | Rec. 60 8 | % 0 |
|--------------|---------|---|------------------|----------------------------|---------------|---------------------------|----------------------------|--------------|------------|-------|--------------|-----------|------------|
| - | | | - 0.4 | ωu | ഗ S-8 | 0.5ft) | % 1 | 1.2 | 60 | 10 | SPT (1 20 | 30 40 | 0 |
| | | 16.0'/EI2.9 | a-2-4 / sm | - 16.0- | | | | | | | | | |
| 5 - | | CLAY and SILT , trace Sand, soft, wet, homogeneous, poorly graded, rounded, medium plastic fines, gray, alluvium. | | | · S-9 | 1-1-2-2 Pen=0.25 tsf | 4 | 2.0 | 100 | | | | |
| -0 | | | | | · S-10 | 2-2-1-1 Pen=0.25 tsf | 4 | 2.0 | 100 | | | | ! |
| - - 10 | | | a-6 / cl | | | | | | | | | | |
| - | | 25.0'/El11.9 Coarse SAND , little Clay, little Gravel, medium dense, wet, heterogeneous, poorly graded, sub-rounded to sub-angular, medium plastic fines, brown, alluvium. | | - 24.0- - 26.0- | • S-11 | 3-3-4-4 Pen=0.50 tsf | 9 | 2.0 | 100 | | | | |
| 15 - | | | a-3 / sp | - 29.0- | • S-12 | 4-4-5-6 | 12 | 2.0 | 100 | | | | |
| 20 | | | | - 31.0- | | | | | | | | | |
| | | | | | | | | | | | | | : 1 |



Boring WH-05

ENGINEER'S LOG

District: _____ County: Philadelphia

Sheet <u>3</u> of <u>4</u>

<u>NOTE</u>: N values and all graphical plots are for information only.

Lab Testing Performed on Sample

| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ | N ₆₀ RQD | REC (ft.) | REC (%) | ⊙ So 20 | | ck R | lec.% |
|-------|---------|---|------------------|-----------------|---------------|---------------------------|----------------------------|--------------|------------|------------|-------------|-----------------------|-------------------------|
| ш | - | | | ωD | | 0.5ft) | % | | | 1,0 | SP 20 | (N ₆ 30 | ₅₀) ▲ 40 |
| = | | Coarse SAND , little Clay, little Gravel, medium dense, wet, heterogeneous, poorly graded, sub-rounded to sub-angular, medium plastic fines, brown, alluvium. (<i>Layer continued from the previous page.</i>) | | - 36.0- | S-13 | 17-12-8-10 | 27 | 1.6 | 80 | | | | |
| -25 — | | | a-3 / | | | | | | | | | | |
| _ | | | sp | - 41.0- | S-14 | 7-6-7-12 | 17 | 1.7 | 85 | | | | |
| -30 — | | | | | | | | | | | | | |
| - | | 44.0'/EI30.9 | | - 44.0- | | | | | | ļįį | įį | įį | Ni |
| _ | | GRAVEL and SAND , trace Silt, very dense, wet, heterogeneous, poorly graded, sub-angular to angular, low plastic fines, brown, alluvium. | a-1-b | | S-15 | 25-18-24-30 | 56 | 1.7 | 85 | | | | |
| -35 — | | 49.0'/EI35.9 | / gp | | | | | | | | įį | | 1.1 |
| = | | SAND , little Silt, little Gravel, dense to very dense, wet, homogeneous, poorly graded, sub-rounded to sub-angular, non-plastic, light brown to tan, alluvium, | | | S-16 | 15-15-21-31 | 48 | 2.0 | 100 | | | | |
| - | | Class. on jar samples collected from S-17 to S-21 A-2-4(0)/SM N.M.C.=17.3%. | A-2-4 / SM | - 51.0- | | | | | | | | | |
| -40 — | | | | | | | | | | | | | |
| | 0 0 0 | | | | | 25-27-19- | | | | Lii | <u>.i.i</u> | <u>.i.i</u> | <u>.i.i</u> |

ECMS

SR ______ Section _____ Sta. _____ Offset _____



ECMS

Boring WH-05

ENGINEER'S LOG

SR ______ Section _____

Sta. _____ Offset _____

District: _____ County: Philadelphia _____

Sheet <u>4</u> of <u>4</u>

<u>NOTE</u>: N values and all graphical plots are for information only.

Lab Testing Performed on Sample

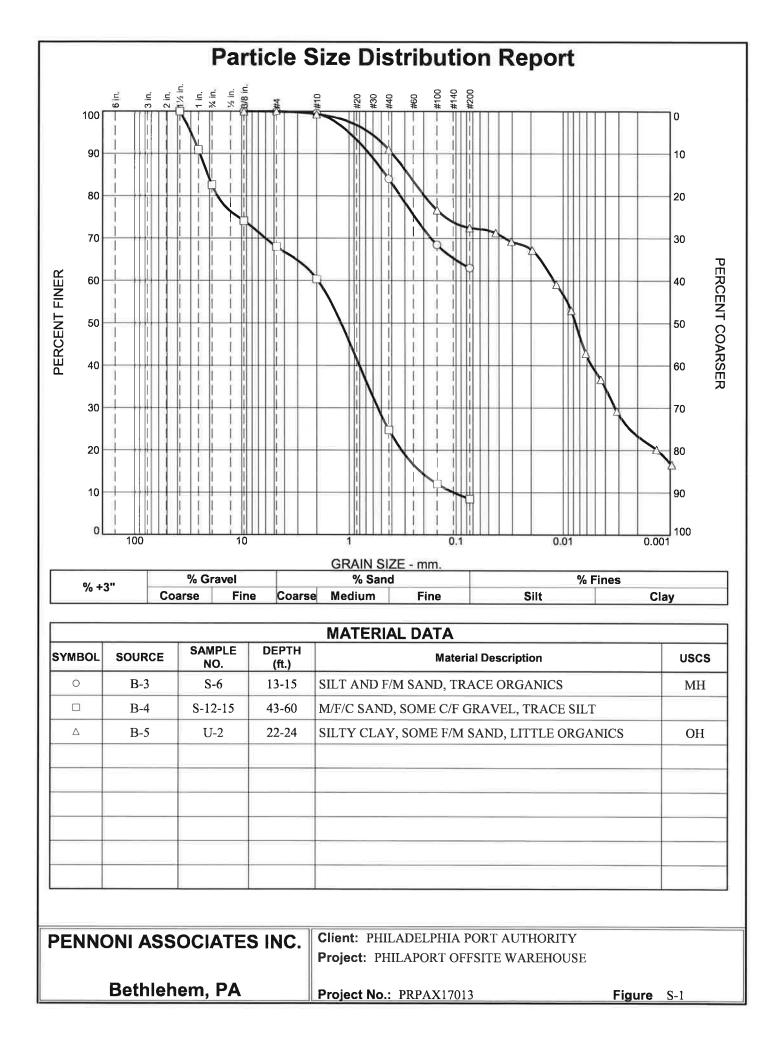
| ELEV. | GRAPHIC | MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS | AASHTO / USCS | SAMPLE DEPTH | SAMPLE No. | BLOW COUNTS (Blows/ | N ₆₀ RQD | REC (ft.) | REC (%) | | oil/F | | | .% • |
|--------------|---------|--|------------------|------------------------------|---------------|---------------------------|----------------------------|--------------|------------|---|-------|---------------|---------------------|------|
| ш | RO | | , 0000 | PI | SA | 0.5ft) | % | (10.) | | : | ▲ SI | PT (N 20 3 | √ ₆₀) ∡ | 40 |
| | | SAND , little Silt, little Gravel, dense to very dense, wet, homogeneous, poorly graded, sub-rounded to sub-angular, non-plastic, light brown to tan, alluvium, | | _ 55.9_ | S-17 | 50/.4' | >61 | 1.7 | 89 | | | | | |
| 45 | | Class. on jar samples collected from S-17 to S-21 A-2-4(0)/SM N.M.C.=17.3%. (Layer continued from the previous page.) | | | | | | | | | | | | |
| | | | | - 61.0- | S-18 | 36-43-47-50 | 120 | 1.9 | 95 | | | | | |
| 50 50 | | - clay seam 64.8'-65.2'. | A-2-4 / SM | - 64.0 - - 65.9 _ | - S-19 | 9-21-33- 50/.4' | >72 | 1.9 | 100 | | | | | |
| 55 | | | | | S-20 | 39-46-48- 50/.3' | >125 | 1.2 | 67 | į | ÷ ÷ ; | | | |
| • | | - heaving sands @ 72.0'. | | _ 70.8 _ | | | | | | | | | | |
| 60 | | 74.9'/El61.8 | | | S-21 | 34-50/.4' | >67 | 0.8 | 89 | | | | | |
| | | Bottom of boring. | | 21/201 | | NAL | | | | | | | | |

