

July 19, 2023

To: All Bidders

From: Kate Bailey Director of Procurement

Re: ADDENDUM NO. 6 23-026.1 - RFP for Design Build of Temperature Controlled Warehouse

This Addendum No. 6 is issued to:

- 1. Provide a *revised* Geotechnical Report (attached) which shall supersede the report provided in Addendum 5. Note, this report is being supplied for informational purposes only.
- 2. Clarify that Proposers are not required to identify the specific DBE subcontractors, suppliers, or manufacturers within the DBE-3 DBE Listing, Page 1 or 1 (Per Appendix E, DBE Listing.)

However, if a DBE subcontractor is known at time of submission, the proposer must be included in Proposers Appendix D submission.

All other terms and conditions remain unchanged.

Bidders shall acknowledge receipt of this addendum by immediately emailing a copy of the completed acknowledgment to Kate Bailey at <u>procurement@philaport.com</u>

ACKNOWLEDGMENT OF RECEIPT OF ADDENDUM NO. 6 Project #23-026.1 RFP for Design Build of Temperature Controlled Warehouse

Date____

By	

Company_____

Telephone_____

Fax

Email_____



Revised Geotechnical Report

(For informational purposes only)



GEOTECHNICAL ENGINEERING SERVICES

PhilaPort Distribution Warehouse Packer Avenue Philadelphia, PA



Submitted To:

Philadelphia Regional Port Authority 3460 N. Delaware Avenue Philadelphia, PA 19134

Submitted By:

Pennoni Associates Inc. 2041 Ave C, Suite 100 Bethlehem, PA 18017

Daniel P. Marano Jr., PE

Geotechnical Project Engineer



January 25, 2018 (Revised May 13, 2019)

PRPAX 17013.04



January 25, 2018 (Revised May 13, 2019)

PRPAX 17013.04

Ms. Lisa Magee, PE Chief Engineer/Director of Engineering Philadelphia Reginal Port Authority 3460 N. Delaware Avenue Philadelphia, PA 19134

Re: Geotechnical Engineering Services PhilaPort Distribution Warehouse Philadelphia, Pennsylvania

Ms. Magee:

We are pleased to submit our geotechnical engineering report for the referenced project. Work was initiated in general accordance with our revised proposal dated December 6, 2017, and your subsequent authorization to proceed.

In January of 2019 the project details began to finalize, this included building size, location, building loads and finished floor elevation. We have revised our report and recommendations based on the changes described above.

We trust that the information presented herein is what you require at this time and we thank you for the opportunity to assist you with this project. If you have any questions, or if you need any further assistance with this project, please contact this office at your earliest convenience.

Respectfully yours,

PENNONI ASSOCIATES INC.

Daniel P. Marano Jr., PE Geotechnical Project Manager

Erederick A. Brinker, PE Associate Vice President Geotechnical Division Manager

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APPENDICES

APPENDIX A – Field Data

Current Study Boring Logs

Boring Location Plan Test Pits Location Plan Boring Log Key Sheet

Preliminary Study Boring Logs Pennoni; B-1 through B-20 TP1 through TP-10 P-1 through P-10 Drawing LP-1 Drawing LP-2

Raudenbush Engineering, Inc.; WH-01 through WH-05

APPENDIX B – Laboratory Data

Current Study Summary of Laboratory Test Data Gradation Curves Unconfined Compression Test Consolidation Test Dial Readings vs. Time Laboratory Testing Procedures

Table L-1 S-1 & S-2 UCC-1 CONS-1

Preliminary Study Gradation Curves

APPENDIX C – Standard Symbols

APPENDIX D – Pavement Thickness

APPENDIX E – Important Information About This Geotechnical Engineering Report by GBA



1. EXECUTIVE SUMMARY

Pennoni Associates, Inc. (Pennoni) has completed field exploration for the proposed PhilaPort Distribution Warehouse, located in the City of Philadelphia, Pennsylvania. The project area will occupy the existing new car parking lot between Pattison and Packer Avenues. The purpose of our study was to determine the subsurface conditions at the project site within the footprint of the proposed warehouse building, evaluate these conditions with respect to the proposed development, and present foundation recommendations.

It is our understanding the proposed construction consists of an approximate 197,000 ft² dry storage building with 42 loading dock spaces on the west side of the building. The finished floor elevation is anticipated to be established at Elev. 13.5+/-. An approximate 215,000 ft² cold storage addition is proposed on the south side of the dry storage warehouse. It is our understanding that the dry storage building will be approximately 45 ft high and house four storage levels (first level is the floor and three pallet levels supported by pallet racks above). Additionally, the use of high mast fork trucks will be used inside of the building and will require minimal differential settlement in the floor slab (1/8 in.) in order to operate. Typical warehouse column, and floor loads are anticipated not to exceed 70 kips, and 450 psf respectively. Structural loading information was provided by our Structural Technologies group.

Between the period of July 25 through August 1, 2017, five borings were drilled by Allied Well Drilling, as part of a preliminary subsurface exploration conducted by others. Appendix A includes the preliminary boring logs.

Between the period of December 21, 2017 through January 3, 2018, 20 borings were drilled by C.G.C. Geoservices, LLC. within the proposed warehouse building footprint. Appendix A includes the boring logs and the Boring Location Plan.

On April 18 and April 19, 2019, 20 test pits were excavated by Ambient Group within the property; 10 shallow test pits were excavated to evaluate the pavement thickness, and 10 test pits were excavated for the infiltration testing. Appendix A includes all test pits logs.

Based on the results from the above explorations, laboratory testing, engineering analyses, and our experience, we conclude that construction of the proposed warehouse is feasible. Based on the soils encountered and the anticipated loading, it is our professional opinion that the proposed structure can be supported on either shallow foundations after ground improvement (Controlled modulus columns/Rigid inclusions) is performed, or on deep foundations. Additionally, the proposed floor slab has higher than normal loading and limited tolerances for movement, so we recommend that the ground floor slab should be constructed as a structural slab supported on improved soils or deep foundations. Encountering obstructions (construction debris) should be anticipated during foundation and utility installation. Encountering groundwater in excavations (on the order of 6 to 8 ft) should be anticipated. Due to the proximity to the Delaware River the groundwater elevation may vary with the tidal action. On-site existing inert granular portions of the fill soils can be reused in compacted load bearing fill. Detrimental long-term post-construction settlements are not expected if the recommendations provided herein are followed.

This report provides a more detailed summary of the field and laboratory testing program as well as a discussion of the conclusions and recommendations pertaining to design and construction of the proposed structure.



May 13, 2019

2. INTRODUCTION

2.1. LOCATION

The project site is located west of the Delaware River in south Philadelphia, Pennsylvania. The site is bounded on the north by commercial buildings (seafood market, cold storage, bank) and South Galloway Street followed by Packer Avenue, on the east by South 3rd Street, on the south by Pattison Avenue, on the west by commercial buildings followed by South Lawrence Street.

2.2. PROPOSED CONSTRUCTION

It is our understanding the proposed construction consists of an approximate 197,000 ft² steel frame, dry storage building with 42 loading dock spaces on the west side of the building. An approximate 215,000 ft² cold storage addition is proposed on the south side of the dry storage warehouse. The finished floor elevation of the dry storage building is anticipated to be established at Elev. 13.5+/-. It is also anticipated that the exterior of the buildings will be clad with insulated metal sandwich wall panels with hardening of the lower exterior and interior face of the facade provided via masonry or concrete panel walls. The dry storage building will be approximately 45 ft high and house four storage levels (first level is the floor and three pallet levels supported by pallet racks above). Additionally, the use of high mast fork trucks will be used inside of the building and will require minimal differential settlement in the floor slab (no more than 1/8 in.) in order to operate. Typical warehouse column, and floor loads are anticipated not to exceed 70 kips, and 450 psf respectively. Structural loading information was provided by our Structural Technologies group.

2.3. OBJECTIVES

Our objectives were to determine the subsurface conditions at the project site within the footprint of the proposed building, evaluate these conditions with respect to the proposed construction, and present recommendations regarding:

- foundation design, including a discussion of alternate solutions, if applicable, anticipated total and differential settlements;
- design frost depth;
- floor slab design;
- lateral earth pressure parameters;
- discussion of potential for consolidation and/or differential settlements of substrata encountered;
- "general procedure" Seismic Soil Site Classification in accordance with Table 1613.5.2 of the 2009 International Building Code;
 - evaluation and determination of the earthwork requirements for use in preparation of the site area, including material selection and placement operations;
- suitability of on-site material for re-use as fill/backfill as part of the site work for the project;
- ground water conditions;
- removal or treatment of objectionable material, and;
- quality assurance, field-testing, and observations during construction.



3. FIELD AND LABORATORY WORK

3.1. PREVIOUS FIELD WORK

Between the period of July 25 through August 1, 2017, five borings were drilled by Allied Well Drilling, as part of a due-diligence subsurface exploration conducted by others. Soil samples were reported to have been obtained in general accordance with ASTM D 1586. The data obtained from the previous exploration were used in our analyses.

3.2. FIELD WORK

Between the period of December 21, 2017 through January 3, 2018, 20 borings were drilled by C.G.C. Geoservices, LLC. within the proposed warehouse building footprint at the approximate locations presented on Drawing No. LP-1. The boring locations were selected and established in the field by Pennoni personnel. Soil samples were obtained in general accordance with ASTM D 1586 and ASTM D1587 methods. Appendix A includes the boring logs and Drawing No. LP-1.

Our D. Marano, PE directed the field work; our D. Copeland, EIT, and S. Corcoran, performed a site reconnaissance and full-timed monitored the drilling operations.

Additionally, on April 18 and April 19, 2019, 20 test pits were excavated by Ambient Group within the property; 10 shallow test pits were excavated to evaluate the pavement thickness, and 10 test pits were excavated for the infiltration testing. Appendix A includes all test pits logs. The test pits locations were selected and established in the field by Pennoni personnel.

Our D. Marano, PE directed the field work; our N. Rex and E. Iannetti, full-timed monitored the excavating operations.

3.3. LABORATORY WORK

The soil samples collected during our fieldwork were delivered to our laboratory. Representative samples were selected and tested to determine moisture contents, organic contents, plasticity indices, unconfined compressive strengths, volumetric (unit weight, void ratio), gradation and consolidation characteristics of the subsoils. Additionally, laboratory testing data from the preliminary study performed by others was used in our study. Appendix B includes the results from both studies and a list of testing procedures.

4. SITE CHARACTERISTICS

4.1. SITE HISTORY

Review of historical documents dating back to 1940 indicates the site underwent massive earthwork during the 1940's and 50's. Due to the limited detail and resolution of the published data it is not clear what the site was used for during this period. Between 1957 and 1963, two large rectangular commercial buildings were constructed. The buildings stretched from Packer Avenue to Pattison Avenue and were separated in the middle by South Galloway Street.

The site remained largely unchanged through 2013. Between 2013 and present day, the buildings were razed. Evidence of the razed buildings is evident where the ground cover consists of compacted



processed aggregate over the former building footprints. The site is currently being used as a parking lot for new cars.

4.2. SURFACE FEATURES

Currently the project site consists of a bituminous paved parking lot with associated curbing and light pole structures. The groundcover in the areas of the razed buildings consisted of compacted processed aggregate. The topography of the site is "bowl" shaped with perimeter elevations varying from Elev. 12 to Elev. 10 and descend towards the center of the site to approximate Elev. 9 to Elev. 8. Overhead electrical utilities were observed traversing in the northerly/southerly direction the center of the site. Stormwater inlets and associated underground utilizes were observed running bilaterally along the center of the site from the northern limit to the southern limit of the site.

4.3. GEOLOGY

The project site is located within the Lowland and Intermediate Upland section of the Atlantic Coastal Plain Province. The dominant topographic features of this section include very low local relief and a flat upper terrace surface cut by narrow, steep-sided to open valleys, shallow valleys; includes the Delaware River floodplain. The underlying subsurface material types consist of unconsolidated to poorly consolidated sand and gravel deposits, underlain by very complex, faulted and folded schist, gneiss, and other metamorphic rocks.

Available geological data indicates that the subject site is underlain by the Trenton Gravel Formation consisting of gray or pale-reddish-brown, very gravelly sand interstratified with crossbedded sand and clay-silt beds. This formation also includes areas of Holocene alluvium and swamp deposits

Underlying the Trenton Gravel Formation is the Wissahickon Formation. The Wissahickon Formation consists of a coarsely crystalline, excessively micaceous schist. Fracturing results in a well-developed, platy pattern. This formation is fissile to thinly bedded, moderately resistant to weathering, and often highly weathered to a moderate depth.

4.4. SUBSOILS

The borings and test pits revealed bituminous concrete/concrete/processed aggregate pavement or processed aggregate layer at the surface that varied in thickness from 5 to 13 inches. Appendix D presents pavement thickness encountered in all borings and test pits performed on site. The underlying subsoils have been grouped by us into six principal strata based on their physical and engineering properties and our interpretation of their origin. Following are descriptions of the subsoils encountered at this site.

Stratum F – Urban Fill

The borings and test pits disclosed an Urban Fill layer with a thickness that varies from approximately 7 to 18 ft. The fill generally consists of granular fine to medium SAND, some to trace gravel size rock fragments (brick, ash, cinder, glass, organics), some to trace silt, or SILT, some to trace fine to medium sand, some to trace gravel size rock fragments (brick, ash, cinder, glass, organics).

Standard penetration test (SPT) N-values indicate the density/consistency of this stratum varies from "very loose"/"soft" to "very dense"/"very hard". Typical USCS Classifications associated with this stratum are SM, SP-SM, and ML.



Although not encountered in the borings, encountering remnants of previous foundations and shoring systems during construction, should be expected within Stratum F. If encountered, these obstructions will most likely impair the construction process, especially utility and foundation construction.

Stratum 1 – Silty Clay/Clay (Alluvial)

A stratum of Silty CLAY/CLAY with varying amounts of fine sand gravel and organics (7.9% to 10.5%) was encountered beneath Stratum F fill in many of the borings. The thickness of this layer varies from approximately 5 to 15 ft. SPT N-values indicate the consistency of this soil varies from "very soft" to "firm". The typical USCS Classifications associated with this stratum are OL and OH.

Consolidation testing disclosed a preconsolidation pressure (tsf), compression and recompression index of 0.95, 0.49 and 0.03, respectively. Laboratory testing and visual classification disclosed this layer contained trace to little organics. These data disclose Stratum 1 soils to be compressible.

Stratum 2 – Clayey SILT (Alluvial)

A stratum of SILT with varying amounts of fine sand, gravel and organics (up to 26.2%) was encountered beneath the Stratum F Fill or Stratum 1 soils in many of the borings. The thickness of this layer varies from approximately 5 to 15 ft. SPT N-values indicate the consistency of this stratum varies from "very soft" to "stiff". Typical USCS Classifications associated with this stratum are OH and ML.

Laboratory testing and visual classification disclosed this layer contained trace to some organics. The percentage of organics in Stratum 2 is generally associated with high compressibility, significant secondary compression, often unsatisfactory strength characteristics, and low unit weight. This stratum is also considered compressible.

Stratum 3 – Sand/Gravel (Alluvial)

A stratum of SAND ranging in gradation from poorly (generally, gap graded fine to medium) to well graded with varying amounts of gravel and silt, or GRAVEL with varying amounts of sand was encountered beneath Strata 1 and 2. The thickness of this layer varies from approximately 10 to 32 ft. SPT N-values indicate the relative density of this stratum generally varies from "very loose" to "medium dense". Typical USCS Classifications associated with this stratum are SP and SP-SM.

Stratum 4 – Sand/Gravel (Alluvial)

A stratum of well graded SAND with varying amounts of gravel, or poorly to well graded GRAVEL with various amounts of sand was encountered above and/or beneath Stratum 3 in the borings. Stratum 4 was generally encountered at depths ranging from 43 to 80 ft below the ground surface. SPT N-values indicate that the density of this stratum generally varies from "medium dense" to "very dense". Typical USCS Classifications associated with this stratum is SW-SM, GM and GP.

It should be noted that COBBLES encountered Borings B-2 and B-12 at depths ranging from 45 to 50 ft below the ground surface were included in this Stratum. The material was observed when the augers were extracted.



Stratum 5 – Raritan Clay

A stratum of CLAY/Sandy CLAY with varying amounts of fine sand and gravel was encountered beneath and or between Stratum 4 in some of the borings. Stratum 5 was generally encountered at depths ranging from 53 to 80 ft below the ground surface and generally varies in thickness from approximately 5 to 7 ft. SPT N-values indicate the consistency of this soil varies from "stiff" to "very hard". The typical USCS Classification associated with this stratum is CL.

Auger refusal was encountered in Borings B-2 and B-12 at depths of 47 and 50 ft below existing grades, respectively. Auger refusal is thought to be due to cobbles, rather than the top of rock.

4.5. GROUND WATER

Observations for groundwater were made in the borings during sampling and shortly after completion of drilling. Evidence of groundwater was generally encountered in the borings at depths of approximately 6 to 13 ft below existing grades (Elev. 6.5 to Elev. 0.0). Borings B-17, B-18 and B-20 disclosed evidence of groundwater at depths ranging from 18 to 28 ft below existing grades (Elev. -2.0 and Elev.-11.5), respectively. It is our professional opinion that these latter readings were affected by hydraulically restrictive Stratum 1, and not indicative of the static groundwater table.

Additionally, evidence of ground water was generally encountered in test-pits at depths of approximately 8 to 10.5 ft below existing grades. These observations are for the times indicated and may not be indicative of seasonal, daily or tidal variations in the ground water levels.

Given the project site's vicinity to the Delaware River, daily fluctuations in the groundwater table could be influenced by the tide. Daily and seasonal variations of several feet should be anticipated.

5. ANALYSES AND RECOMMENDATIONS

5.1. SEISMIC SITE CLASS

The borings disclosed subsurface conditions generally described according to the 2015 International Building Code (IBC) as having a soil-profile corresponding to Site Class E – soft clay soil profile.

5.2. SITE WORK

Comparison of the proposed grades to existing grades indicates that cuts as on the order of 1 ft deep and fills up to 5 ft high are expected to establish the ground floor slab. Comparison of the proposed grades to existing grades indicates that cuts as deep as 3 ft and fills up to 2 ft high are required for general site grading. The borings and laboratory testing disclosed Stratum 1 and 2 are compressible. Fills greater than 2 ft high will likely result in consolidation related settlement, which may be significant (> 3 inches). New fills should be placed as early as possible within the construction schedule to allow for settlements to occur.

Prior to the construction of foundations, structural slabs, and pavements, any bituminous concrete must be removed from within the proposed areas of construction. Existing utilities located within the proposed building footprint should be abandoned and relocated outside the limits of the new structure. Any existing



utility line abandoned in-place should be grouted or the line should be removed and the trench appropriately backfilled.

From historic aerial photography, it was disclosed that the site was once partially occupied by structures and associated paved parking. At the time of our field work evidence of previous structures was observed throughout the razed building footprints; however, remnants of the former foundations were not observed, or evident in the borings. The excavation of test pits prior to construction should be considered to better determine if remnants of the previous building will interfere with construction.

Any exposed subgrade should be proof-rolled in the presence of Pennoni personnel in an attempt to disclose unstable surface areas. During proof-rolling, any unstable area found should be stabilized by excavating and replacing those soils with suitable soil that is adequately compacted. This can be accomplished by properly adjusting the moisture content of the subgrade soils and compacting them, or by other methods (placing a geotextile and stone layer, etc.).

Our experience indicates that the clean inert granular portions of the Fill stratum can be reused in a compacted fill for backfill of utility excavations as long as it has a maximum particle size of 3 in., and is free of trash, environmental hazards, and other deleterious material. Additionally, demolition debris consisting of concrete and pavement millings can be used in compacted load bearing fills provided there are no environmental hazards associated with the materials and it is crushed to reduce the maximum particle size to less than 3 inches. Adjusting the moisture content prior to fill placement should be expected. Stratum 1 and Stratum 2 soils are not suitable, in their current state, for re-use in compacted load bearing fill.

Imported structural fill should be selected from suitable borrow sources and be approved by the Geotechnical Engineer's representative well in advance of fill construction. Granular fill ideally should consist of well-graded material with not more than 20 percent passing the No. 200 sieve and have a plasticity index not greater than 8 percent; PennDOT 2A, modified stone or recycled concrete can be considered. Other gradations can be considered based on laboratory testing and at the discretion of the Geotechnical Engineer.

Granular fills should be placed in layers not exceeding 10 to 12 in. loose thickness. This criterion might be adjusted by the geotechnical engineer in the field depending on the conditions present at the time of construction, on the compaction equipment used, and on the fill material selected. Fills for support of foundations and pavement should be compacted to at least 98 percent and 95 percent, respectively, of the laboratory determined maximum dry density, ASTM D 698, when small, hand-operated compaction equipment is used, and to at least 95 percent and 93 percent, respectively, of the laboratory determined maximum dry density, ASTM D 698, heavy–duty construction equipment is used. Fills should extend a minimum of 5 ft beyond the exterior edge of a loaded area and have side slopes not steeper than 2 horizontal to 1 vertical.

Specifications should indicate that the percentage of maximum dry density attained in the field is not the only criteria to be used for assessing fill compaction. Observation of the behavior of the fill under the loads of construction equipment should also be used. If the test results indicate that the percentage of compaction is being achieved, but the soil mass is moving under the equipment, placement of additional fill should not be continued until the movement is stabilized. Otherwise, settlement of the fill may occur.



May 13, 2019

5.3. FOUNDATIONS

Based on the soils encountered and the anticipated loading, it is our professional opinion that the proposed structure should be supported on shallow foundations bearing on improved soils or deep foundations. Controlled Modulus Columns/Rigid Inclusions (CMC's/RI's) can be considered to sufficiently improve the subsoils to allow the construction of shallow spread foundations. Alternatively, deep foundations like concrete filled steel pipe piles and auger cast-in-place piles can be considered for support. Because of the load carrying capacity of the deep foundations, as described, pile load tests (compression and tension) will be necessary.

5.3.1. CMC's/RI's

In order to support the structure on shallow spread footings we recommend improving the subgrade soil by installing CMCs/RIs elements. These elements improve the existing soil conditions to reduce both total and differential settlements by increasing the overall stiffness of the soil mass. A load transfer platform (LTP), sometimes reinforced with a geogrid, is constructed above the CMCs/RIs using granular fill with a thicknesses that may vary from 12 to 36 inches. CMCs/RIs are installed by a drill rig with a specially designed auger that drills down to the designed termination depth followed by a controlled pressure grouting during extraction. The instillation of the CMCs/RIs results in generating minimal auger spoils and vibration. Spread footings can then be designed to bear in the LTP layer for a maximum allowable net bearing capacity of up to 6,000 psf.

Continuous and isolated footings should be at least 1.5 ft wide and 3 ft square, respectively, to prevent localized shear failure in soil. The subgrade of all exterior footings exposed to freezing temperatures, during construction and/or the life of the structure should be established at least 30 in. below adjacent exposed grades or otherwise protected against frost action. Foundation subgrades should be checked by a representative of Pennoni to confirm conditions suitable for support of the design bearing pressure. Where an area is questionable, it should be further explored and/or remedied by removal and replacement of unsuitable material.

5.3.2. Concrete-filled Steel Pipe Piles

Concrete-filled steel pipe piles with an outside diameter (OD) of 16 in. and a minimum wall thickness of 0.5 in. driven into the dense to very dense sand and gravel deposit (Stratum 4) can be considered. Our analyses indicate piles installed to the recommended depths can obtain an allowable load carrying capacity in compression up to 125 tons. A temporary increase in the capacity of up to 33% can be applied to transient loads including wind, etc.

Based on the findings of the test borings and our analyses, the pile tips will be located approximately 60 to 80 ft. below the existing grades. The steel pipe pile should conform to ASTM A-252, Grade 3, specifications. The piles should have a flat boot plate of at least 2 in. thickness fully welded at the tip and flush with the outside wall of the pipe (no projection). The minimum pile spacing should be at least 3 times the pile diameter. In addition to the allowable compression capacity recommended above, the vertical piles can be designed for an allowable uplift capacity of 25 tons, and an allowable lateral capacity of 8 tons per pile.



To facilitate pile installations, the piles may be installed by pre-augering through upper portions of fill layer, if necessary. After pre-augering, the piles should be driven into the dense to very dense sands of Stratum 4, to attain the recommended design capacity. The piles should be driven for at least the last 10 ft. of their length to a resistance determined in accordance with Pile Dynamic Analysis (PDA) testing a suitable dynamic formula, such as a WEAP Analysis, and as verified by successful pile load tests. Production piles may be used for load tests.

5.3.3. Auger Cast Piles

Auger Cast Piles (ACIP) can also be considered for support of the proposed structure. This pile type is constructed by first drilling to the pre-determined depth/elevation using a standard continuous flight auger that removes or displaces material. After reaching the design depth, cement grout is injected, under pressure, as the auger is gradually withdrawn, forming an uncased grout shaft. A 28-day compressive strength of at least 5,000 psi is recommended for the cement grout. The pile shaft can be reinforced with one full-length reinforcing bar extending to the bottom and, if necessary, a reinforcing steel cage can be installed into the upper portion of the grout column while the grout is still fluid.

The piles will derive their capacity by a combination of skin friction and end bearing. An 16-in. diameter ACIP pile will have an estimated allowable axial load carrying capacity of 100 tons per pile. These piles should be constructed estimated to depths of 60 to 80 ft. below existing grade. We estimate these piles as described will have tension and lateral capacities on the order of 50 tons and 8 tons per pile, respectively.

Piles designed to resist uplift loads (tension) should have reinforcing steel extending all the way to the pile tip. Moreover, piles subjected to lateral loads should have properly designed reinforcing in the upper portion of the pile shaft. We further recommend that the piles designed to carry uplift and lateral loads be spaced at least 3 pile diameters apart. The final design and/or allowable capacities should be determined by a specialty contractor with adequate experience in auger cast concrete pile design and construction. Production piles may be used for load tests but should failure occur, the pile can no longer be used. The auger cast pile installer is responsible for closely monitoring the pile during the load test and proving the pile was damaged during testing.

5.4. LOAD TESTING

CONCRETE FILLED STEEL PIPE PILES

The Wave Equation analysis should be used to determine the suitability of the proposed driving equipment. The contractor should incorporate the results of the wave equation analysis within any submittals that are due prior to construction for approval. Consideration should be given to performing dynamic monitoring on a minimum of 5% piles using a Pile Driving Analyzer (PDA). The PDA will provide information on the actual driving stresses, verification of ultimate geotechnical resistance, energy transfer efficiency, pile damage assessments, and verify the refusal criteria during pile installation. A minimum factor of safety of 2.25 should be used during the PDA testing to confirm the recommended installed pile capacity. In addition to the PDA we recommend that static load test piles be installed to better define pile length(s) and to confirm/refine pile installation procedures. We recommend that 2 sets of static load tests (axial, tension and lateral) be conducted.



We recommend that the installation of each pile should be monitored and documented by geotechnical personnel under the direct supervision of a professional engineer.

ACIP

Prior to production pile installation, we recommend that test piles be installed to better define pile length(s) and to confirm/refine pile installation procedures. We recommend that 2 sets of static load tests (axial, tension and lateral) be conducted and dynamic tests conducted on 5% of the production piles. The dynamic integrity testing for the auger cast piles should consist of Pile Integrity Testing (PIT) to confirm the construction of the piles.

GENERAL PILE LOAD TESTING RECOMMENDATIONS

The proposed pipe and auger cast piles are essentially a combination of tip bearing and/or friction piles. The load tests must verify a safe load carrying capacity and they must demonstrate that only a very small net settlement will occur while the full design load is carried by the pile. Therefore, the load test should be conducted in such a fashion and provided with such instrumentation that the loads carried by the pile shaft and pile tip, and the strains of the top, mid-point, and base of the test pile can be measured, where feasible.

The maximum test load should be not less than specified by Code and it is recommended to be higher to facilitate total load transfer to the tip of the pile. Experience has shown that testing a pile to a load greater than the Code requirement, although costlier initially, can prove advantageous during installation because of inconsistencies during construction. Therefore, we recommend that a maximum test load at least 2.5 times the maximum design load carrying capacity of the selected pile should be considered for evaluating maximum load carrying capabilities and load-settlement relationships.

Static and dynamic load tests should be conducted in accordance with the provisions of the latest version of the ASTM Standards. For static testing instrumentation, load test set-up, and loading procedures should be governed by ASTM D-1143 except that the procedures described under "Apparatus for Measuring Movements", "Lateral Movements", and "Incremental Loading Procedures" should be mandatory. PDA testing on driven piles should be performed in accordance with ASTM D-4945.

The geotechnical engineer should select load test locations. Load tests should not be production piles; if the pile/soil interface is failed during testing it will no longer be capable of supporting loads. No construction activity transmitting vibratory or impact loads should be permitted on the project site during load testing. The load test set-up should be protected from inclement weather (wind, rain, intense heat, sunlight, etc.), provided with lights for nighttime readings, and guarded on a full-time basis.

Technical details of the intended pile installation equipment and of the load test set-up (sketch, description, etc.) together with certification of the loading device, etc. should be submitted to the geotechnical engineer at least 1 week in advance of load test construction. Each load test must be monitored on a full-time basis and test results analyzed by a registered geotechnical engineer.



5.5. SETTLEMENT

Settlement of a soil mass is a function of the characteristics of the supporting materials and the stresses imposed on the soils from an external source. Our calculations indicate that settlements will occur due to the stresses imposed on the subsoils by newly placed load bearing fill for site fills and are proportional to the amount of pressure applied (fill height). Additionally, the organic layer of soil was determined to contain approximately 26% of organic material. Long term, secondary settlement is also anticipated in this layer as the material breaks down and consolidates.

The fill heights and secondary settlement may lead to uneven settlement below the floor slab. Therefore, consideration should be given to suspending the utilities from the structural slabs to prevent any serious differential movements in different portions of the utilities. Moreover, flexible connections should be used where the suspended pipes meet the outside pipelines not supported by piling.

Provided the building and structural slab are supported on deep foundations (driven piles, ACIP piles), determinantal total and differential settlements are not anticipated.

5.6. STRUCTURAL SLAB

Because of the differential settlement tolerances the ground floor slab should be designed as structural slab supported by piles and grade beams or they should be designed as "flat plates" supported by piles. The required new fill to attain the finish ground floor subgrade level should be placed as recommended in the Earthwork Section 5.2 to serve as an underside form for slab construction, but it will eventually settle away from the bottoms of the slabs due to consolidation of the compressible organic silt layers.

5.7. GROUND WATER AND SURFACE WATER MANAGEMENT

Observations for groundwater made in each test pit and boring indicate that water was generally encountered 6 to 13 ft. below existing grades. Water table fluctuations may occur with the tidal action of Delaware River. Static water levels could affect utility installation if they are proposed at depths greater than the Mean High Water (MHW) Elevation. The use of sumps and pumps should be expected; well points and/or a sheeting/shoring system comprised of steel interlocking sheeting and high capacity pumps may be required to control ground water during utility installation in deeper excavations (>5 ft. deep).

Surface runoff should be prevented from entering or ponding in excavations by creating soil berms or diversion swales along the perimeter, if the excavation will be left open for an extended period. Where ponding does occur, the water should be removed immediately by pumping. Grades should then be established to prevent further ponding.

5.8. LATERAL EARTH PRESSURE PARAMETERS

The soil parameters presented in Table 1 can be used to estimate earth pressures to design below grade structures and temporary shoring. If the top of the structure is restrained from movement, thereby preventing the mobilization of active soil pressures, the structure should be designed using the at-rest pressure coefficient.



The earth pressure coefficients are based on the assumption of vertical walls, horizontal backfill, no surcharges, no wall friction, and a safety factor of 1.0. A clear distance of 10 ft should be maintained during construction, between perimeter walls and stored materials or the wall must be design to resist the surcharge load from the stored materials. Where sufficient drainage cannot be provided to intercept and re-direct seepage and perched water from structures, hydrostatic pressures must also be considered in the design.

	Strata 🔰						
Parameter	F	1	2	3	4	5	Processed Aggregate (PennDOT Type 2A)
Unit Weight (pcf)	120	100	90	125	130	118	135
Angle of Internal Friction (degrees)	28	17	23	32	38	32	38
Cohesion (psf)	-	200	0	-	- \	1000	-
Friction Factor (concrete)	0.35	0.20	0.20	0.40	0.50	0.40	0.50
Friction Factor (steel)	0.25	0.20	0.20	0.25	0.30	0.25	0.30
ka	0.36	0.55	0.44	0.31	0.24	0.31	0.24
k _o	0.53	0.71	0.61 💊	0.47	0.38	0.47	0.38
kp	2.77	1.83	2.28	3.25	4.20	3.25	4.20

5.9. CONSTRUCTION DIFFICULTIES

Experience has shown that remnant construction and obstructions are often encountered when building within similar, previously developed urban sites. Encountering remnants of previous foundations and shoring systems should be expected. If encountered, these obstructions will most likely impair the construction process. Existing foundations or other structural components disclosed should be removed to a minimum depth of 18 in. below the bottom of new ground floor slabs and 36 in. below the bottom of new foundations.

6. RECOMMENDATIONS FOR FURTHER GEOTECHNICAL SERVICES

Our experience on numerous construction projects is that the interests of the project team are best served by retaining the Geotechnical Engineer to provide construction observations during earthwork and foundation construction operations. To determine if soils, other materials, and ground water conditions encountered during construction are similar to those encountered in the borings and test pits, and that they have comparable engineering properties or influences on the design of the structures, we recommend that Pennoni should provide field observation services during pile driving and load testing, and excavation; construction of compacted fill; preparation of foundation, floor slabs, and pavement subgrades; and installation/construction of foundations, floor slabs, and pavements. Pennoni's Geotechnical Technology should review specifications for earthwork and foundation design/construction when they are prepared.



May 13, 2019

7. LIMITATIONS

This work has been done in accordance with our authorized scope of work and in accordance with generally accepted professional practice in the fields of geotechnical and foundation engineering. This warranty is in lieu of all other warranties either expressed or implied. Our conclusions and recommendations are based on the data revealed by this exploration. We are not responsible for any conclusions or opinions drawn from the data included herein, other than those specifically stated, nor are the recommendations presented in this report intended for direct use as construction specifications.

This report is intended for use with regard to the specific project described herein; any changes in loads, structures, or locations should be brought to our attention so that we may determine how they may affect our conclusions. An attempt has been made to provide for normal contingencies but the possibility remains that unexpected conditions may be encountered during construction. If this should occur, or if additional or contradictory data are revealed in the future, we should be notified so that modifications to this report can be made, if necessary. If we do not review relevant construction documents and witness the relevant construction operations, then we cannot be responsible for any problems that may result from misinterpretation or misunderstanding of this report or failure to comply with our recommendations.