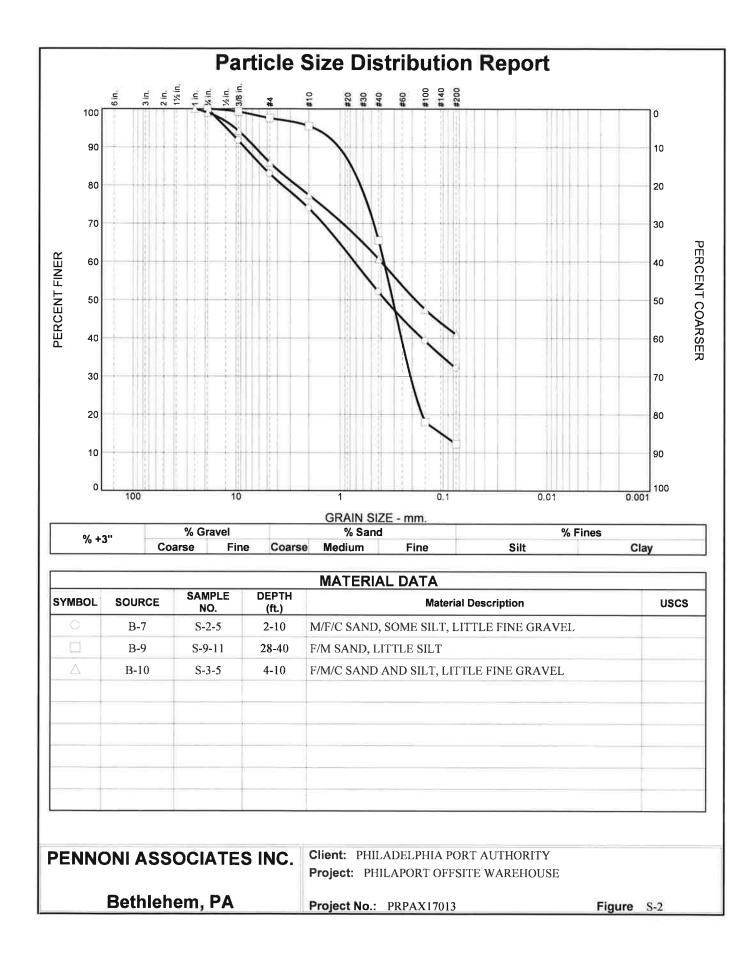
APPENDIX B – Laboratory Data



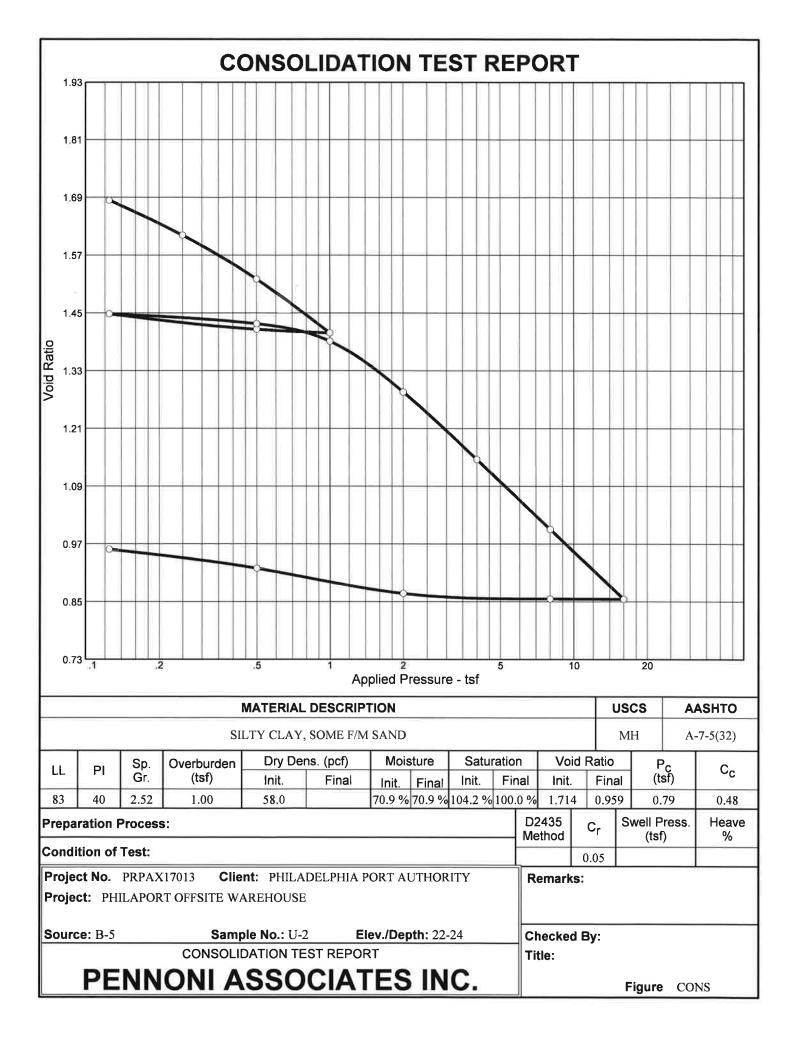
| | | | | | - | | | - | | T | _ | | _ | r | - | - 1 | _ | - | - | | - | - | _ | |
|---|----------------------------|---|-------|----------|---------|-------|-------|---|-------|--------|-------|-------|---|---|---|-----|-------|---|---|---|---|---|---|--|
| | HLDN | (%) NIVES TERNIN (%) | | | | 14.4 | | | | | | | | | | | | | | | | | | |
| | R STRENGTH | COHESION (tat) | | | | 0.37 | | | | | | | | | | | | | | | | | | |
| | SHEAR | ELKENCLH (121) COWLKEZEIAE NACONEINED | | | | 0.74 | | | | | | | | | | | | | | | | | | PRPAX 17013 L-1 |
| | % | ORGANIC CONTENT | 4.2 | | | 7.9 | 10.5 | | | | | 26.2 | | | | | | | | | | | | |
| | (J) | COMPRESSION INDEX | | | | | 0.49 | | | | | | | | | | | | | | | | | JOB No.: TABLE No.: |
| | (Cr) | KECOMPRESSION INDEX | | | | | 0.03 | | | | | | | | | | | | | | | | | JOB No.: TABLE N |
| | | PRECONSOLIDATIO PRESSURE (TSF) Pc | | | | | 0.95 | | | | | | | | | | | | | | | 1 | | |
| | ON | GTANDARD/MODIFIED | | | | | | | | | | | | | | | | | | | | | | SNOF |
| | COMPACTION DATA | CONTENT % OPTIMUM MOISTURE | | | | | | | | | | | | | | | | | | | | | | VAREI A |
| | COM | DENSILA (^{del)} Wyximum DKA | | | | | | | | | | | | | | | | | | | | | | JON WA |
| - | | S&TURATION % DECREE OF | | | | 91 | 100 | | | | | | | | | | | | | | | | | F DISTRIBUTION PHILADELPHIA, |
| | ETRIC | (9) ΟΙΤΛЯ ΟΙΟΥ | | | | 1.66 | 1.71 | | | | | | | | | | | | | | | | | T DIST PHILA |
| | VOLUMETRIC | DBX NNIT MEICHT (pei) | | | T | 63.5 | 58.0 | | | | | | | | | | | | | | | | | DJECT: PHILAPORT DISTRIBUTION WAREHOUSE CATION: PHILADELPHIA, PA |
| | | SPECIFIC GRAVITY (G) (*) ASSUMED | | | T | 2.70* | 2.52 | | | | | | | | | | | | | | | | | PROJECT: PHILAP LOCATION: |
| 5 | % M | WOISTURE CONTENT | 40.1 | 0 | 11.8 | 55.7 | 70.9 | | 27.3 | 20.5 | 35.4 | 131.2 | | | | | | | | | | | | ت: 2018 ت: 2018 |
| | | ΓΙΟΛΙΒΙΙΑ ΙΑΒΕΧ Ι ^Γ | | | | 1.6 | 0.7 | | | T | | | | | | | | | | | | | | DATE 1/22/ DATE |
| | ICITY | ^d I X300 X101 X100 X I | ЧN | | | 14 | 40 | | | | | NP | | | | | | | | Π | | | | 12 |
| | PLASTICITY | PLASTIC LIMIT WP | 86 | | | 33 | 43 | | | | | | | | | | | | 2 | | | 1 | | |
| 2 | | LIQUID LIMIT WI | 84 | | | 47 | 83 | | | | | | | | | | | | | | | | | Y: BY: |
| | TION | % AVID/LIIS | 63 | - | ~ | | 34/39 | | 32 | 12 | 41 | | | | | | | | | | | | | DRAWN BY RJE CHECKED E |
| | GRAIN SIZE DISTRIBUTION | % ANVS | 37 | 407 | 8 | | 27 | | 51 | 85 | 46 | | | | | | | | | | | | | CHE |
| | DIS | CKAVEL % | | 21 | 10 | | | ļ | 17 | т | 13 | | | | | | | | | | | | | ŃC. |
| | T | SOIL GROUP SYMBO | HM | | | OL | НО | | | | | | | | | | | | | | | | | TES II |
| | | DEPTH (ft) | 13-15 | 13 60 | 43-00 | 6-8 | 22-24 | | 2-10 | 28-40 | 4-10 | 18-20 | | | | | | | | | | | | PENNONI ASSOCIATES INC. |
| | | SAMPLE NUMBER | S-6 | 6 1 J 16 | c1-71-0 | S-4 | U-2 | | S-2-5 | S-9-11 | S-3-5 | S-7 | | | | | | | | | | | | ONI A |
| | | BORING NUMBER | B-3 | | 5 7 | B-5 | | 1 | B-7 | B-9 | B-10 | | | | | | | | | | | | | PENN |