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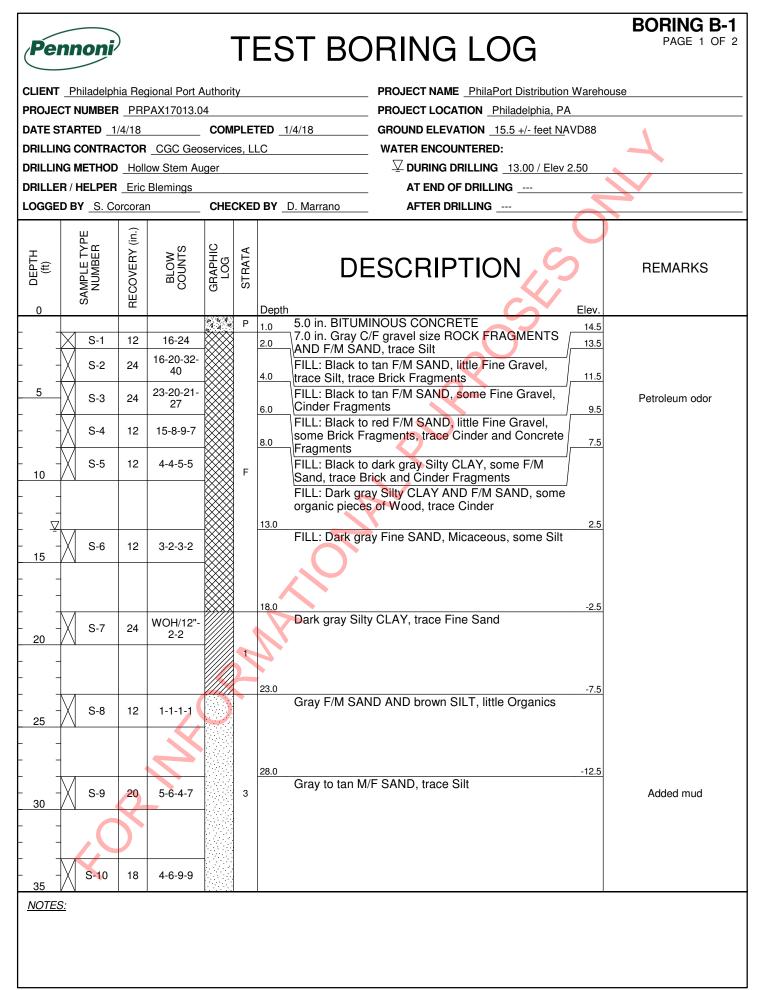


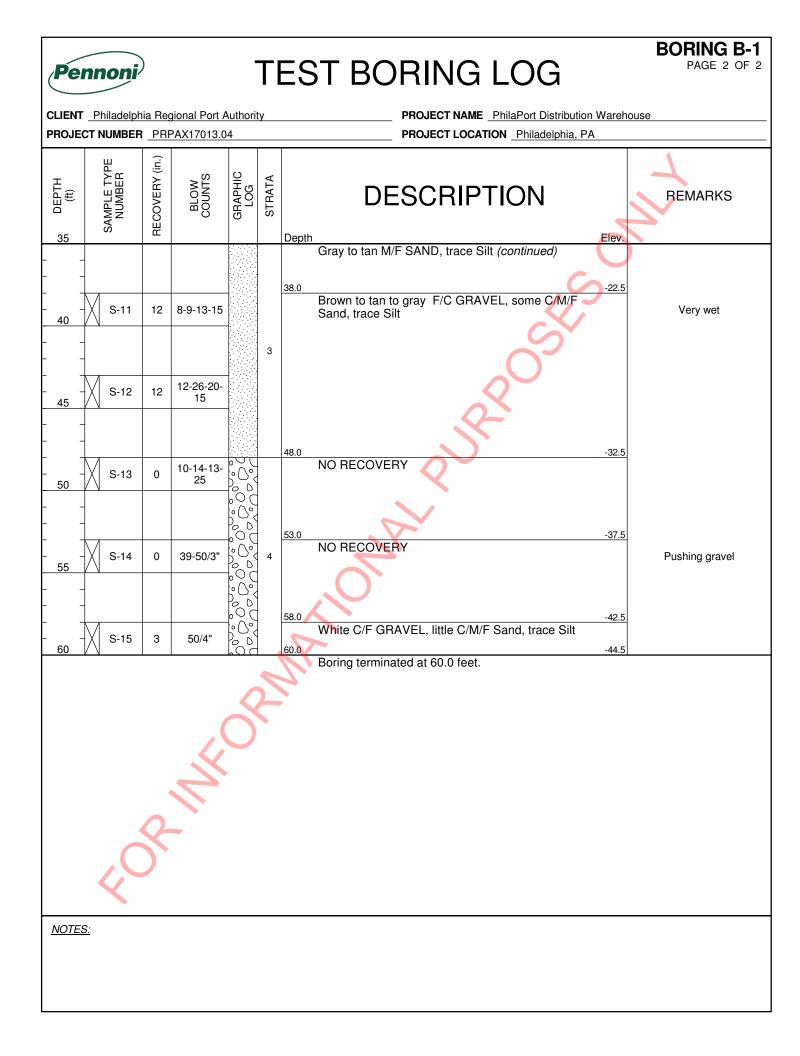
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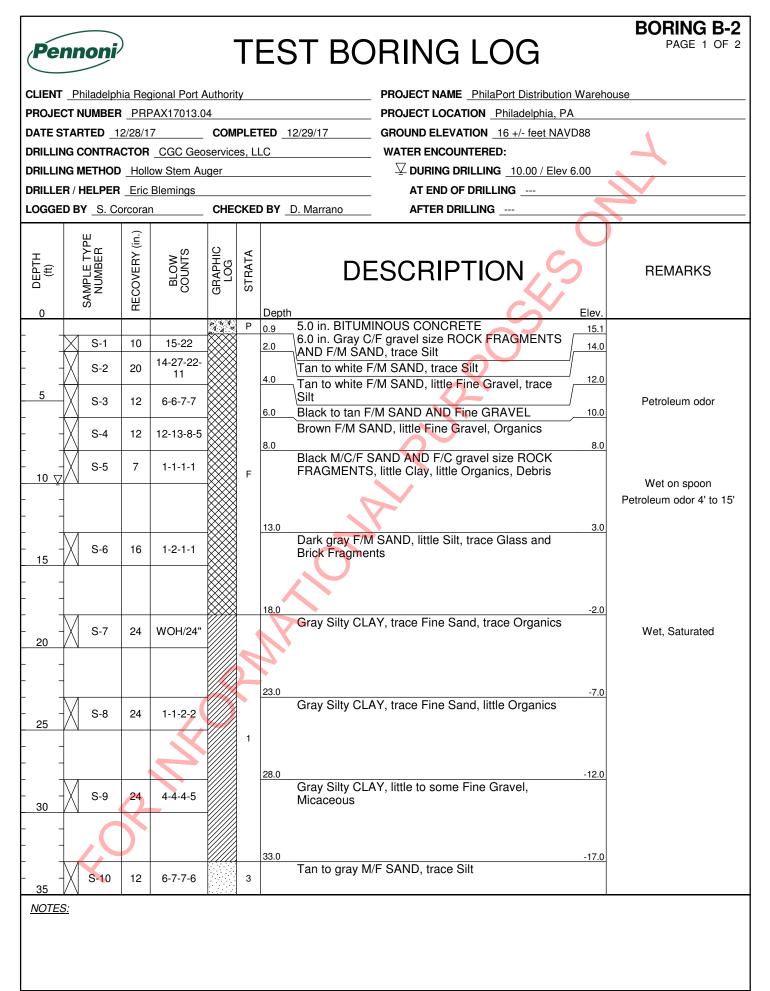


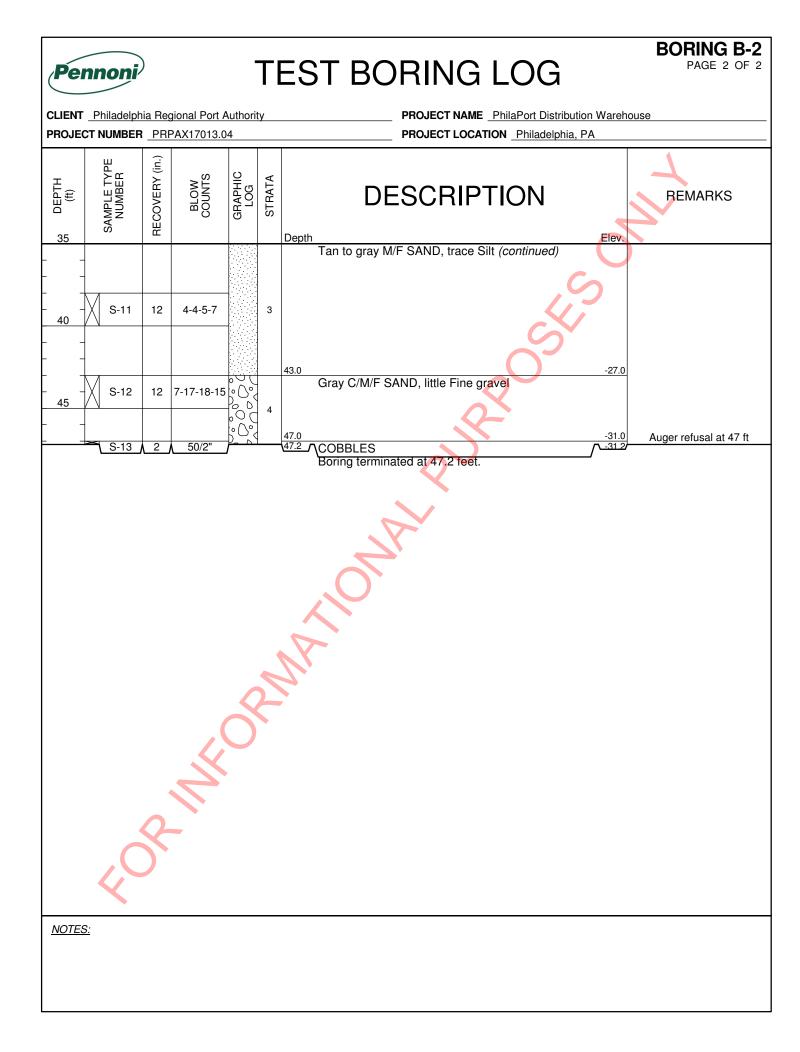
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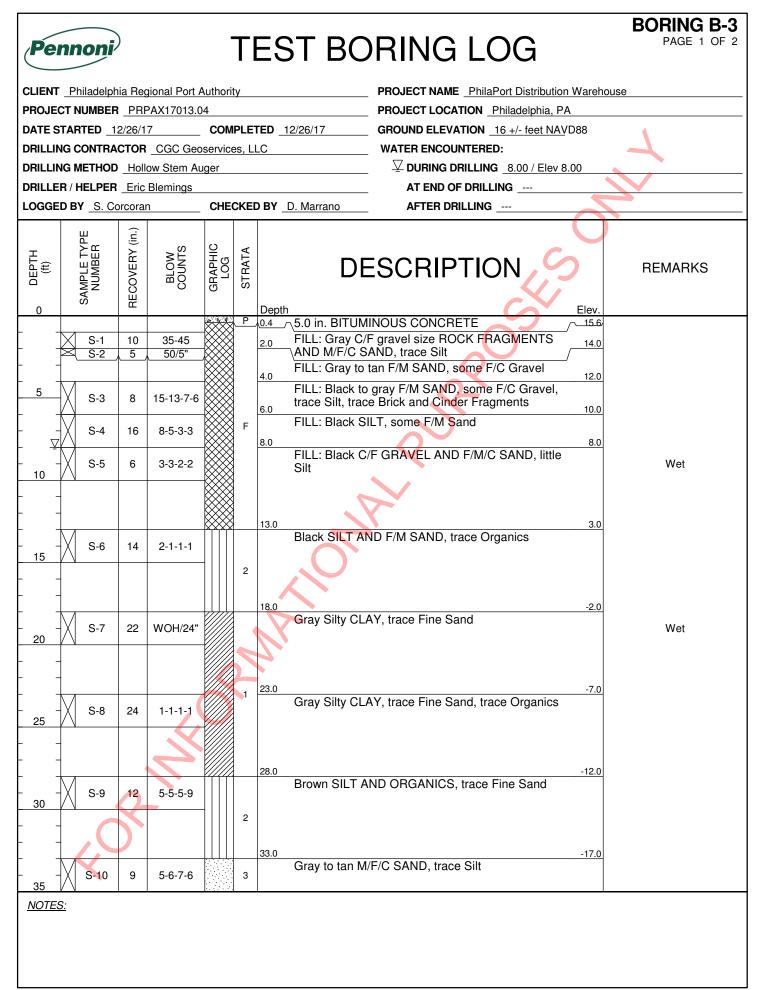


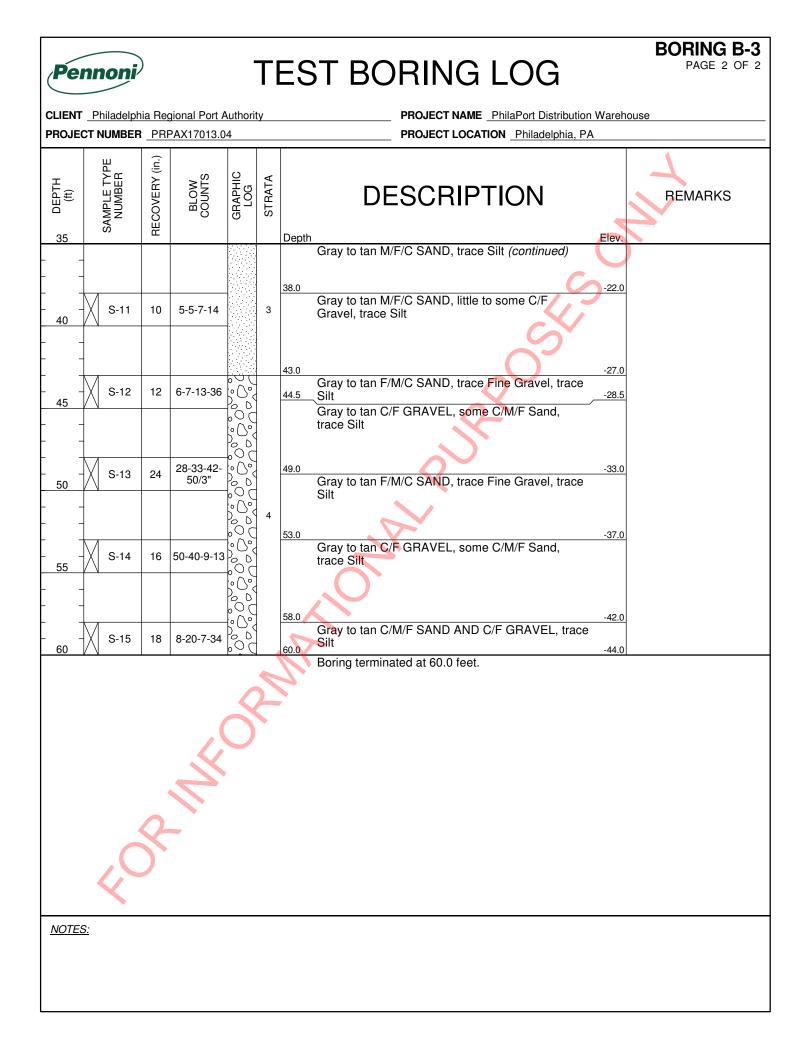


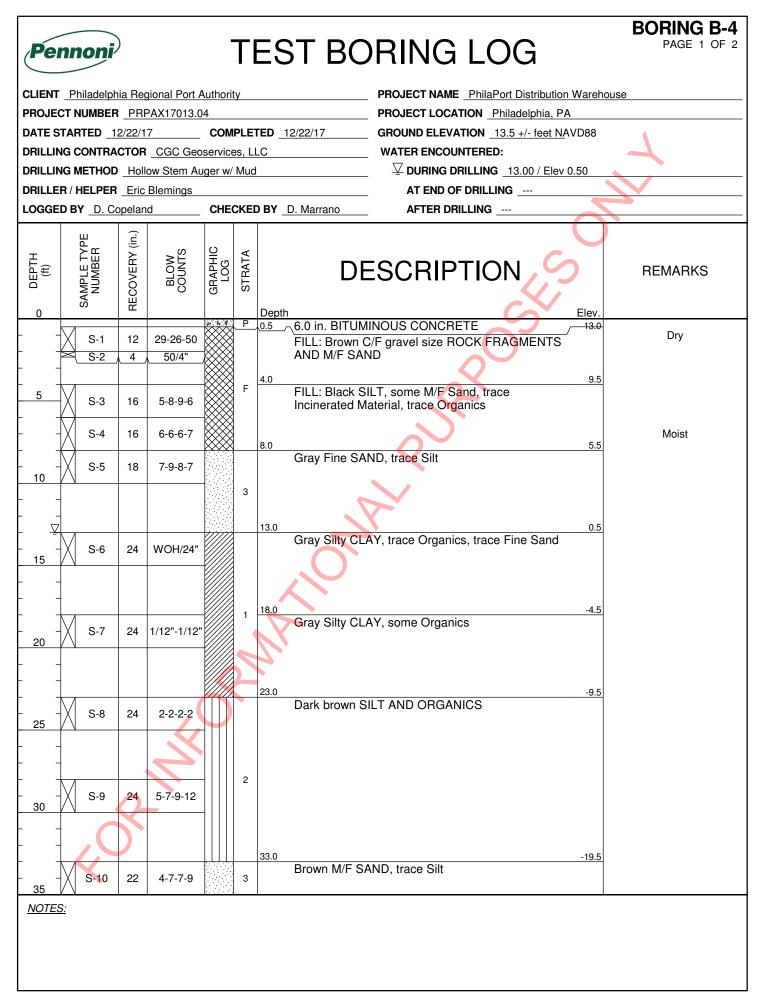


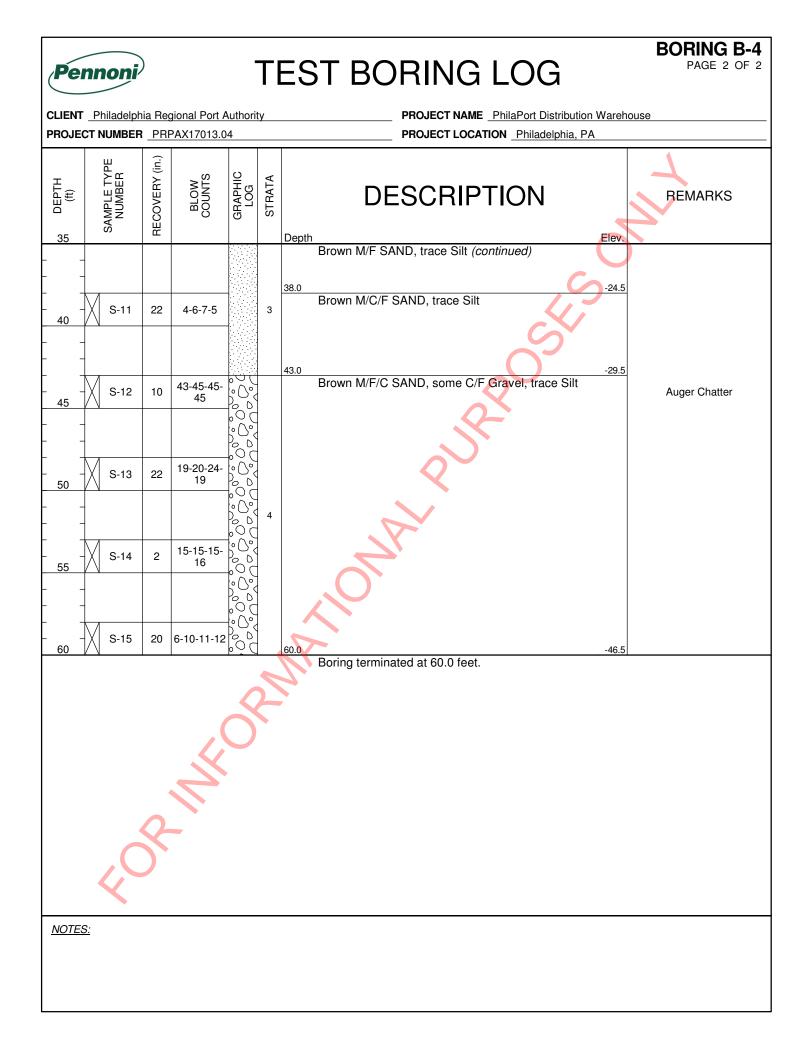


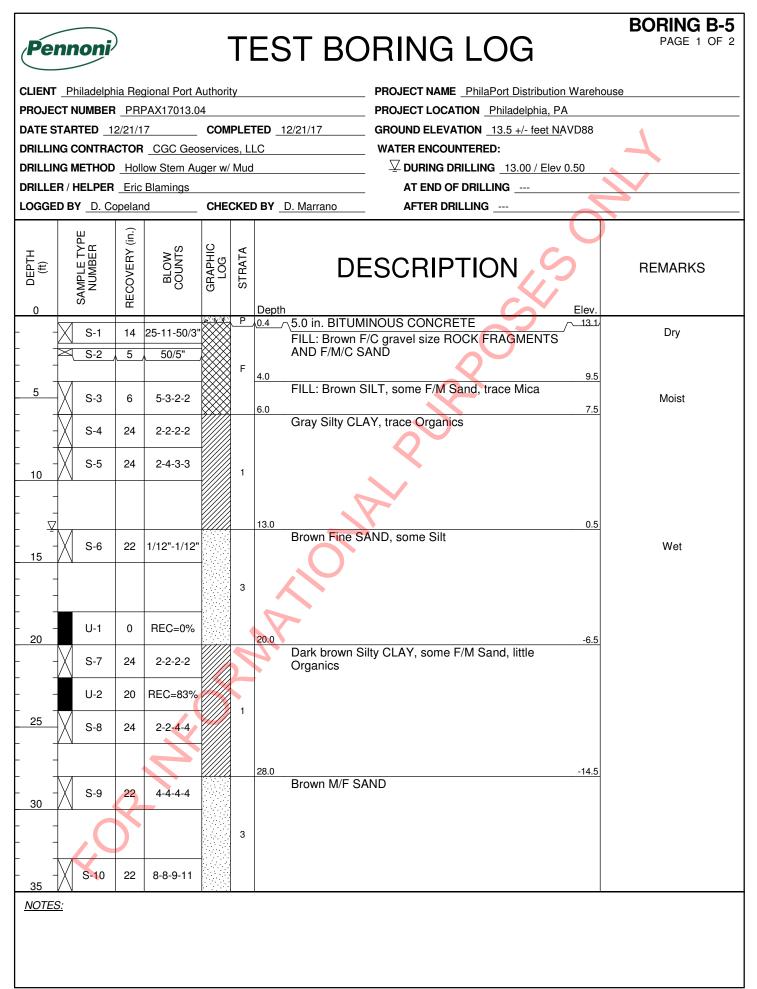


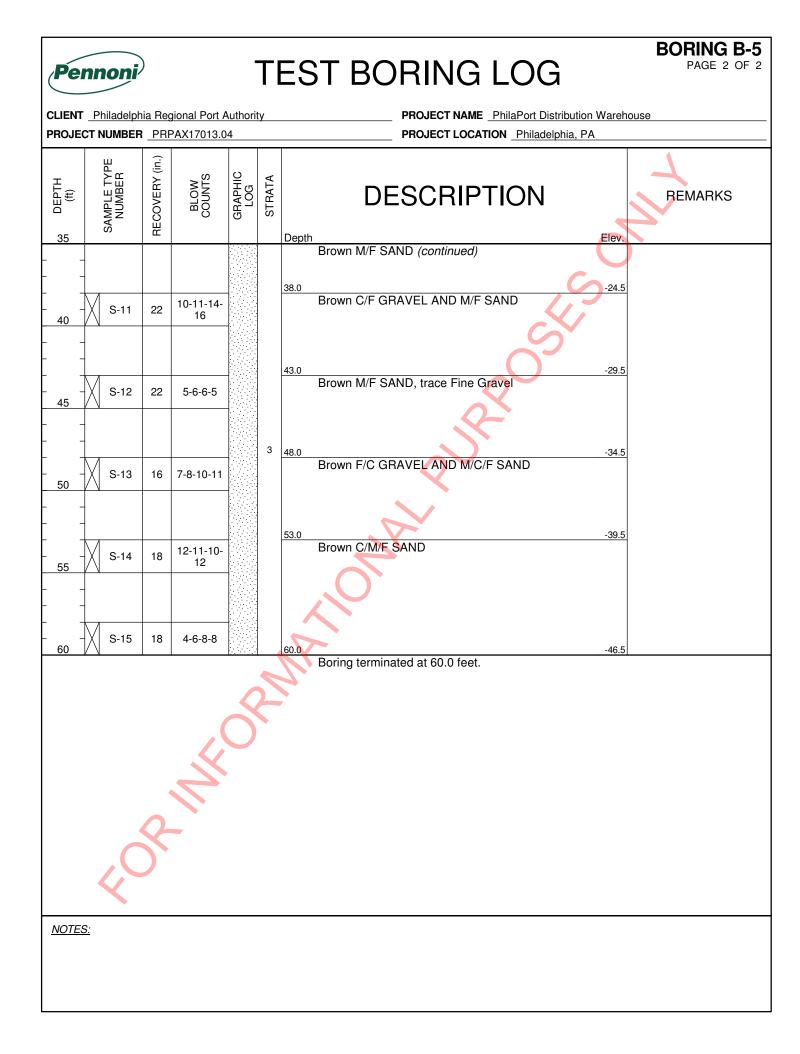


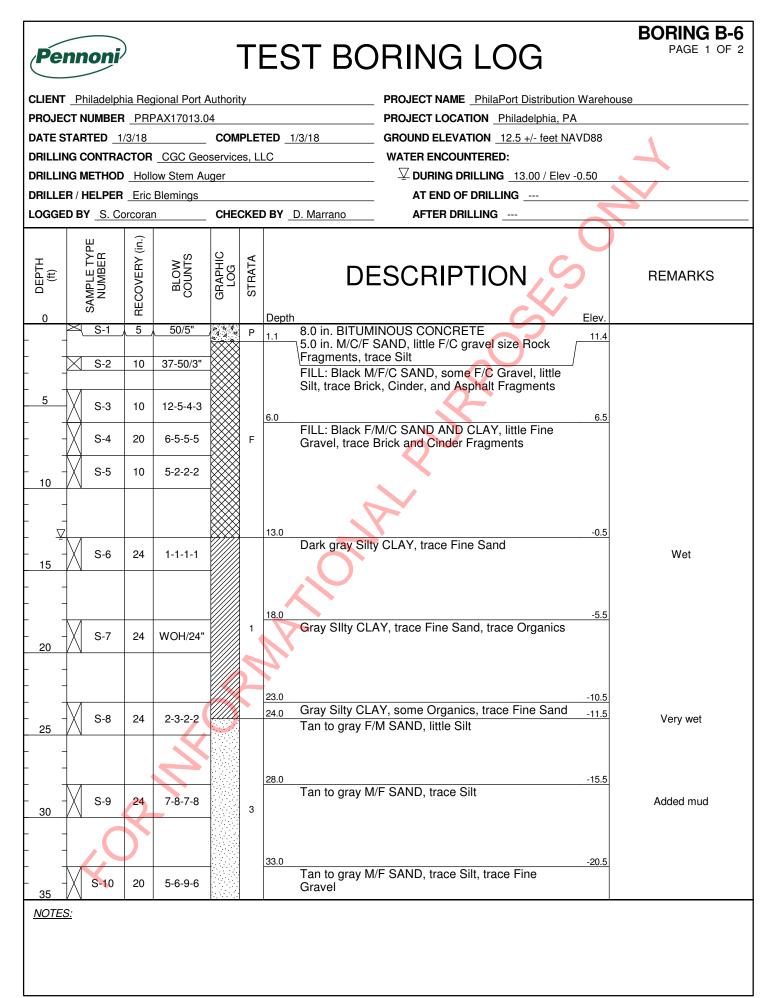


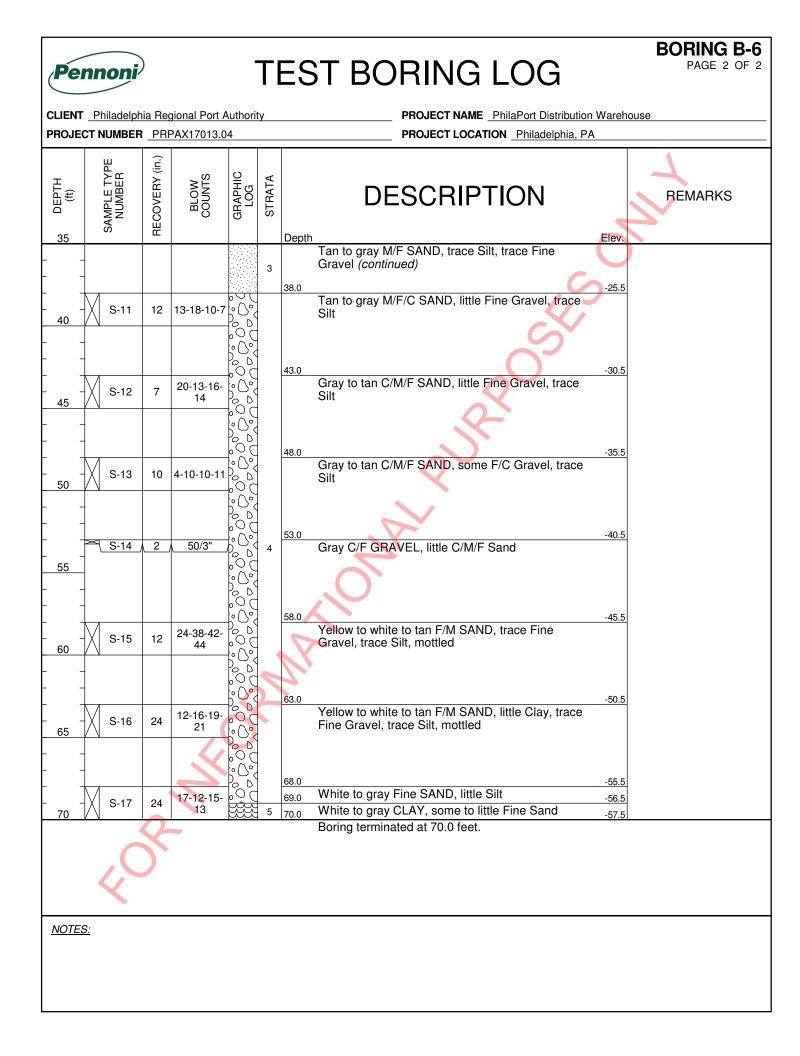


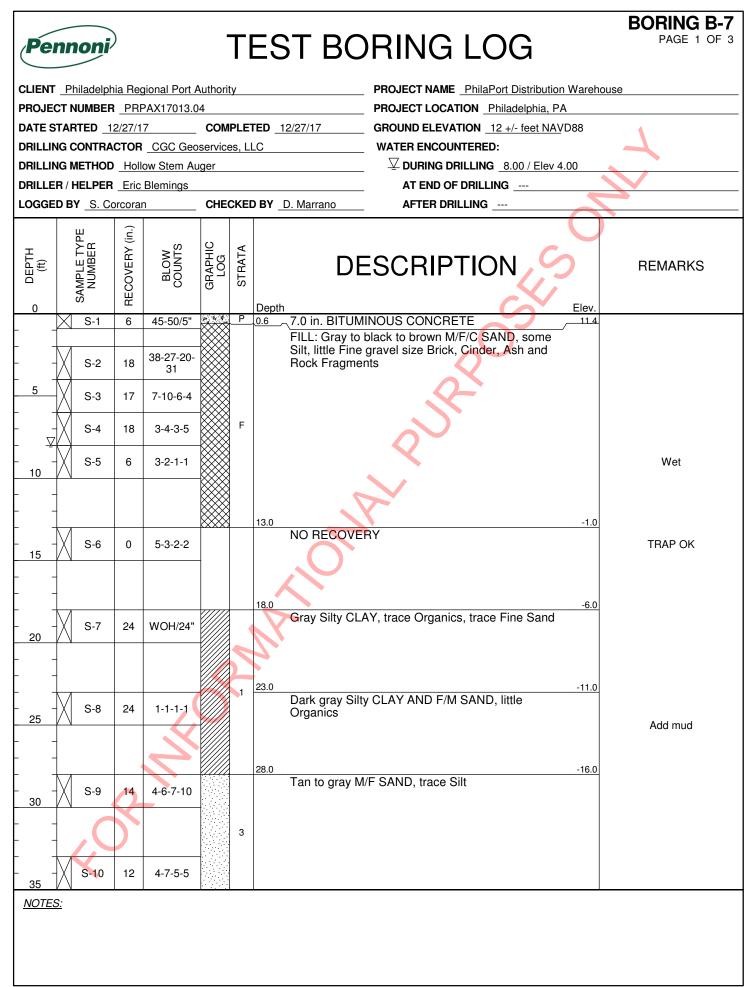


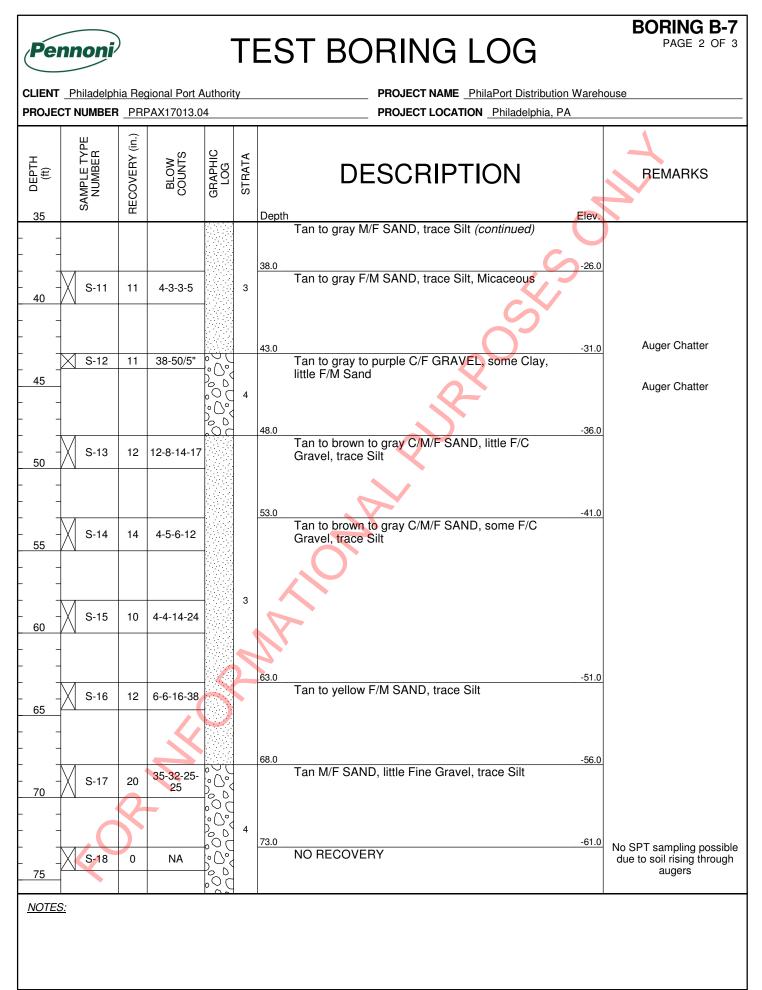


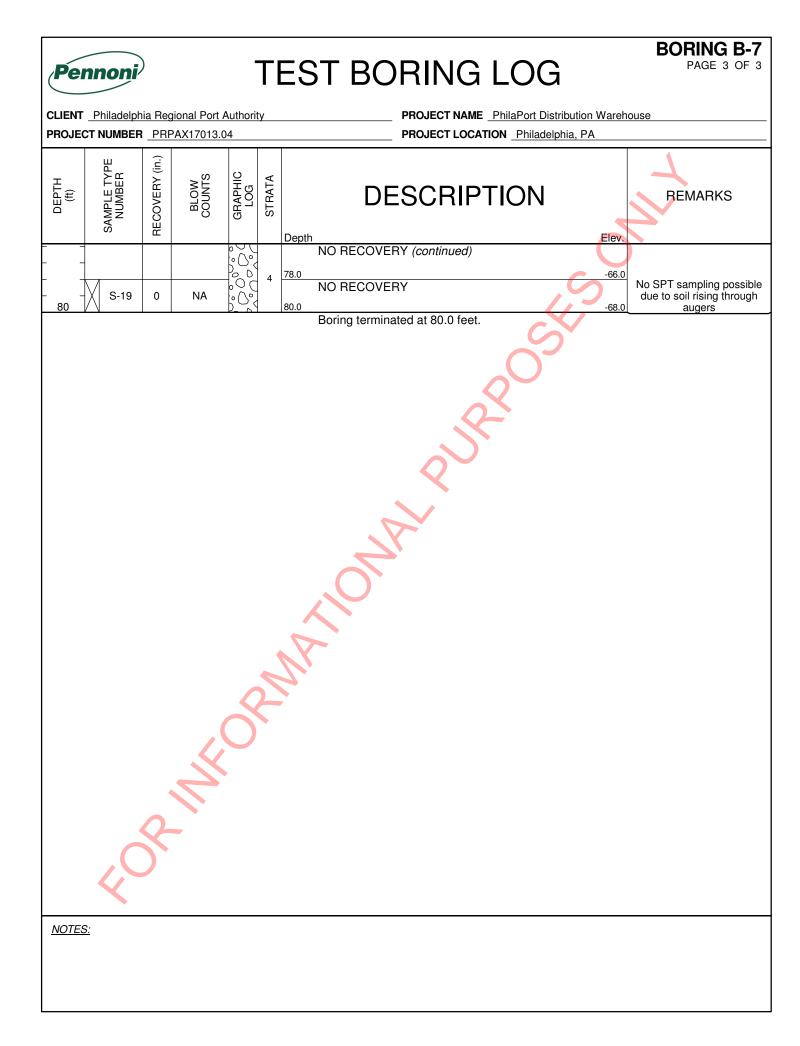


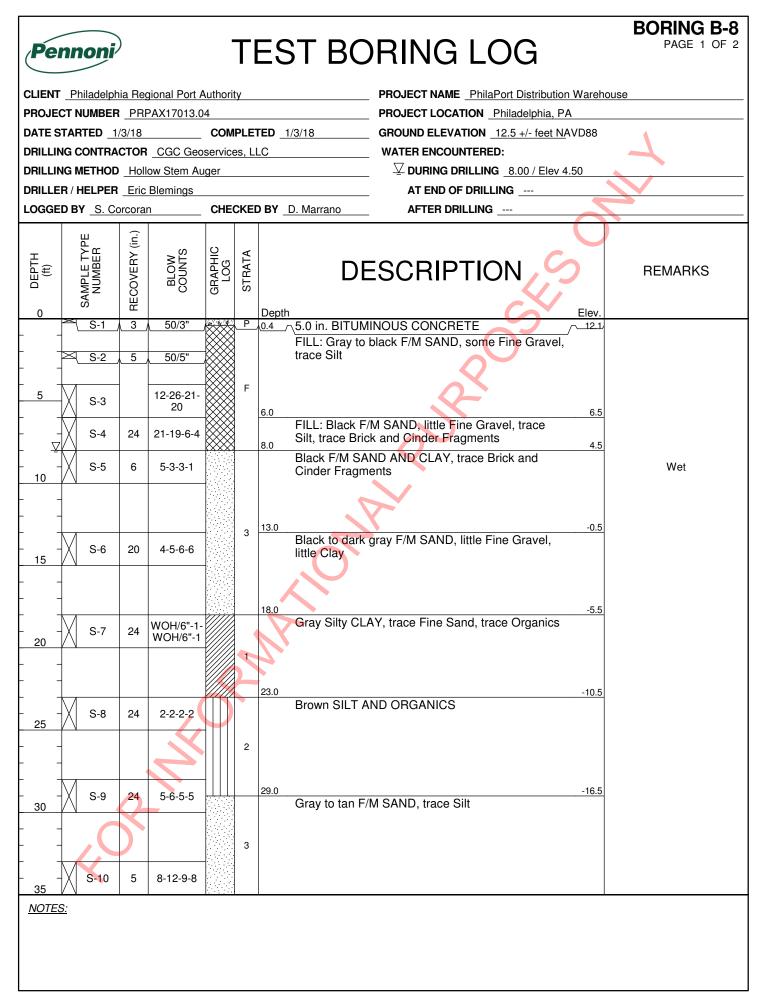