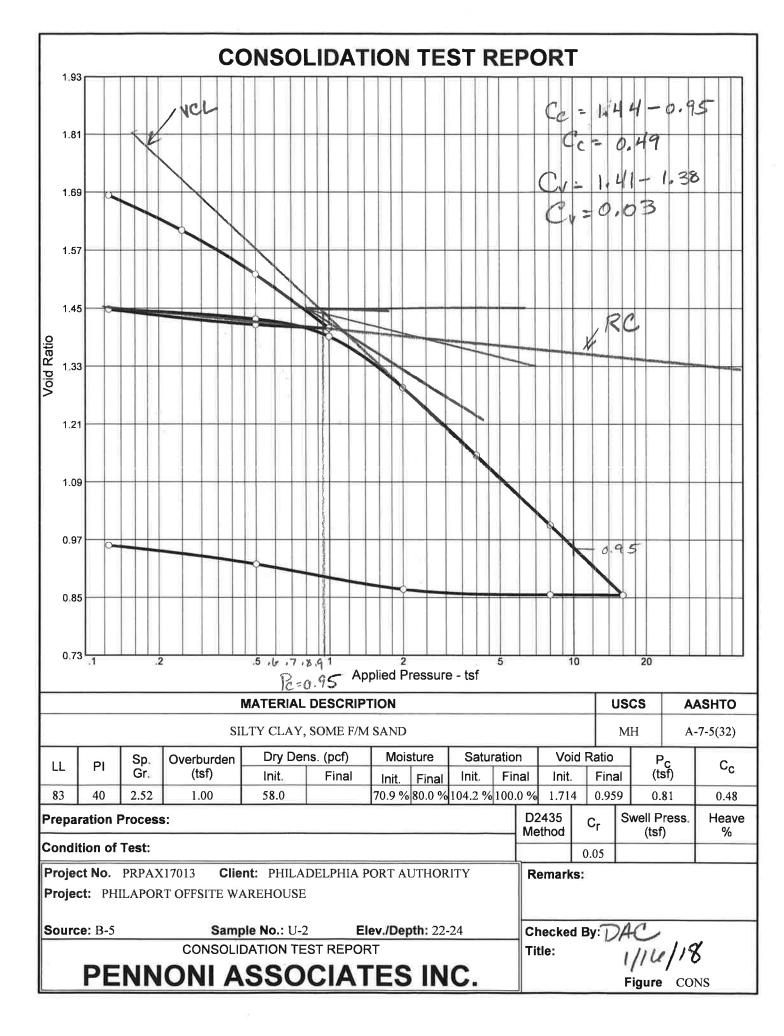
SUMMARY OF LABORATORY DATA

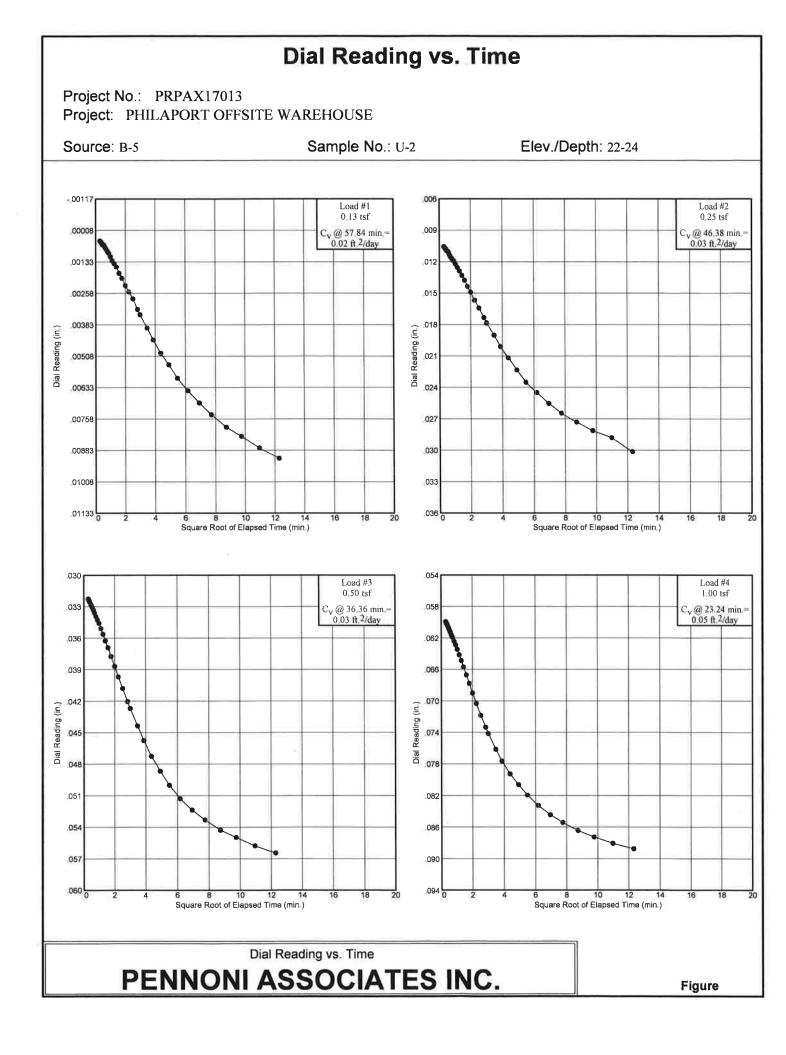


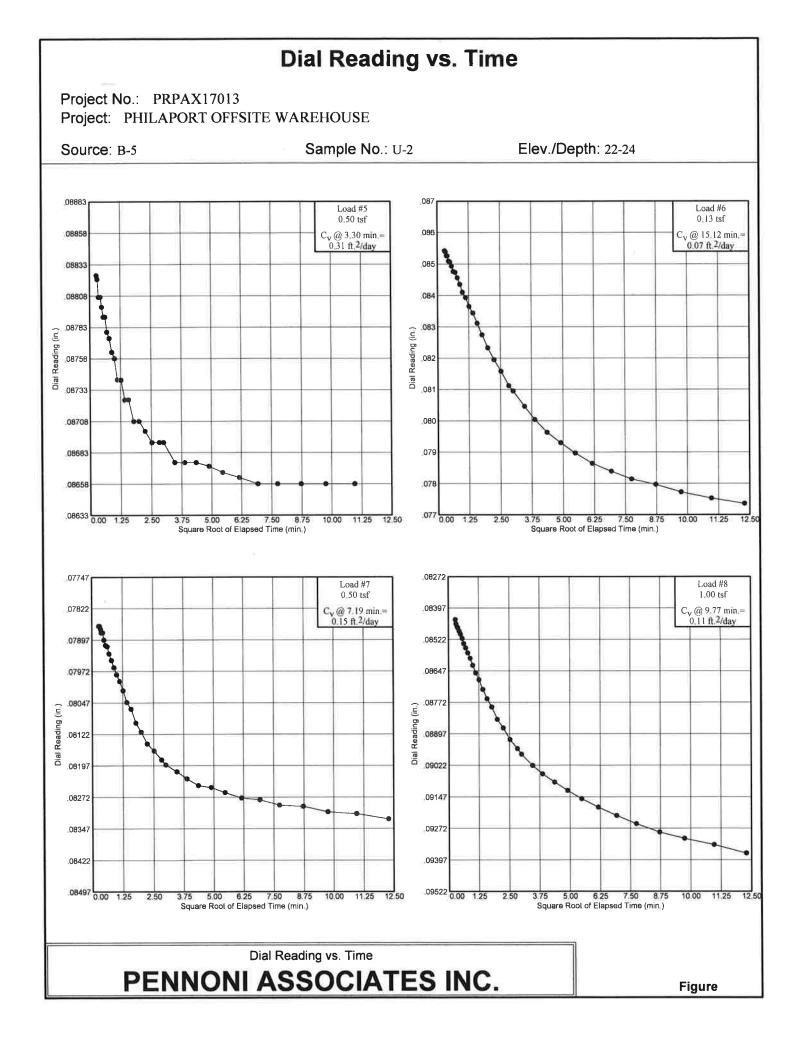


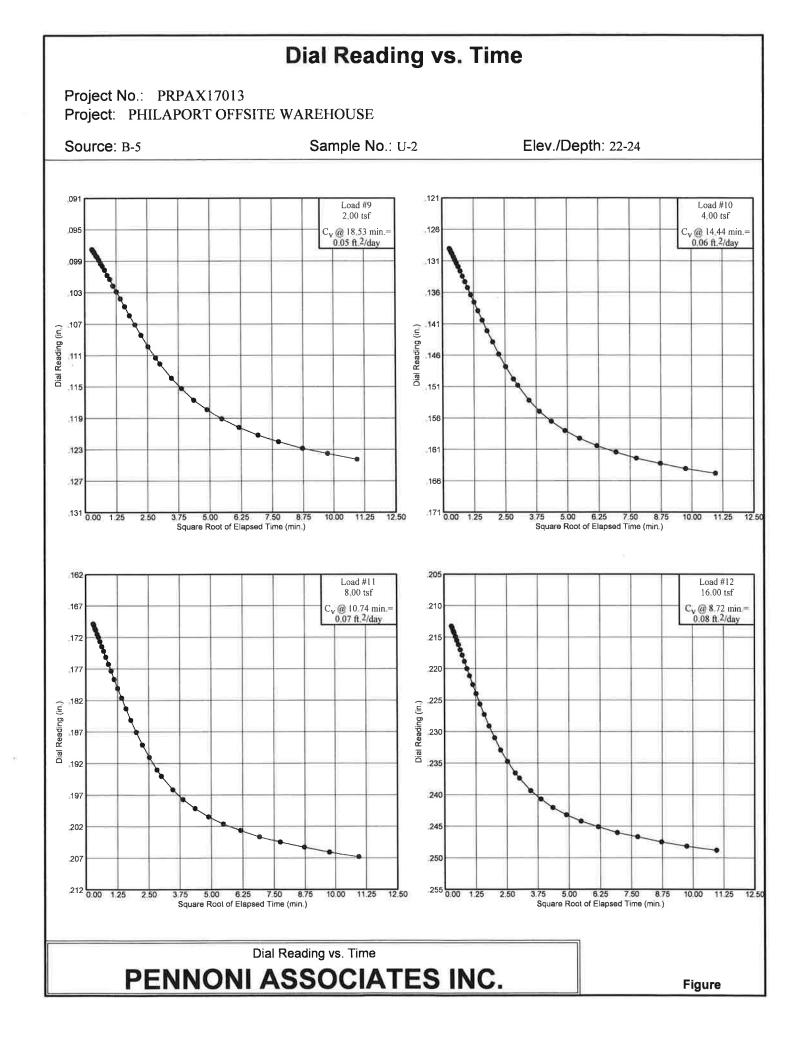
| | | INCO | MEI | | | 201 | MD | DE | 22 | | TE | т р : | • | |
|--------------------------------|------------------------------|------|---|---|--|-----------------------------|-----------|-------|-------|------|----------|---------------|-----|---|
| | U | NGC | | | | | | NL. | 551 | | | .51 | | |
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| | | | | | ۸vi | | ain, % | 4 | | | | | | |
| | | | | | | | an, 7 | 0 | | | | | | |
| Sample No. | | | | | | | 1 | | | | | | | |
| Unconfined streng | th, tsf | | | | | | 0.7 | 40 | | | | | | |
| Undrained shear s | trength, tsf | | | | | | 0.3 | 70 | | | | | | |
| Failure strain, % | | | | | | | 14 | .4 | | | | | | |
| Strain rate, in./min | l | | | | | | 0.0 | | | | | | | |
| Water content, % | | | | | | _ | 55 | | | | | | | |
| Wet density, pcf | | | | _ | | _ | 98 | | _ | | | _ | | |
| Dry density, pcf | | | | | | | 63 | | _ | | | | | |
| Saturation, % | | | | | | _ | 90 | | | | | | | |
| Void ratio Specimen diamete | ar in | | | | | | 1.6 | | _ | | | | | |
| Specimen diameter | | | | | | | 2.2 | | | | | | | |
| Height/diameter ra | | | | | | - | 2. 1.9 | | _ | | | | | |
| Description: | | | | | | | 1., | - | _ | | | 1 | | 1 |
| LL = 47 PL = 33 PI = 14 | | | | | | A | ssur | ned (| GS= | 2.70 | Т | ype: | SPT | |
| Project No.: PRPA | Project No.: PRPAX17013 Clie | | | | | t: PH | ILAD | ELPH | IIA P | ORT | AUTI | | | |
| Date Sampled: | | | | | | | | | | | | | | |
| Remarks: | | | Project: PHILAPORT OFFSITE WAREHOUSE | | | | | | | | | | | |
| | Source of Sample: B-5 Depth | | | | | | | | | | | | | |
| | | | | | | | | | | l | Dept | 1: 6-8 | \$ | |
| | | | | | Jaille | UNCONFINED COMPRESSION TEST | | | | | | | | |
| Eigure UCC 1 | | | | | | | 5 | | | | | | | |
| Figure UCC-1 | | | | | PENNONI ASSOCIATES INC. Bethlehem, PA | | | | | | | | | |

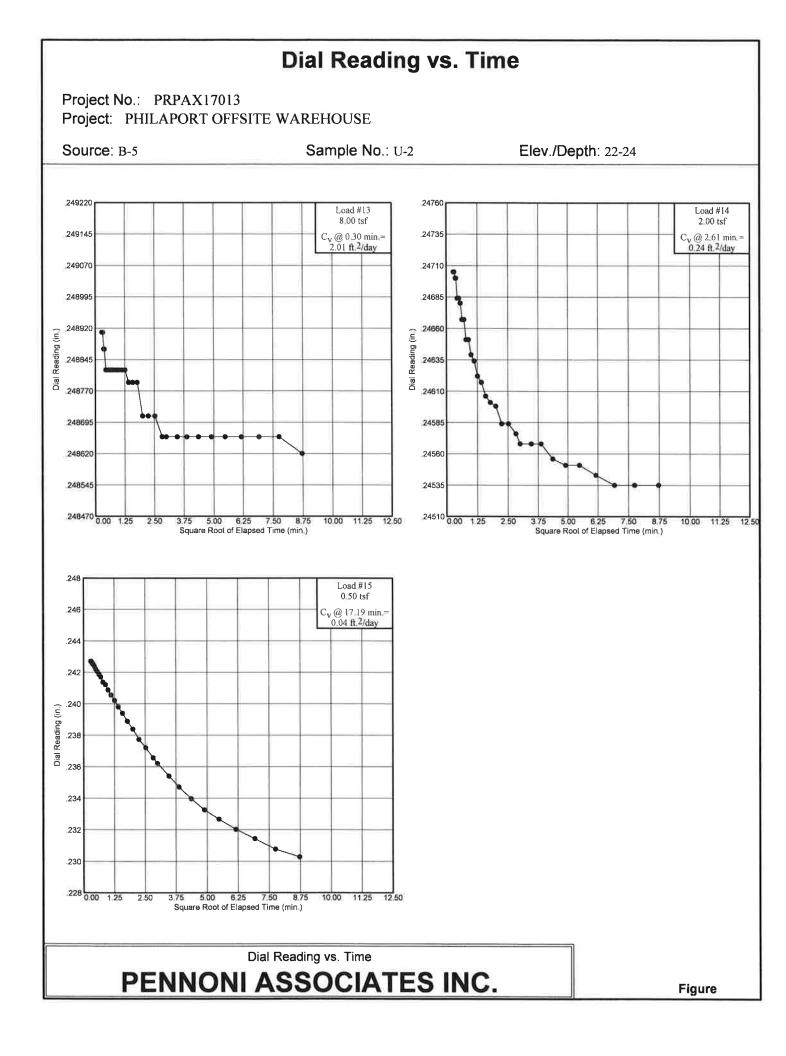












LABORATORY TESTING PROCEDURES