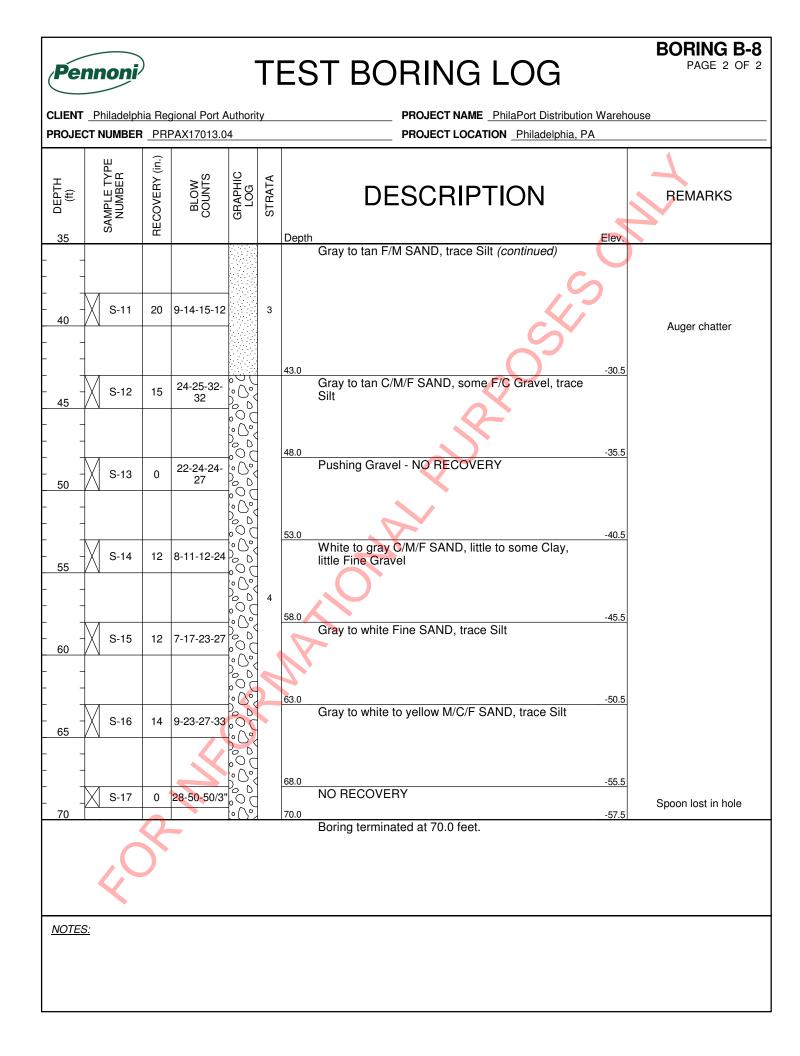


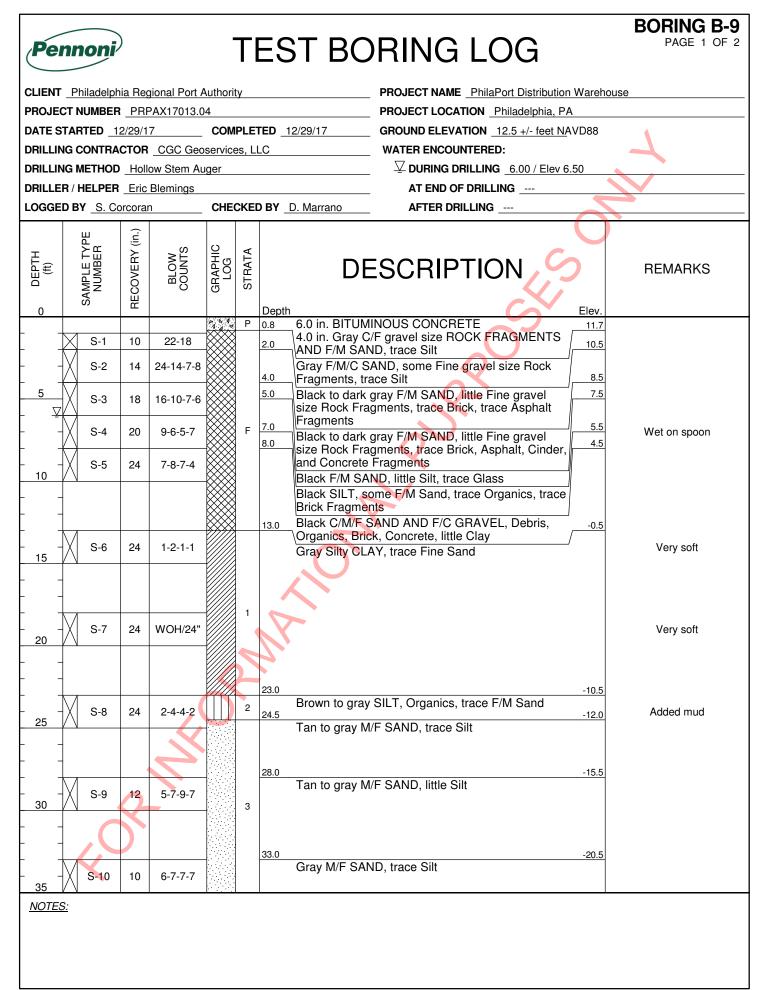


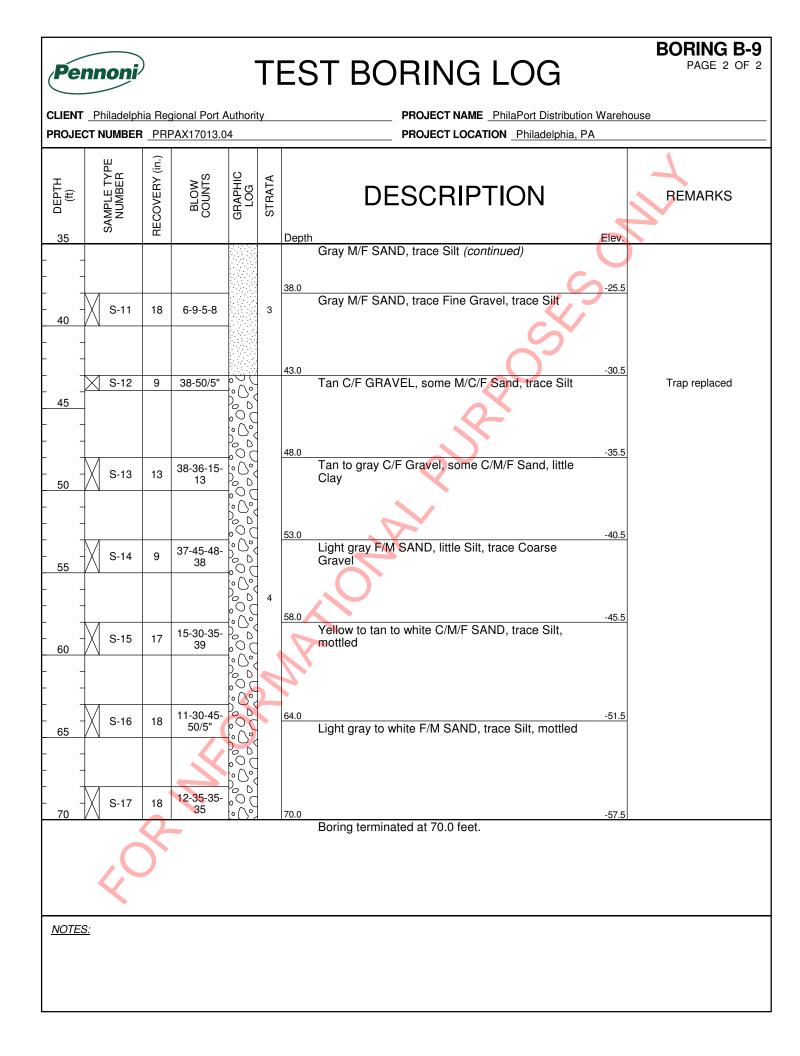


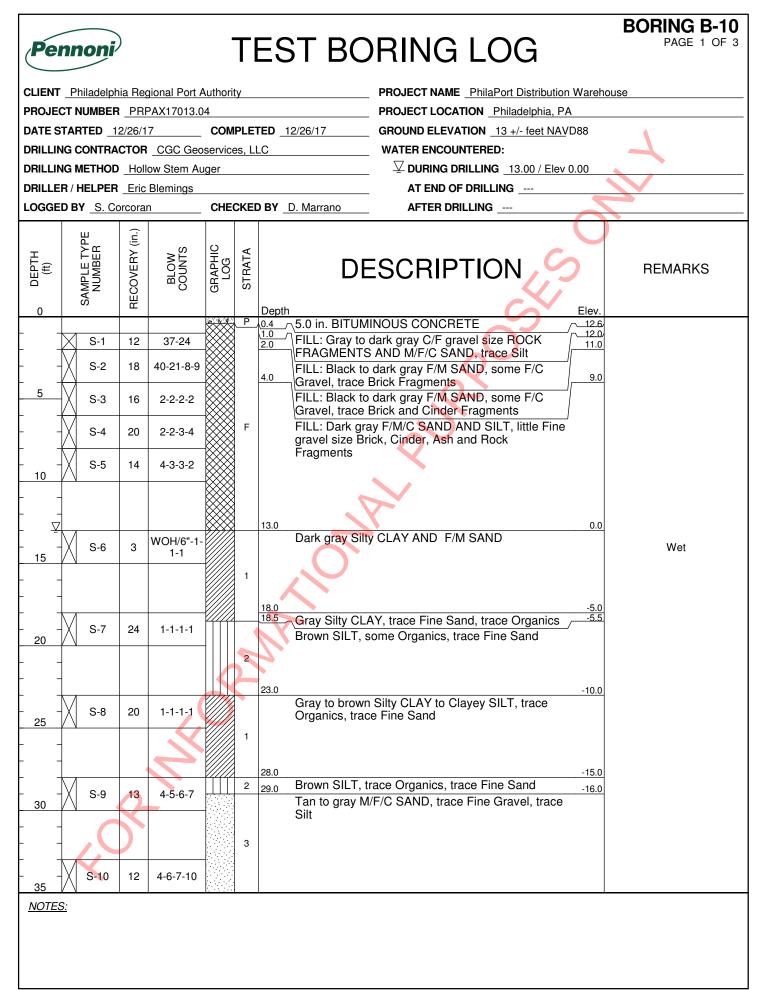


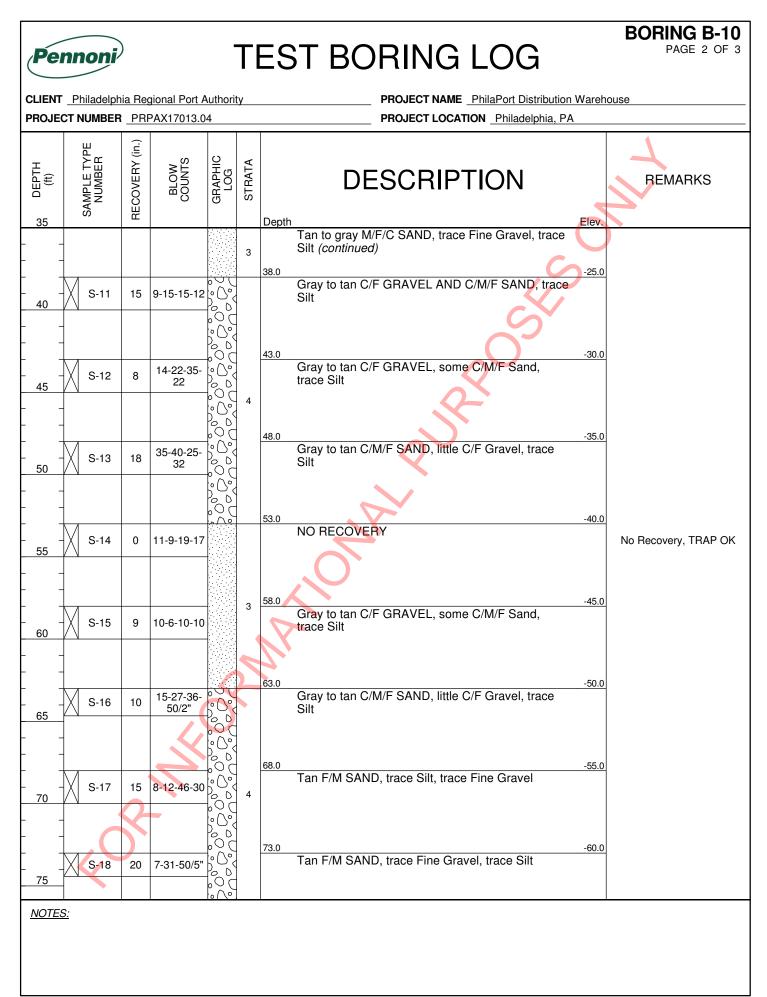






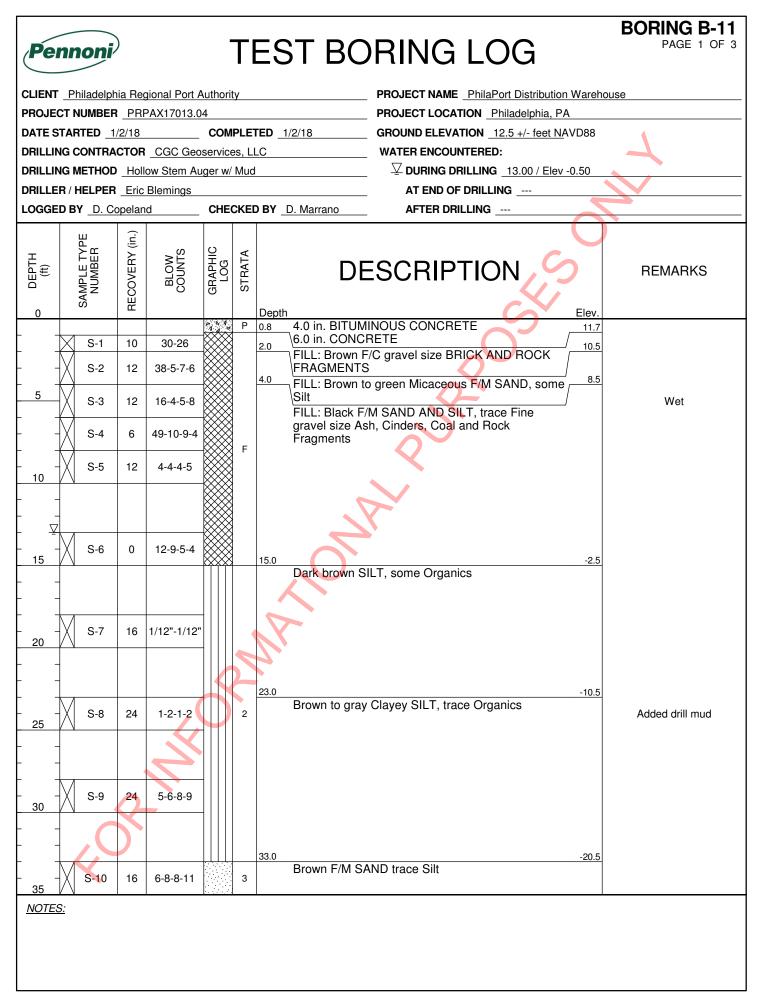


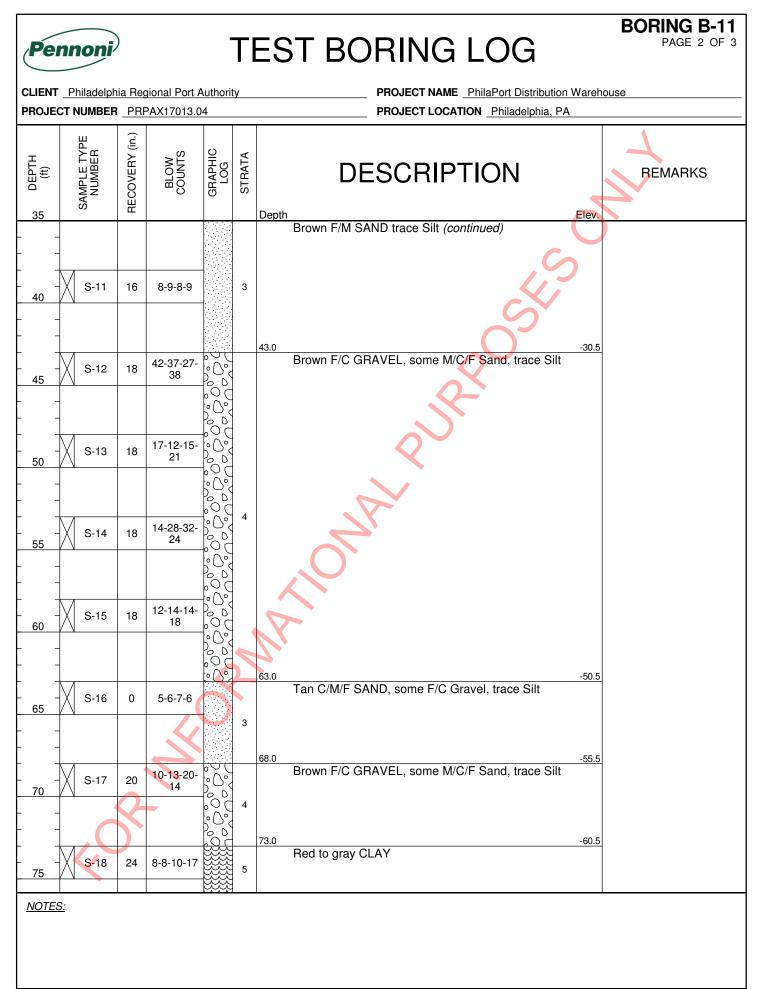




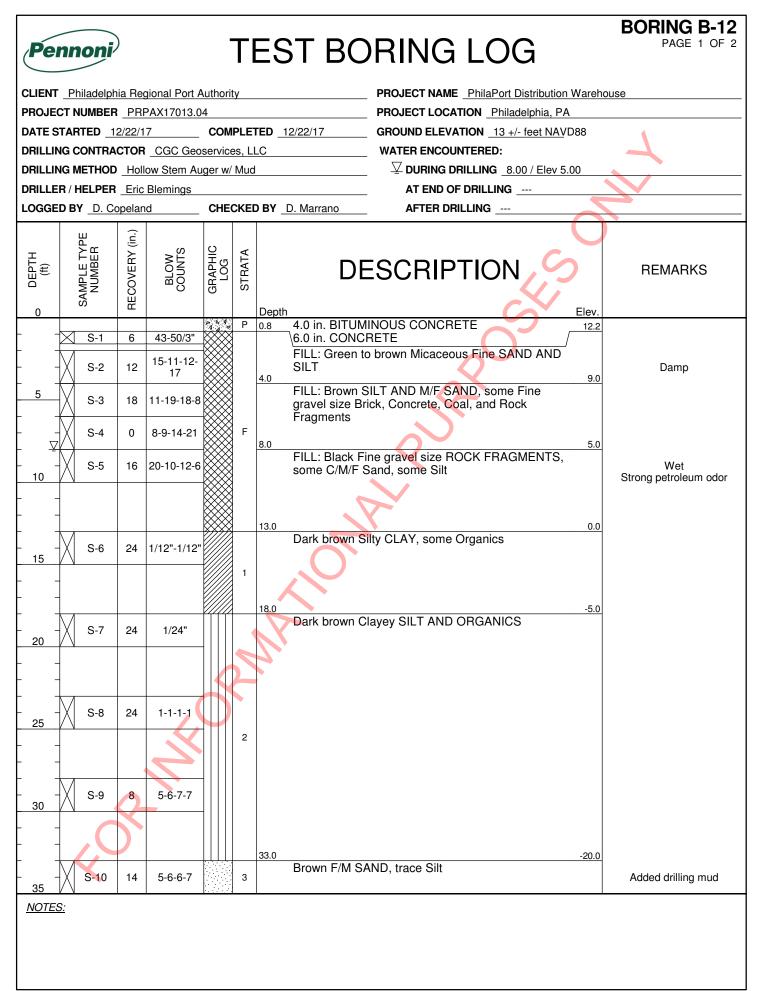
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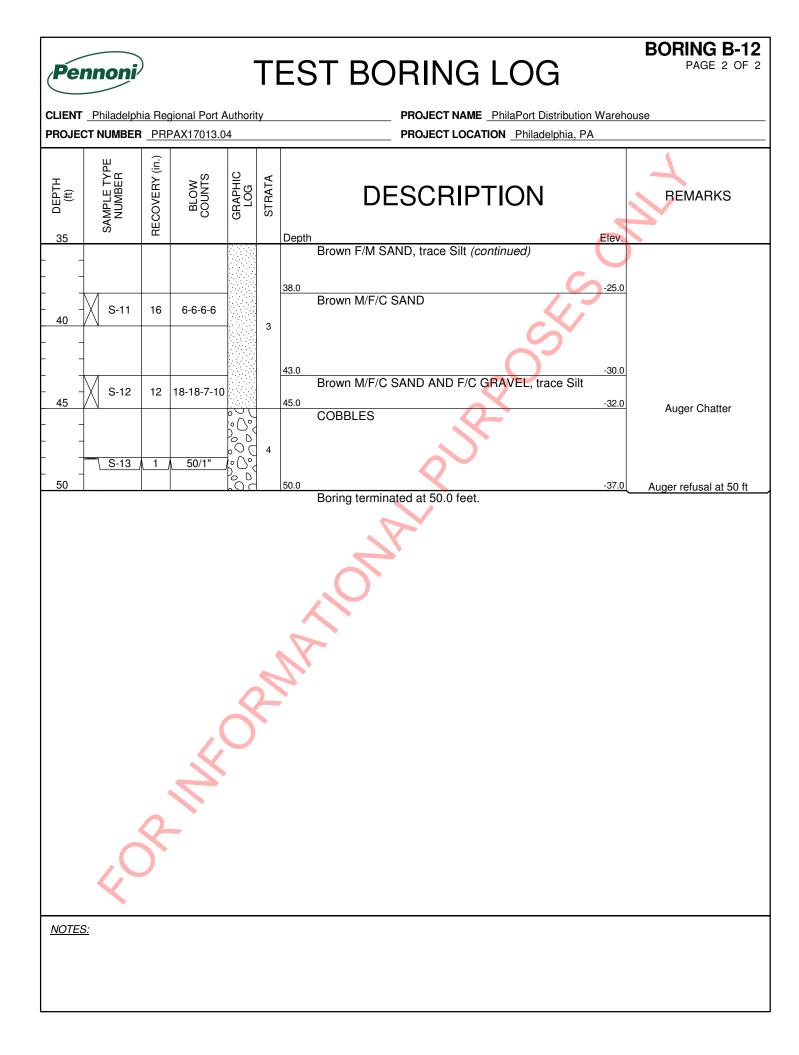
Per	nnoni)		•	Т	EST BORING LOG	BORING B-10 PAGE 3 OF 3
	Philadelph	ia Reg	gional Port A			PROJECT NAME _ PhilaPort Distribution Ware	house
	CT NUMBER					PROJECT LOCATION Philadelphia, PA	
DEPTH (ft)	SAMPLE TYPE NUMBER	RECOVERY (in.)	BLOW COUNTS	GRAPHIC LOG	STRATA		REMARKS
					4	Tan F/M SAND, trace Fine Gravel, trace Silt (continued)	
	S-19	18	5-6-7-7		5	Red to white to purple Silty CLAY, trace Fine Sand	
NOTES	K C	\$				Boring terminated at 80.0 feet.	0