All testing is either done in accordance with the indicated ASTM Designation-latest edition, or with other standard or generally accepted engineering practice as described:

- <u>Consolidation Test of Soils</u> Preparation of samples and testing procedures generally follow the methods described in Lambe, op. Cit. In addition, the time of loading may be selected on the basis of:
 - a. Controlled rate of percent of consolidation
 - b. Controlled pore pressure gradient
 - c. Controlled strain

The method of test is selected to suit the soil type in question and the test is conducted in accordance with generally accepted engineering practice.

- 2. Atterberg Limits Plasticity Indices
 - a. Liquid limit of soils, ASTM D 4318
 - b. Plastic limit and plasticity index of soils, ASTM D 4318
 - c. Shrinkage factors of soils, ASTM D 427

(Moisture content is also determined with the Atterberg Limit test, and liquidity index is also computed)

- 3. <u>Moisture Content of Soil</u> ASTM D 2216
- Particle Size Analysis of Soils ASTM D 421, Dry preparation of soil samples; ASTM D 422, Sieve and/or hydrometer analysis.
- Triaxial Compression Test of Soils Sample preparation, apparatus, and testing generally follow the procedures outlined in <u>Soil</u> <u>Testing for Engineers</u>, T.W. Lambe, John Wiley & Sons, Inc., New York, 1951 and in <u>The</u> <u>Measurement of Soil Properties in the Triaxial</u> <u>Test</u>, Alan W. Bishop & D.J. Henkel, 2nd Edition, St. Martin's Press, New York, 1962
- Unconfined Compression Strength of Cohesive Soil ASTM D 2166

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- 7. <u>Specific Gravity of Soils</u> ASTM D 854
- 8. <u>Unit Weight Determination of Soils</u> See ASTM D 2166 for preparation of specimen except that sample size may differ. For moisture content see ASTM D 2216.
- <u>Visual Identification of Soil Samples</u> All soil samples are visually identified and/or classified. The classification system used is shown in Table L-1.
- 10. Identification of Rock

Rock core samples are identified by the character and appearance of newly fractured surfaces of unweathered pieces, by core conditions and characteristics, and by the determination of simple physical and chemical properties.

- 11. Compaction Test of Soils
 - Moisture-density relations of soils using 5.5 lb. hammer and 12 in. drop, ASTM D 698
 - b. Moisture-density relations of soils using 10
 lb. hammer and 18 in. drop, ASTM D 1557
- Maximum and Minimum Densities of Granular Soils Testing procedures follow D.M. Burmeister, "Suggested Method of Test for Maximum and Minimum Densities of Granular Soils" cited in <u>Proceedings for Testing Soils</u>, Fourth Edition, ASTM, Philadelphia. 1964, pp 175-177.
- Bearing Ratio of Laboratory Compacted Soils ASTM D 1883 (Sometimes called California Bearing Ratio or CBR)
- 14. Organic Content

A modified dichromate oxidation method using ferrous ammonium sulfate is employed in determining the percent of organic matter in soil.

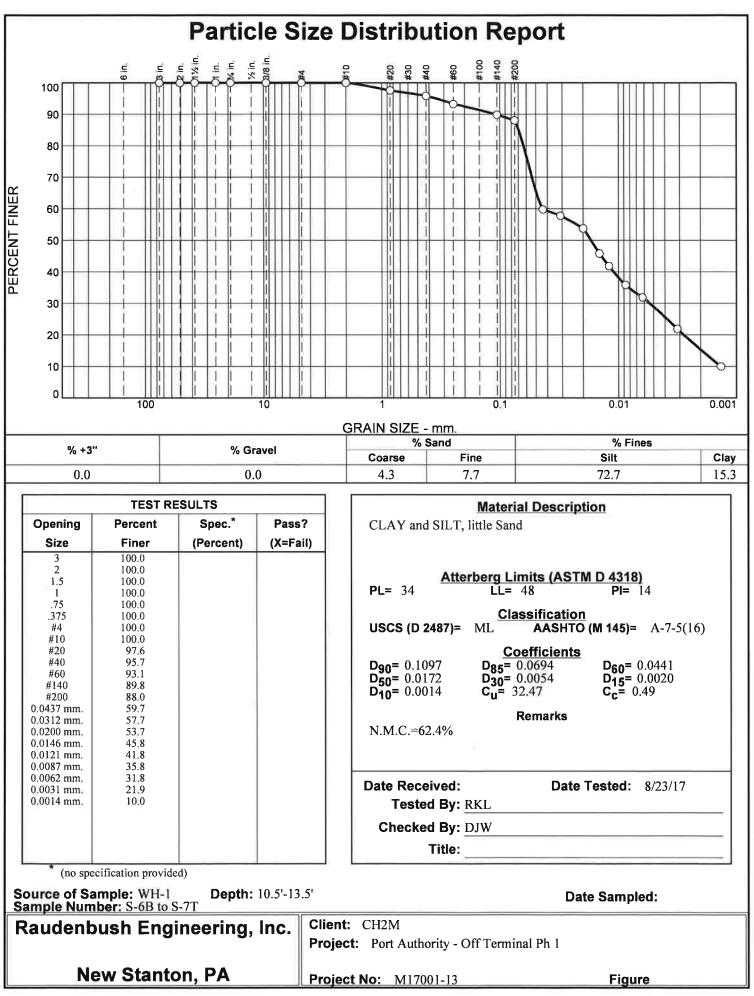


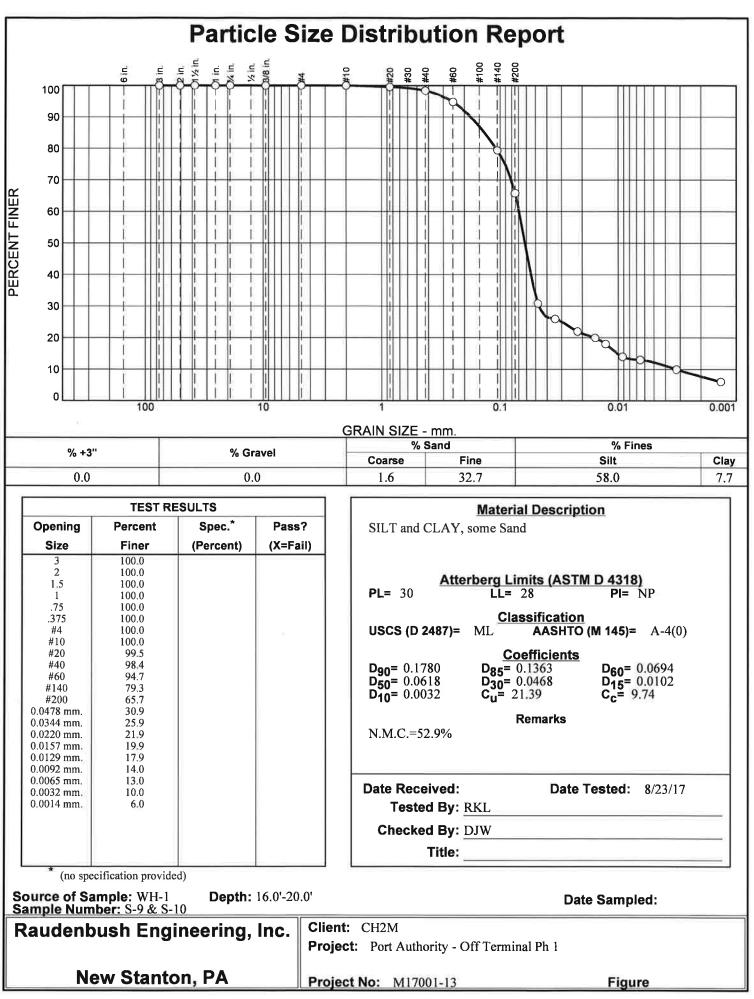
WATER CONTENT DETERMINATION

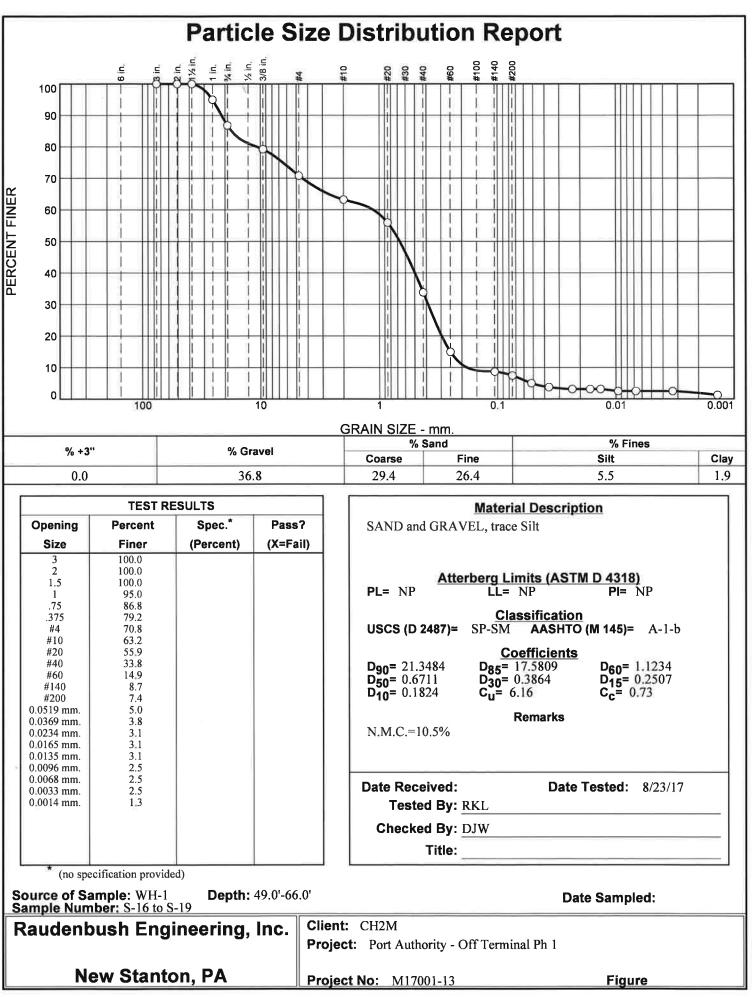
(ASTM D2216-10) / (AASHTO T265)