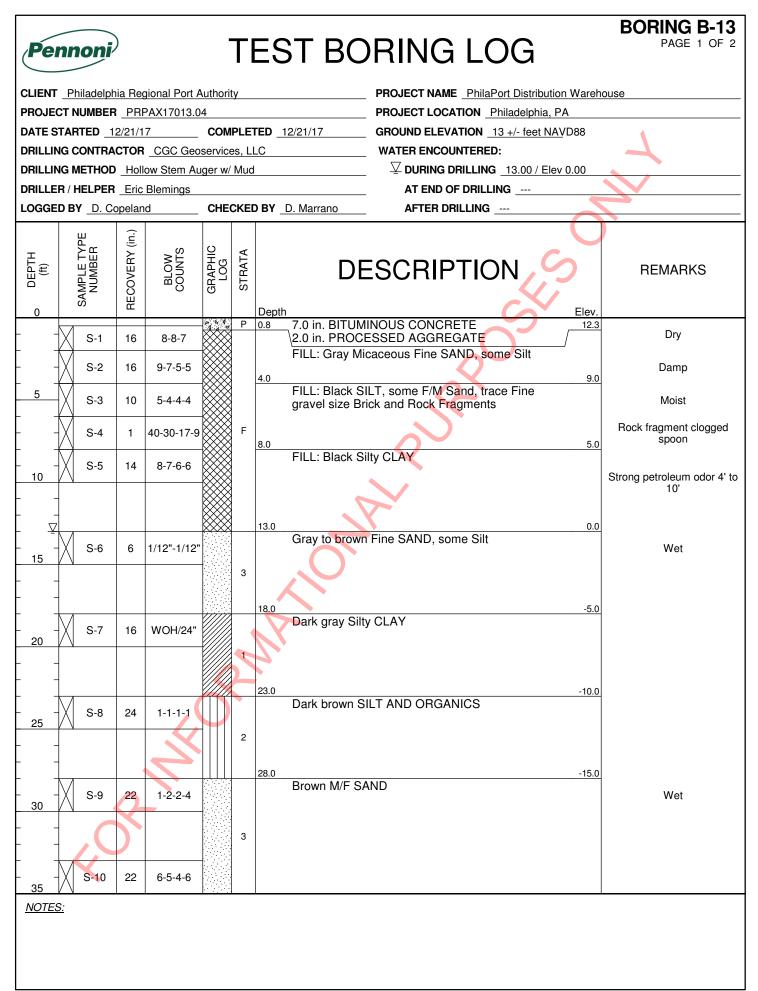


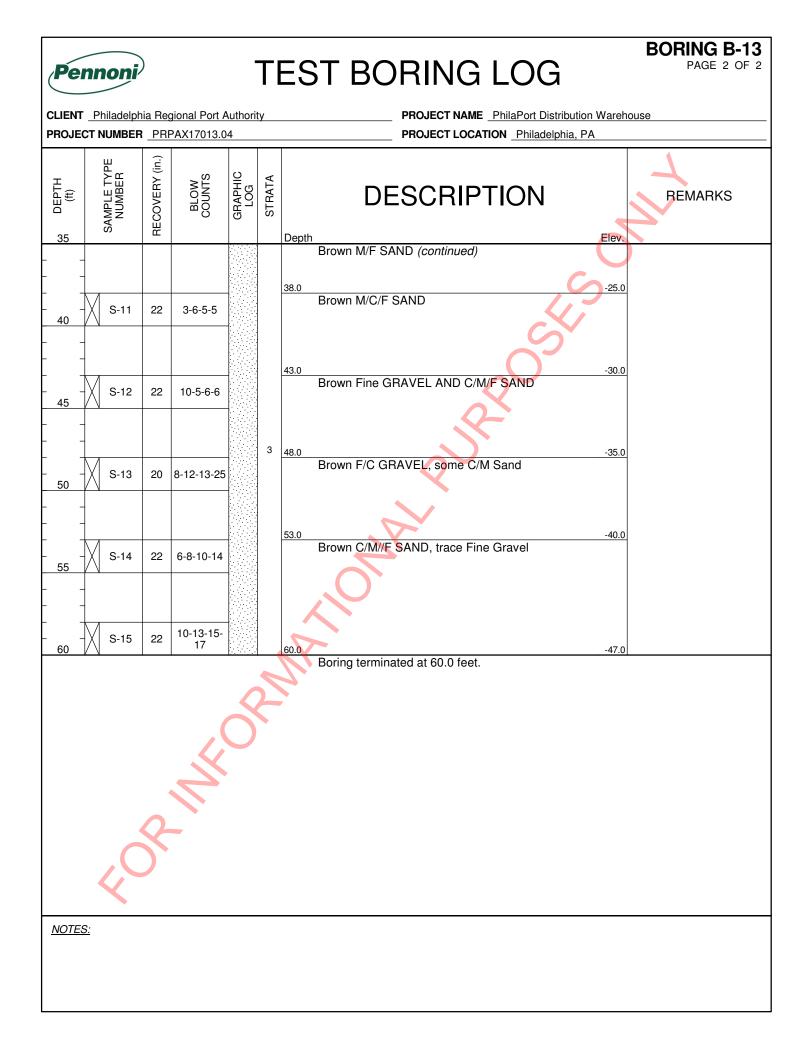


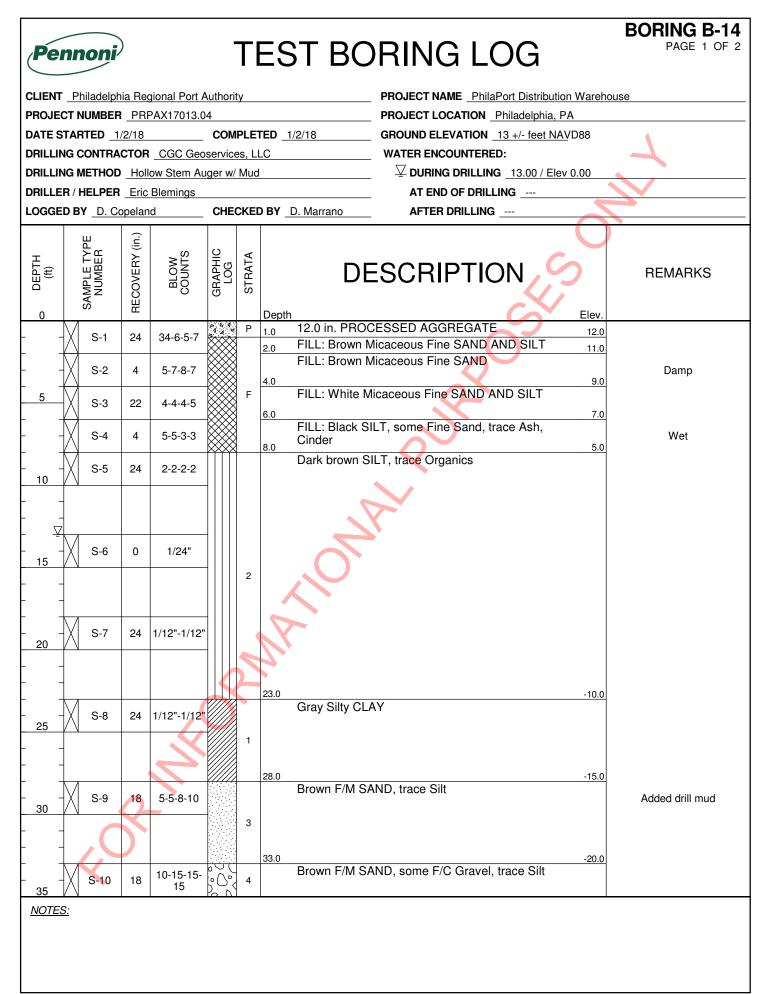
Pe	nnoni)		•	TI	EST BORING LOG BORING B-11 PAGE 3 OF 3
	Philadelph				ty	PROJECT NAME PhilaPort Distribution Warehouse PROJECT LOCATION Philadelphia, PA
DEPTH (ft)	SAMPLE TYPE NUMBER	RECOVERY (in.)	BLOW COUNTS	GRAPHIC LOG	STRATA	DESCRIPTION BEMARKS
 <u>- 80</u>	- S-19	24	6-6-9-14		5	Red to gray CLAY <i>(continued)</i> ^{80.0} Boring terminated at 80.0 feet.
NOTE		\$		3		MALONAL