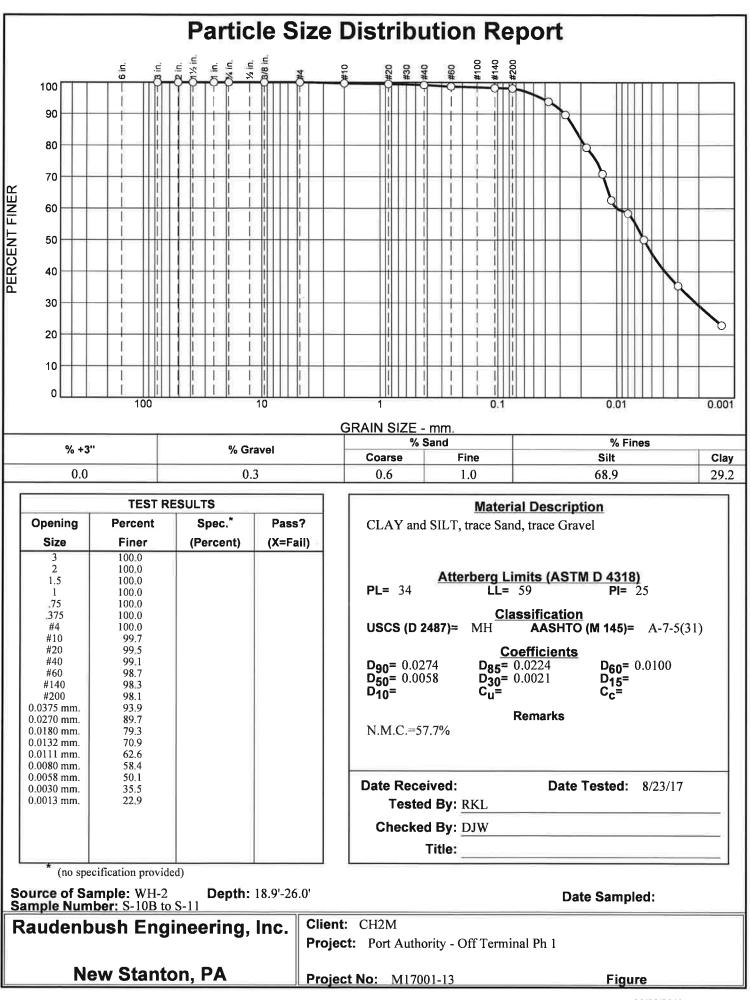
| Client: Project: Project Location: | CH2M Port Authority Off-7 Philidelphia, PA | Terminal Ph. 1 | | Project #: Test Date: Tested By: Chk'd By: | M17001-13 8/18/2017 RKL MDH |
|--|--|----------------|--------------|---|--------------------------------------|
| Lab Sample No.: | 70213 | 70214 | 70215 | 70216 | 70217 |
| Boring No.: | WH-1 | WH-1 | WH- 1 | WH-2 | WH-2 |
| Depth (ft): | 10.5-13.5 | 16.0-20.0 | 49.0-66.0 | 18.9-26.0 | 39.0-51.0 |
| Sample No.: | S-6B & S-7T | S-9 & S-10 | S-15 & S-16 | S-10B & S-11 | S-14 to S-16 |
| Water Content (%): | 62.4% | 52.9% | 10.5% | 57.7% | 13.4% |
| | | | | | |
| Lab Sample No.: | 70218 | 70219 | 70220 | 70221 | 70222 |
| Boring No.: | WH-2 | WH-3 | WH-3 | WH-3 | WH-4 |
| Depth (ft): | 54.0-61.0 | 14.0-18.0 | 29.0-36.0 | 74.0-76.0 | 55.0-61.0 |
| Sample No.: | S-17 & S-18 | S-8 & S-9 | S-12 & S-13 | S-21 | S-17 & S-18 |
| Water Content (%): | 17.6% | 19.8% | 22.3% | 22.2% | 17.2% |
| Lab Sample No.: | 70223 | | | | |
| Boring No.: | WH-5 | | | | |
| Depth (ft): | 49.0-74.9 | | | | |
| Sample No.: | S-17 to S-21 | | | | |
| | | | | | |

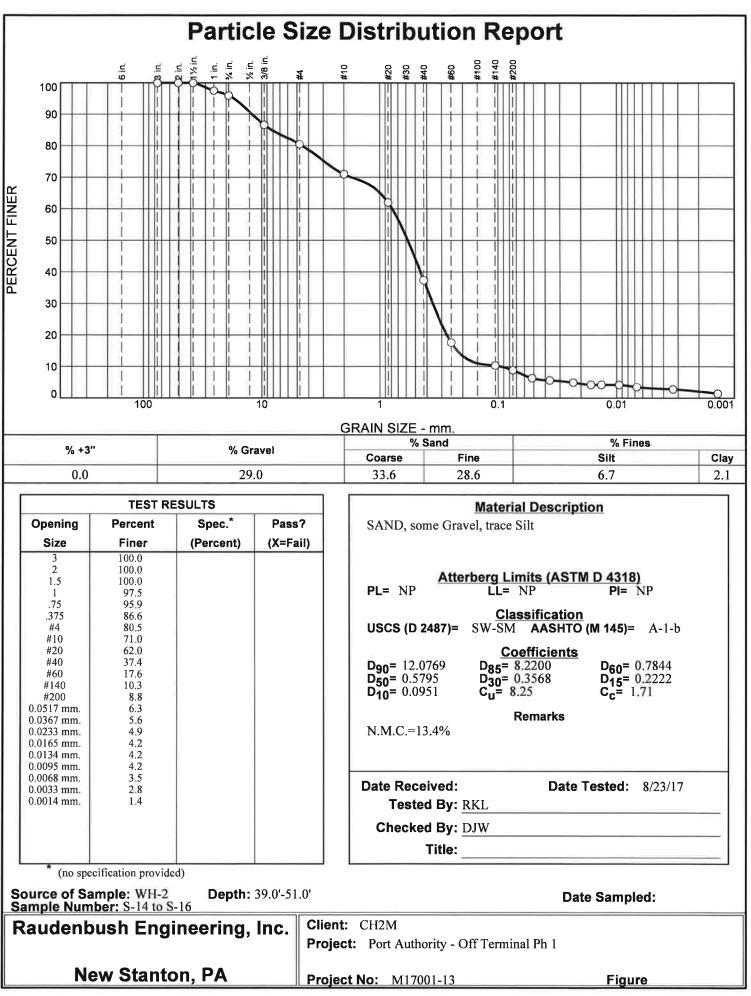
Water Content (%): 17.3%

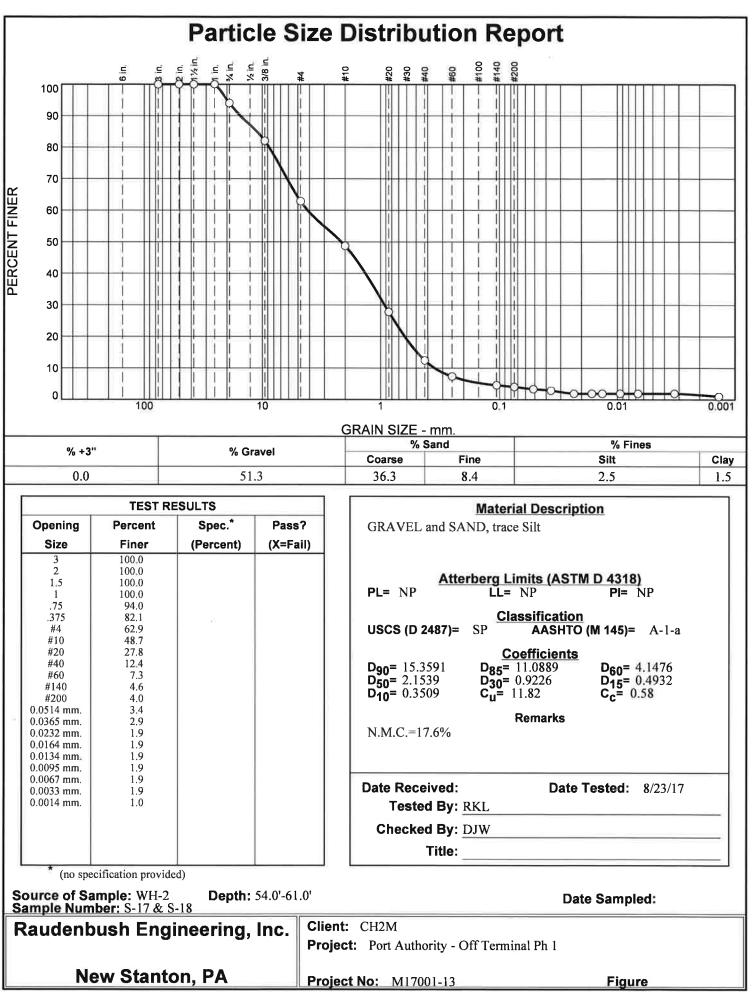


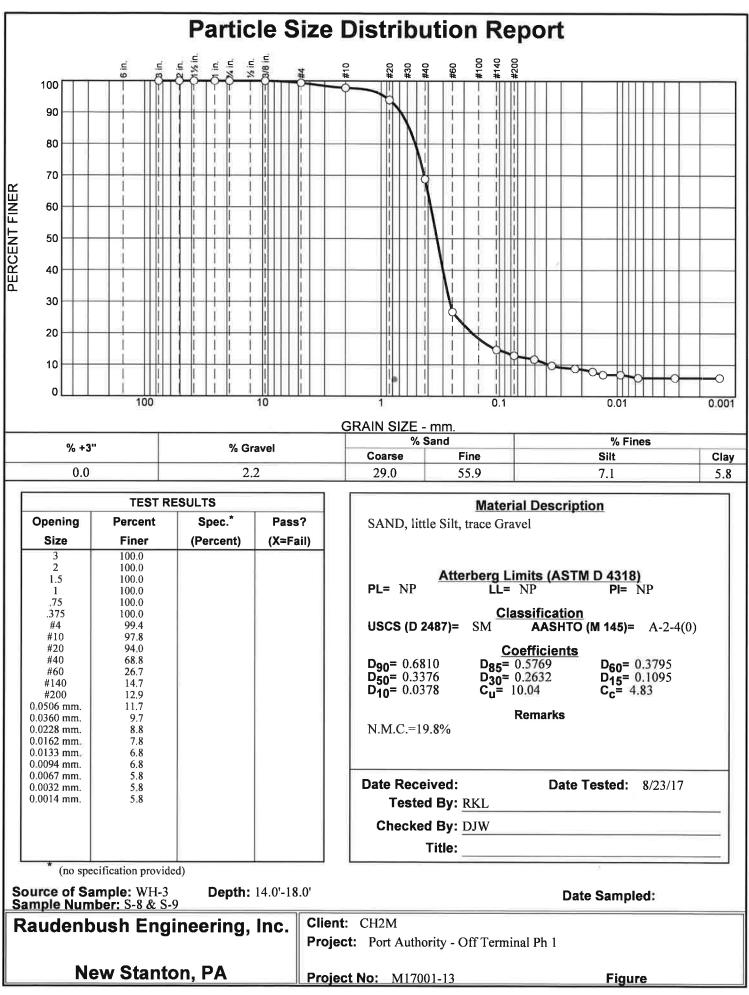


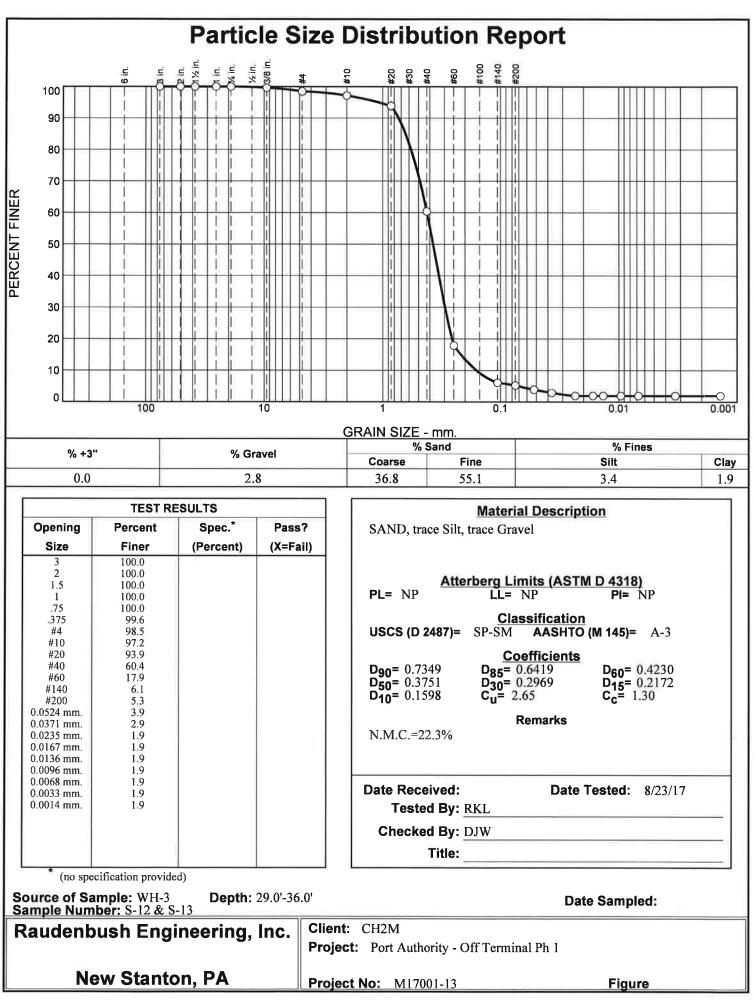


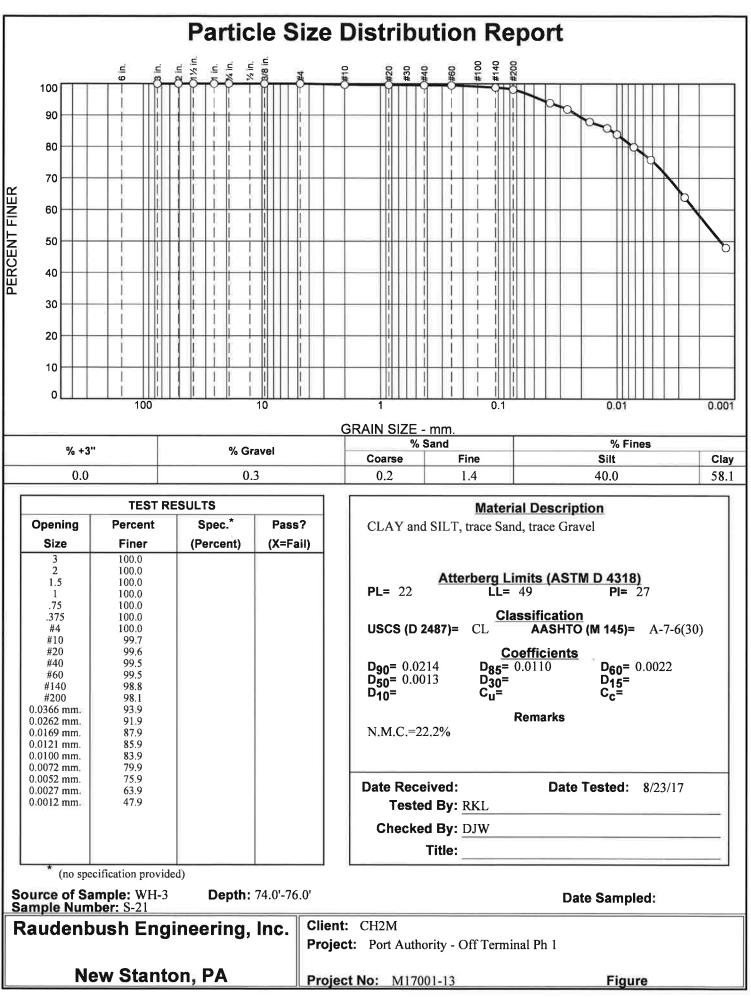


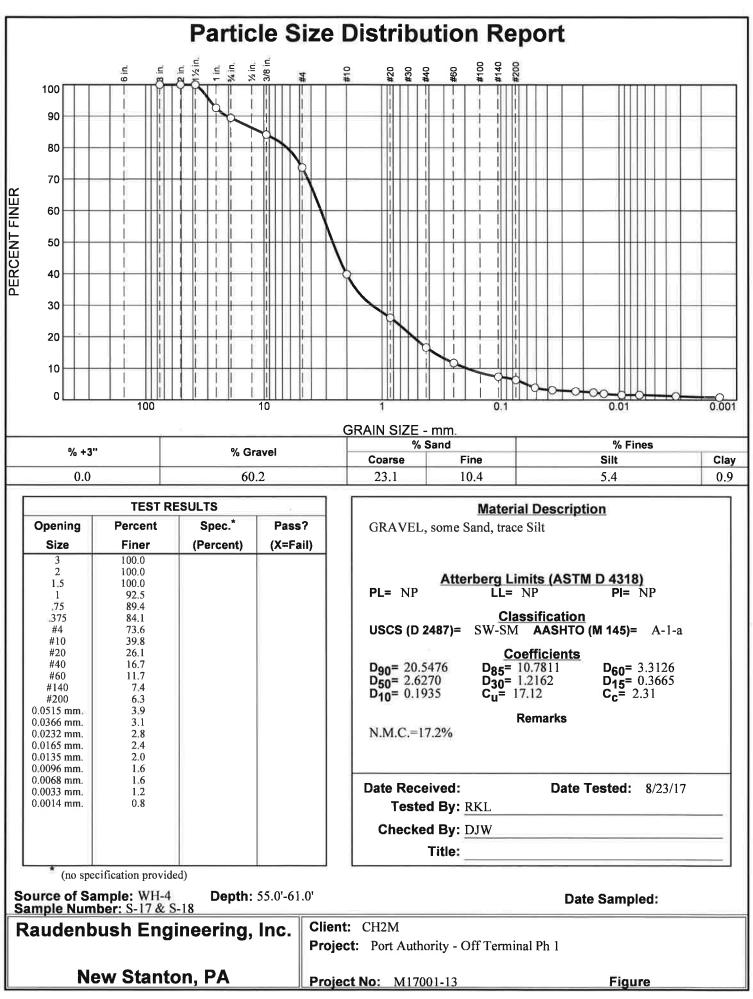


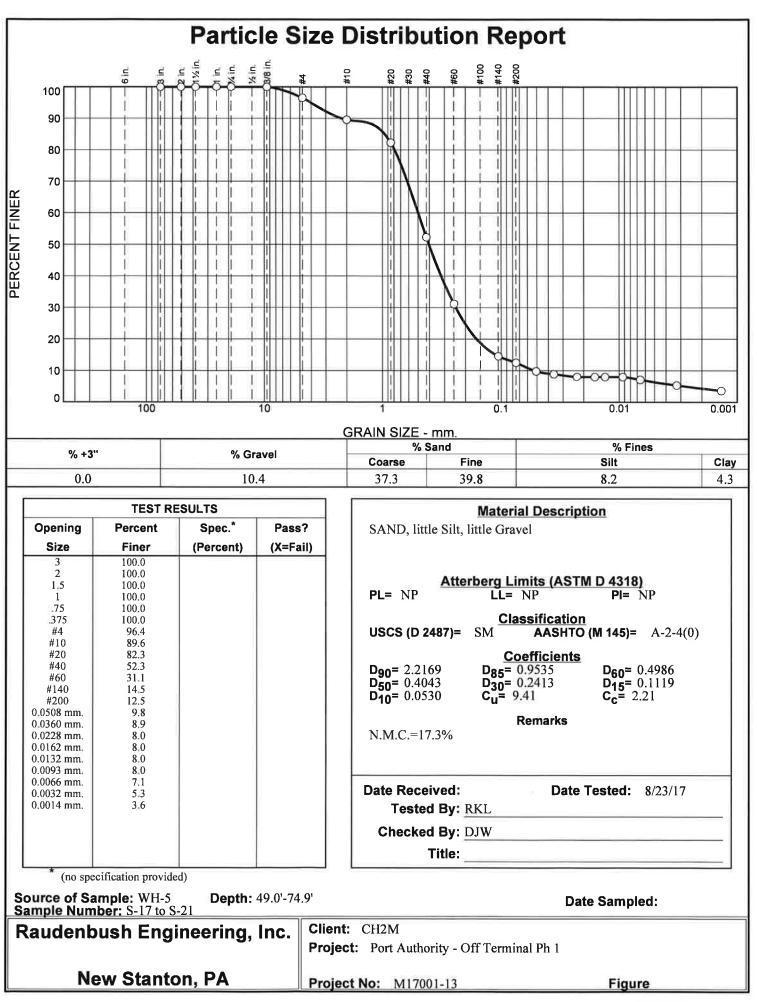












APPEDIX C – Standard Symbols



STANDARD SYMBOLS

| В | Width of footing | Р | deviator stress |
|----------------------------------|---|--------------------------------------|--|
| с | cohesion | Pc | estimated probable preconsolidation pressure |
| c _v C _c | coefficient of consolidation compression index | Po | existing overburden pressure |
| C _c | coefficient of secondary compression | q_{a} | allowable soil bearing pressure |
| C C ₃ | swelling index | Q | triaxial compression test unconsolidated and undrained |
| C_u | uniformity coefficient (D_{60}/D_{10}) | Qc | triaxial compression test consolidated and undrained |
| CBR | California Bearing Ratio | C | |
| D_{f} | depth of foundation | S | triaxial compression test consolidated and drained |
| $\mathbf{D}_{\mathbf{p}}$ | diameter of grain corresponding to | $\mathbf{S}_{\mathbf{r}}$ | degree of saturation |
| | percentage p on grain size curve | υ | pore-water pressure |
| D_{10} | effective grain size | U | degree of consolidation |
| Е | modulus of linear deformation | Uc | unconfined compression test |
| Es | Young's Modulus | \mathbf{W}_{f} | moisture content at end of test |
| \mathbf{E}_{8} | Toung's Modulus | \mathbf{W}_1 | liquid limit |
| e | void ratio | Wn | natural moisture content |
| Fs | factor of safety | $\mathbf{w}_{\mathbf{p}}$ | plastic limit |
| G | specific gravity | γ | unit weight |
| | | $\boldsymbol{\gamma}_{\mathrm{d}}$ | dry unit weight |
| h | hydraulic head | $\boldsymbol{\gamma}_{\mathrm{b}}$ | submerged unit weight |
| Н | stratum thickness | ε | unit linear strain |
| i | hydraulic gradient | $\boldsymbol{\epsilon}_{\mathrm{f}}$ | unit linear strain at failure |
| | | σ | normal stress |
| I_L | liquidity index | σ_1 | major principal stress |
| $\mathbf{I}_{\mathbf{P}}$ | plasticity index | 0 3 | minor principal stress |
| k | coefficient of permeability | τ | shear stress |
| $\mathbf{k}_{\mathbf{h}}$ | coefficient of horizontal subgrade | φ | angle of internal friction |
| | reaction | ka | coefficient of active pressure |
| k _v | coefficient of vertical subgrade | $\mathbf{k}_{\mathbf{p}}$ | coefficient of passive pressure |
| - v | reaction | δ | friction angle |
| 1 | length of footing | tan ð | friction factor |
| n | porosity | | |

APPEDIX D – Pavement Thickness



| Boring No. | Thickness of Bituminous Concrete (in) | Thickness of Processed Aggregate (in) |
|------------|---|---|
| B-1 | 5 | 7 |
| B-2 | 5 | 6 |
| B-3 | 5 | |
| B-4 | 6 | |
| B-5 | 5 | |
| B-6 | 8 | 5 |
| B-7 | 7 | |
| B-8 | 5 | |
| B-9 | 6 | 4 |
| B-10 | 5 | |
| B-11 | 4 | 6* |
| B-12 | 4 | 6* |
| B-13 | 7 | 2 |
| B-14 | | 12 |
| B-15 | | |
| B-16 | | |
| B-17 | | |
| B-18 | | |
| B-19 | | 6 |
| B-20 | 6 | 1 |

TABLE 1 – Pavement Thickness in Borings Performed During 2017 Study TABLE 2 – Pavement Thickness in Test pits Performed During 2019 Study

| Test-pit No. | Thickness of Bituminous Asphalt (in) | Thickness of Processed Aggregate (in) |
|--------------|--|---|
| TP-1 | 4 | 8 |
| TP-2 | 4 | 8 |
| TP-3 | 4 | 8 |
| TP-4 | 4 | 8 |
| TP-5 | 4 | 8 |
| TP-6 | 2.5 | 9.5 |
| TP-7 | 0.5 | 0.5 |
| TP-8 | 4 | 8 |
| TP-9 | 4 | 8 |
| TP-10 | 4 | 8 |
| P-1** | 6 | 6 |
| P-2** | 5 | 9 |
| P-3 | 5 | 8 |
| P-4 | 4 | 11 |
| P-5 | 4 | 8 |
| P-6** | 4 | 9 |
| P-7 | 4 | 10 |
| P-8 | 4 | 10 |
| P-9 | 7 | 6 |
| P-10** | 4 | 8.5 |

*: Noted in boring logs as "Concrete"

**: Sand noted below processed aggregate

APPEDIX E – Important Information About This Geotechnical Engineering Report by GBA



Important Information about This Geotechnical-Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical-engineering study conducted for a civil engineer may not fulfill the needs of a constructor — a construction contractor — or even another civil engineer. Because each geotechnical- engineering study is unique, each geotechnical-engineering report is unique, prepared *solely* for the client. No one except you should rely on this geotechnical-engineering report without first conferring with the geotechnical engineer who prepared it. *And no one* — *not even you* — should apply this report for any purpose or project except the one originally contemplated.

Read the Full Report

Serious problems have occurred because those relying on a geotechnical-engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

Geotechnical Engineers Base Each Report on a Unique Set of Project-Specific Factors

Geotechnical engineers consider many unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk-management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical-engineering report that was:

- not prepared for you;
- not prepared for your project;
- not prepared for the specific site explored; or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical-engineering report include those that affect:

- the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a lightindustrial plant to a refrigerated warehouse;
- the elevation, configuration, location, orientation, or weight of the proposed structure;
- the composition of the design team; or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project changes—even minor ones—and request an

assessment of their impact. *Geotechnical engineers cannot* accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.

Subsurface Conditions Can Change

A geotechnical-engineering report is based on conditions that existed at the time the geotechnical engineer performed the study. *Do not rely on a geotechnical-engineering report whose adequacy may have been affected by*: the passage of time; man-made events, such as construction on or adjacent to the site; or natural events, such as floods, droughts, earthquakes, or groundwater fluctuations. *Contact the geotechnical engineer before applying this report to determine if it is still reliable.* A minor amount of additional testing or analysis could prevent major problems.

Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ — sometimes significantly — from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide geotechnical-construction observation is the most effective method of managing the risks associated with unanticipated conditions.

A Report's Recommendations Are Not Final

Do not overrely on the confirmation-dependent recommendations included in your report. *Confirmationdependent recommendations are not final*, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations *only* by observing actual subsurface conditions revealed during construction. *The geotechnical engineer who developed your report cannot assume responsibility or liability for the report's confirmation-dependent recommendations if that engineer does not perform the geotechnical-construction observation required to confirm the recommendations' applicability.*

A Geotechnical-Engineering Report Is Subject to Misinterpretation

Other design-team members' misinterpretation of geotechnical-engineering reports has resulted in costly

problems. Confront that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Constructors can also misinterpret a geotechnical-engineering report. Confront that risk by having your geotechnical engineer participate in prebid and preconstruction conferences, and by providing geotechnical construction observation.

Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical-engineering report should *never* be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, *but recognize that separating logs from the report can elevate risk.*

Give Constructors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make constructors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give constructors the complete geotechnical-engineering report, but preface it with a clearly written letter of transmittal. In that letter, advise constructors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/ or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. *Be sure constructors have sufficient time* to perform additional study. Only then might you be in a position to give constructors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

Read Responsibility Provisions Closely

Some clients, design professionals, and constructors fail to recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations," many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help others recognize their own responsibilities and risks. *Read these provisions closely*. Ask questions. Your geotechnical engineer should respond fully and frankly.

Environmental Concerns Are Not Covered

The equipment, techniques, and personnel used to perform an *environmental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnicalengineering report does not usually relate any environmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures*. If you have not yet obtained your own environmental information, ask your geotechnical consultant for risk-management guidance. *Do not rely on an environmental report prepared for someone else.*

Obtain Professional Assistance To Deal with Mold

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the express purpose of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold-prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, many mold- prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical- engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.

Rely, on Your GBC-Member Geotechnical Engineer for Additional Assistance

Membership in the Geotechnical Business Council of the Geoprofessional Business Association exposes geotechnical engineers to a wide array of risk-confrontation techniques that can be of genuine benefit for everyone involved with a construction project. Confer with you GBC-Member geotechnical engineer for more information.



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