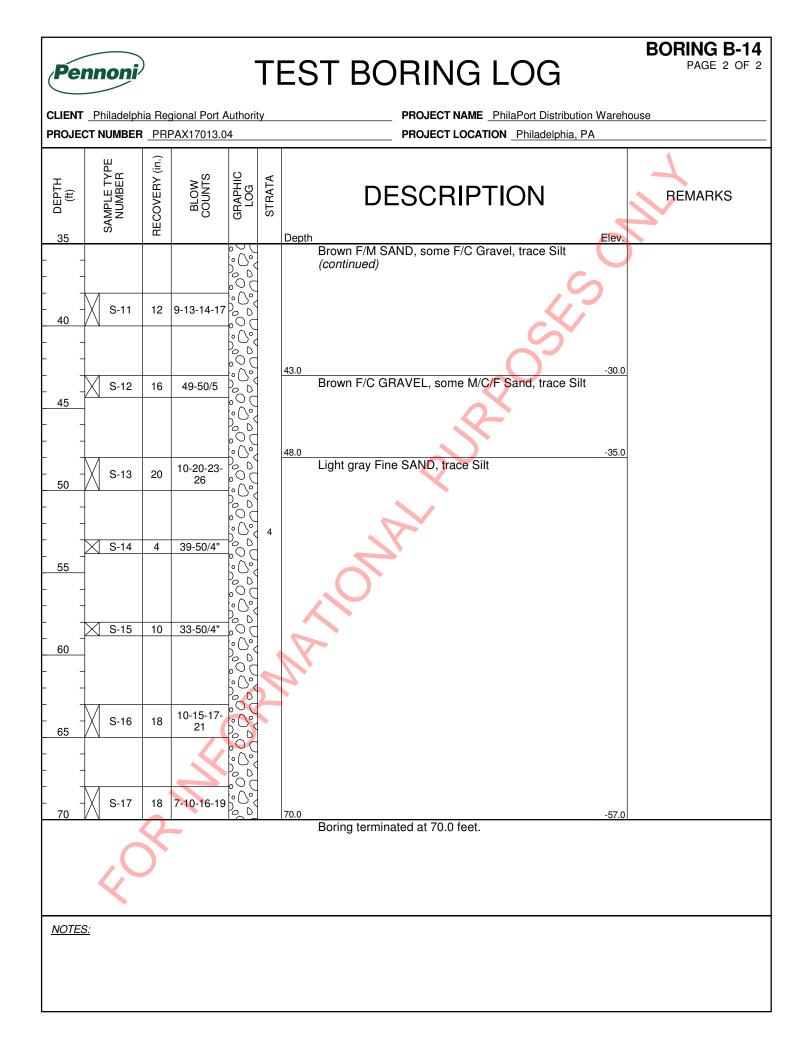


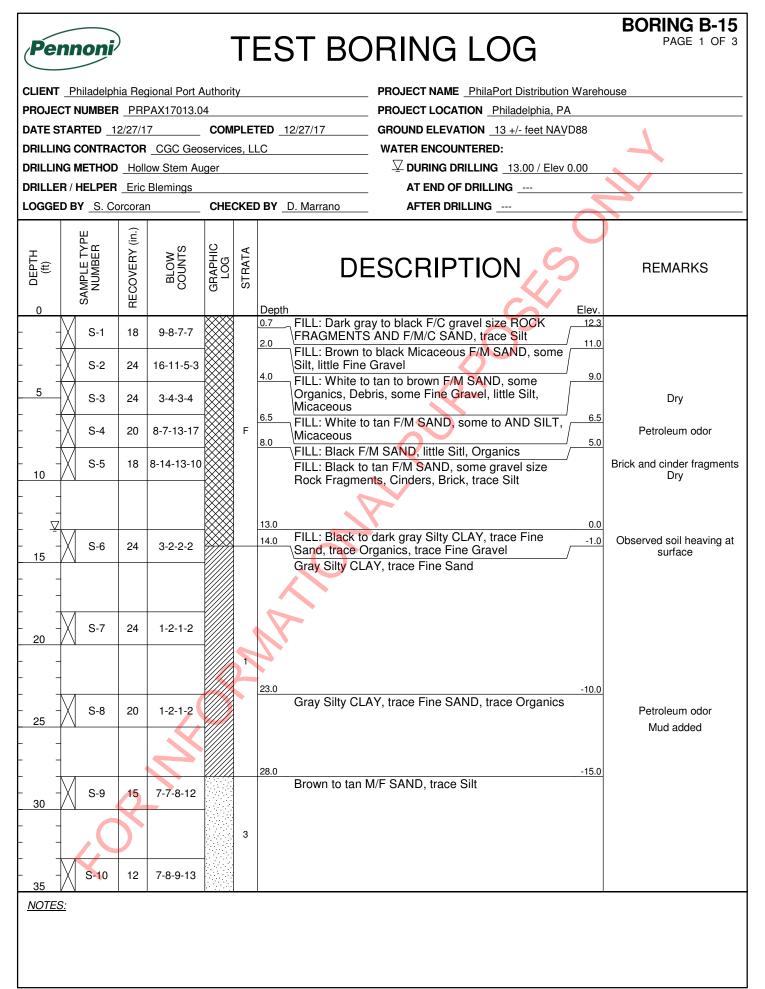


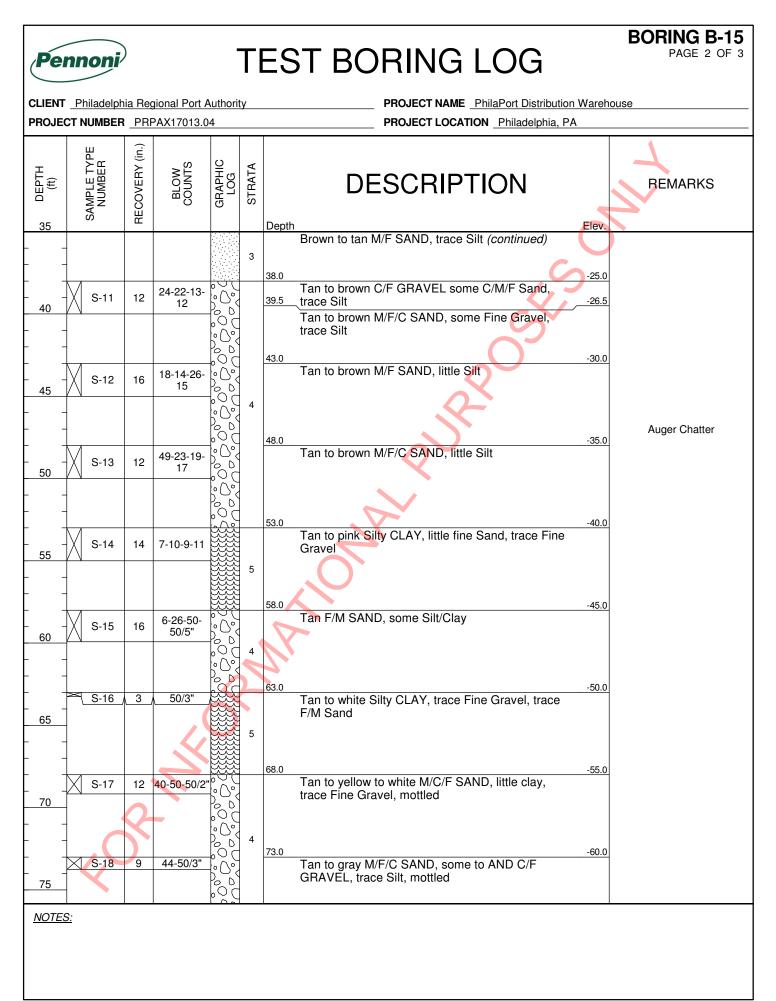




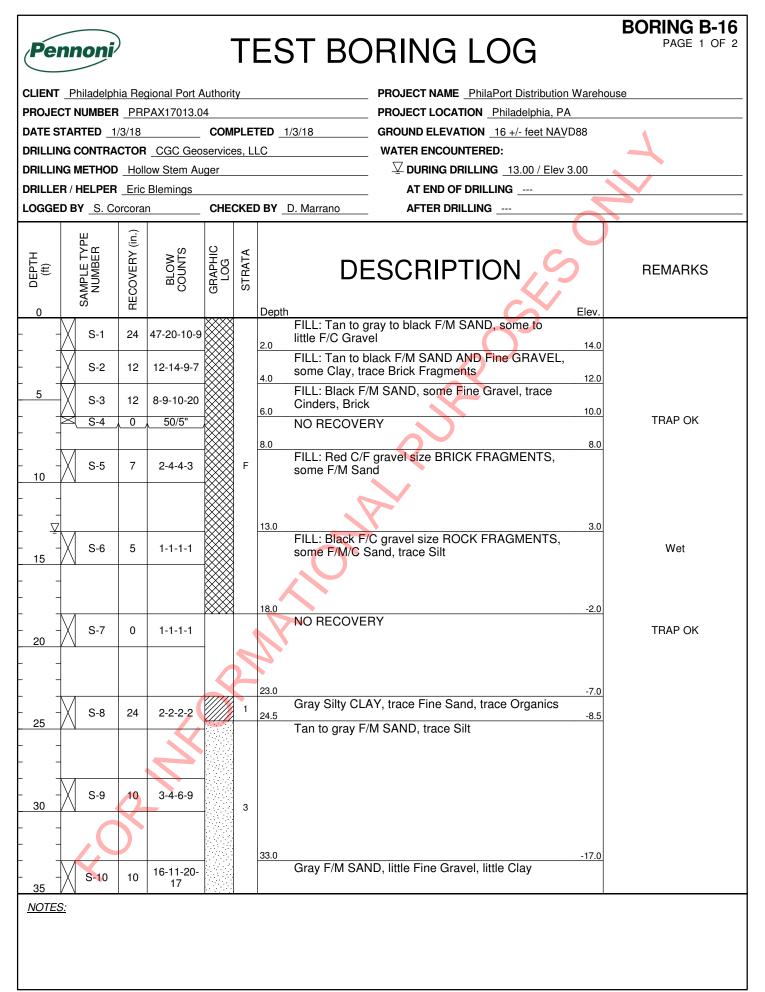


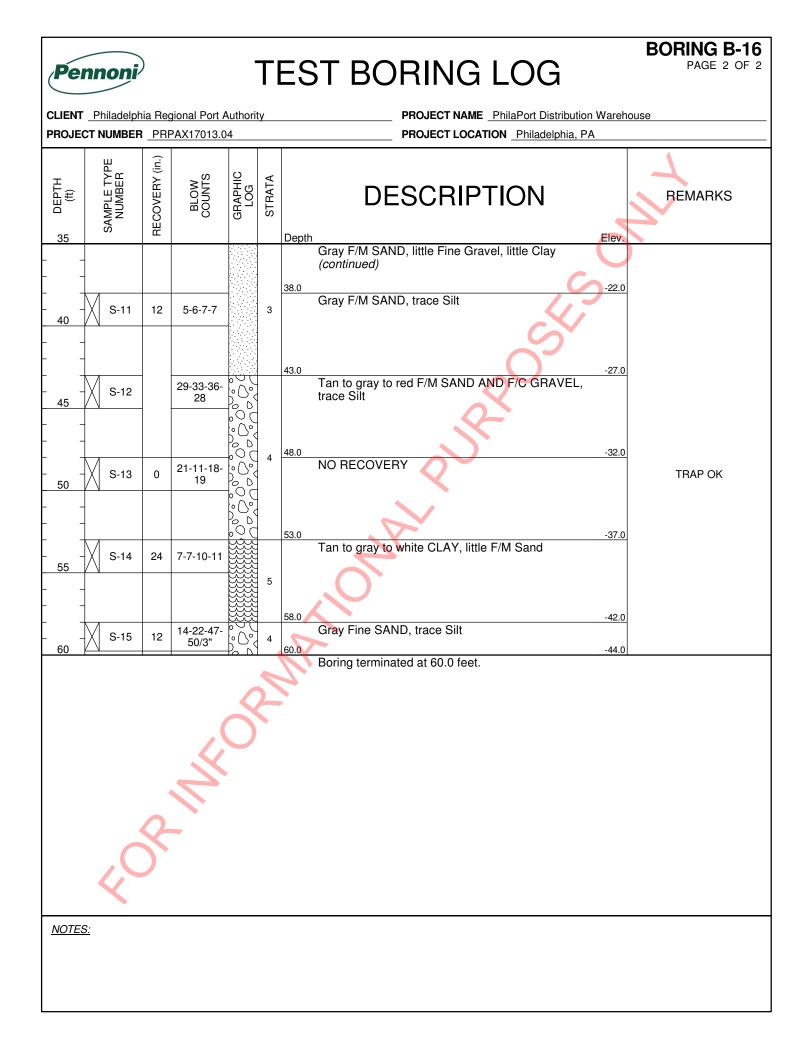


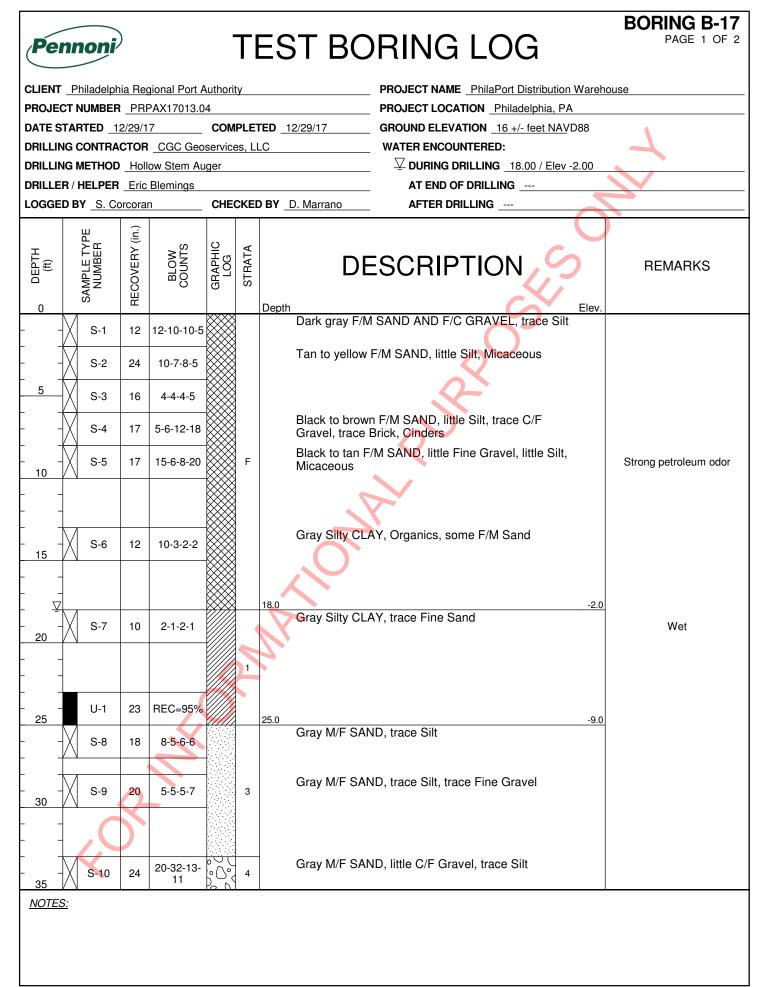




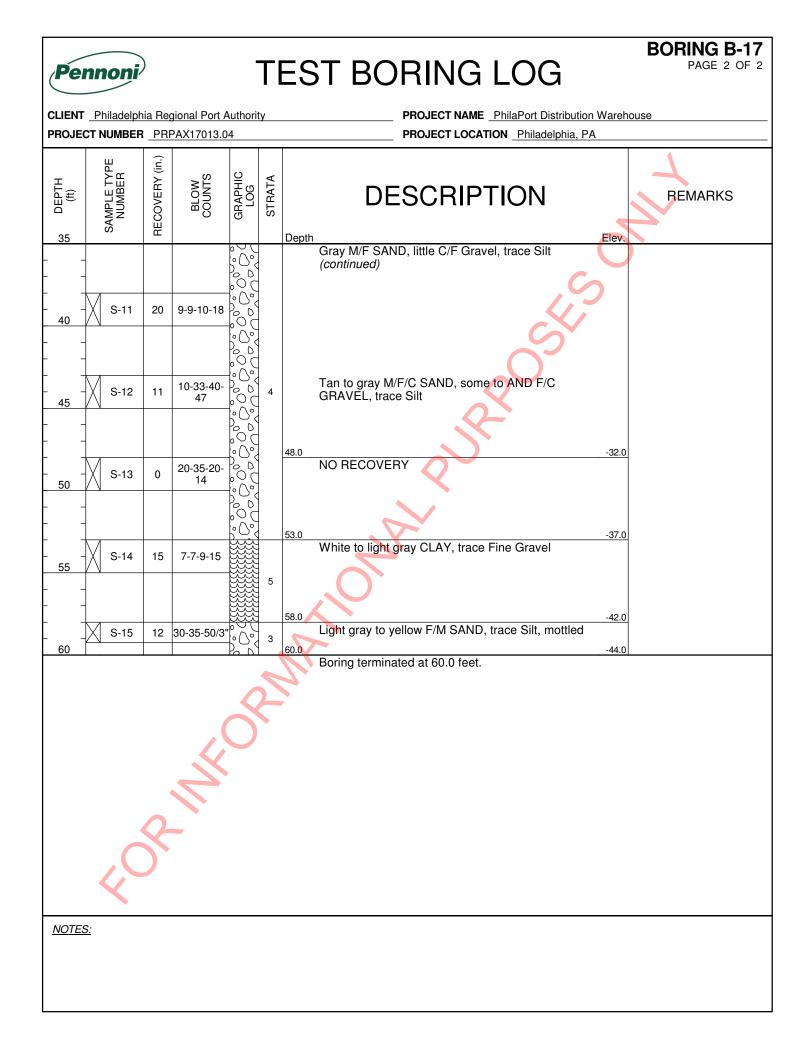
Per	nnoni)		•	T	EST BORING LOG BORING B-15 PAGE 3 OF 3
			gional Port A PAX17013.0		ty	PROJECT NAME _ PhilaPort Distribution Warehouse PROJECT LOCATION _ Philadelphia, PA
DEPTH (ft)	SAMPLE TYPE NUMBER	RECOVERY (in.)	BLOW COUNTS	GRAPHIC LOG		DESCRIPTION BEMARKS
 <u>80</u>	S-19	7	10 40 50/2"		4	Tan to gray M/F/C SAND, some to AND C/F GRAVEL, trace Silt, mottled <i>(continued)</i> Tan to gray to white M/C/F SAND, trace Silt 80.0 Boring terminated at 80.0 feet.
						RURP
						, ONA
					ž	
		8				
NOTES	<u>.</u>					

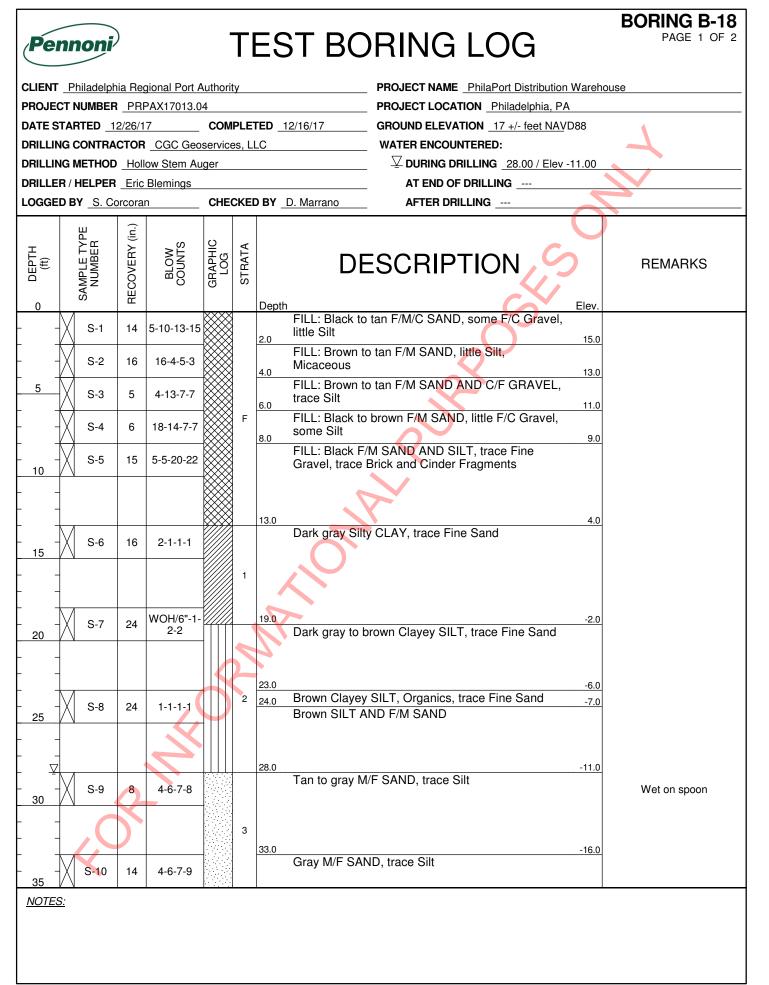


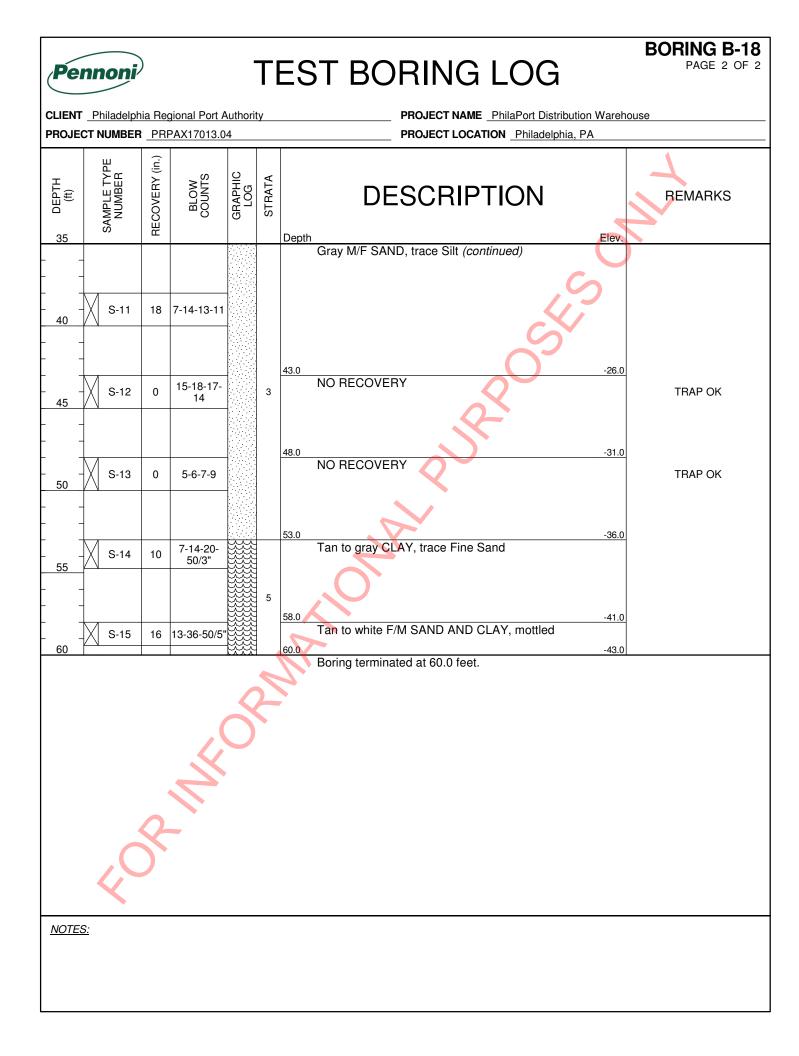


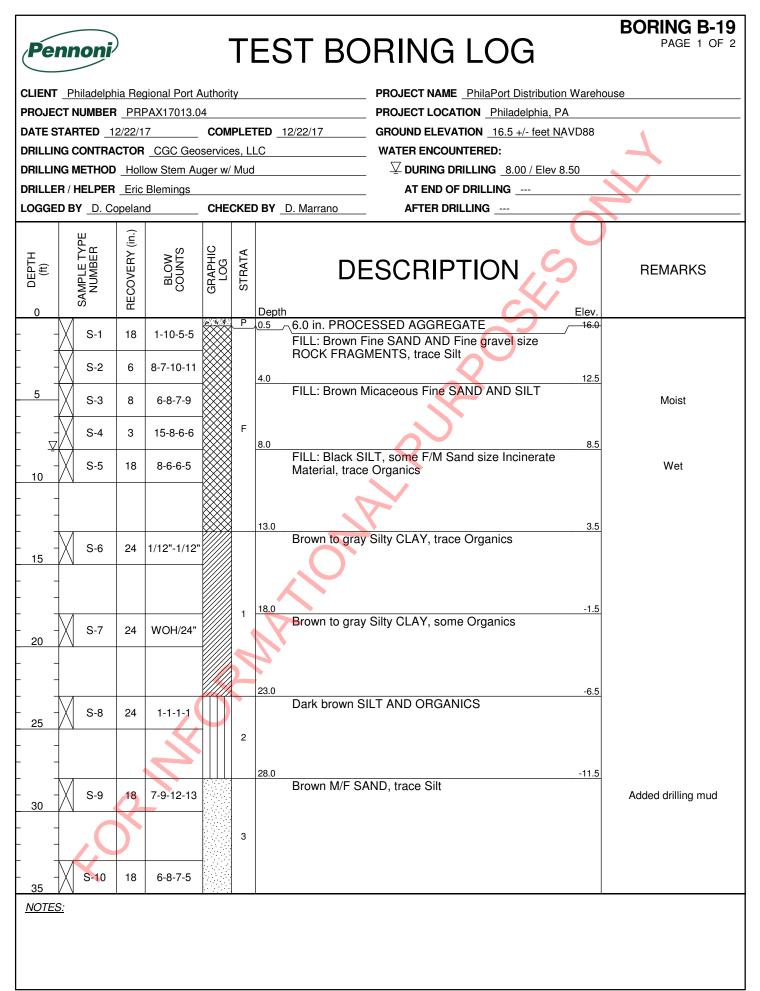


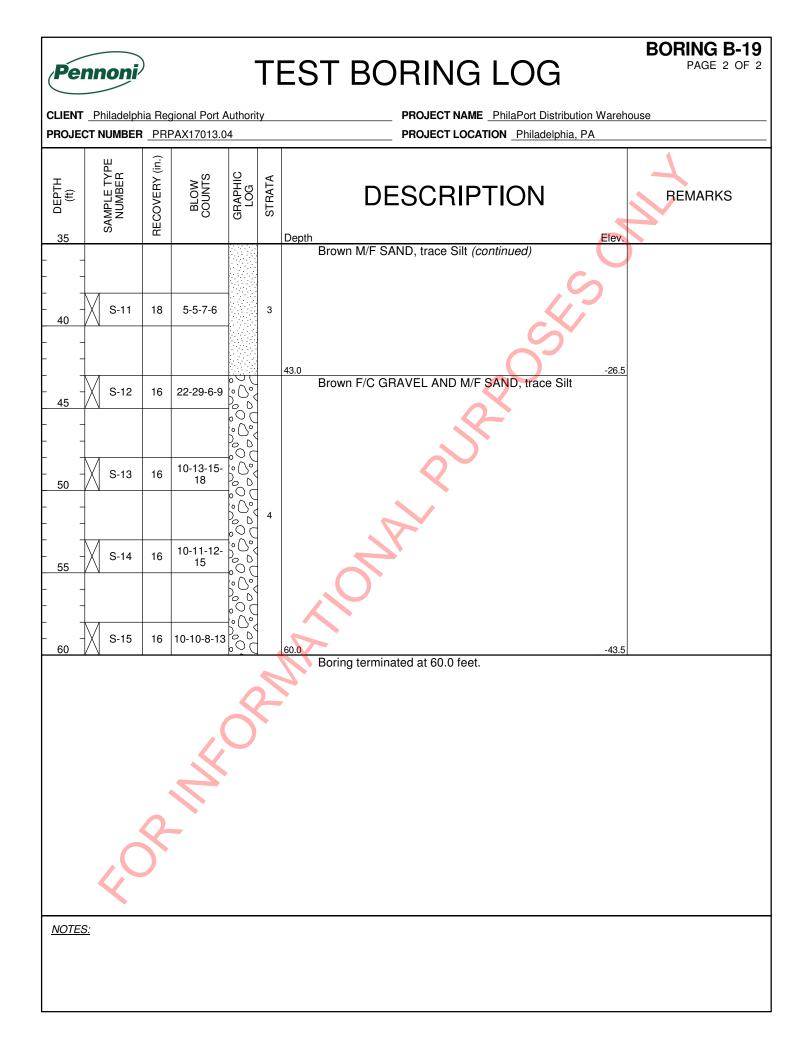
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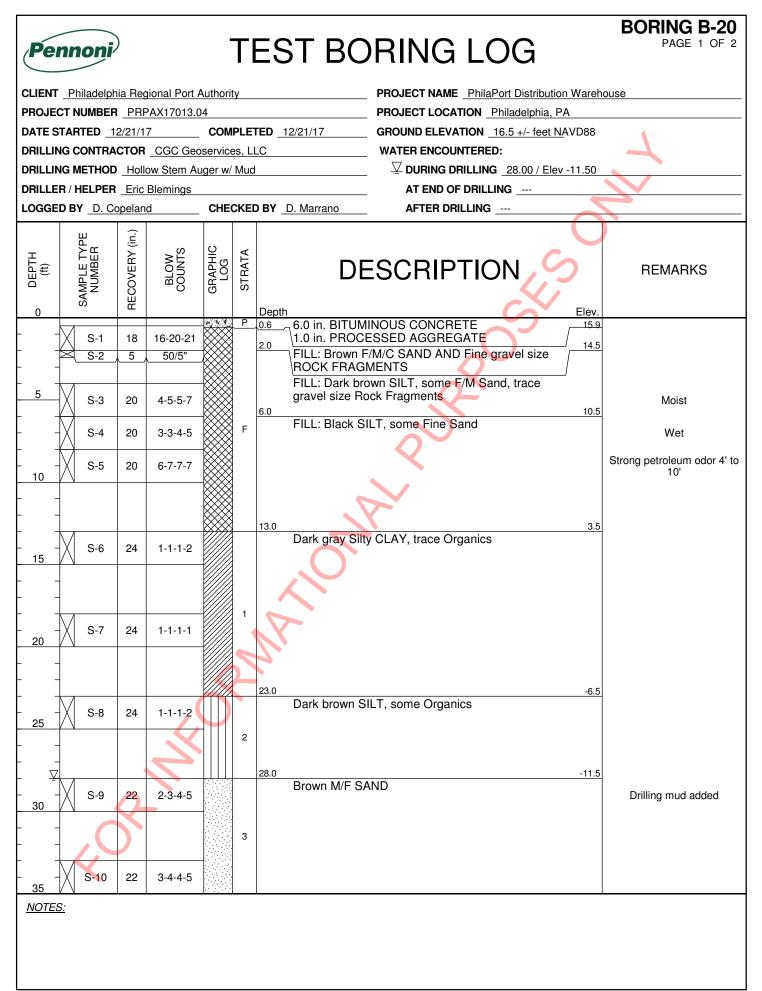


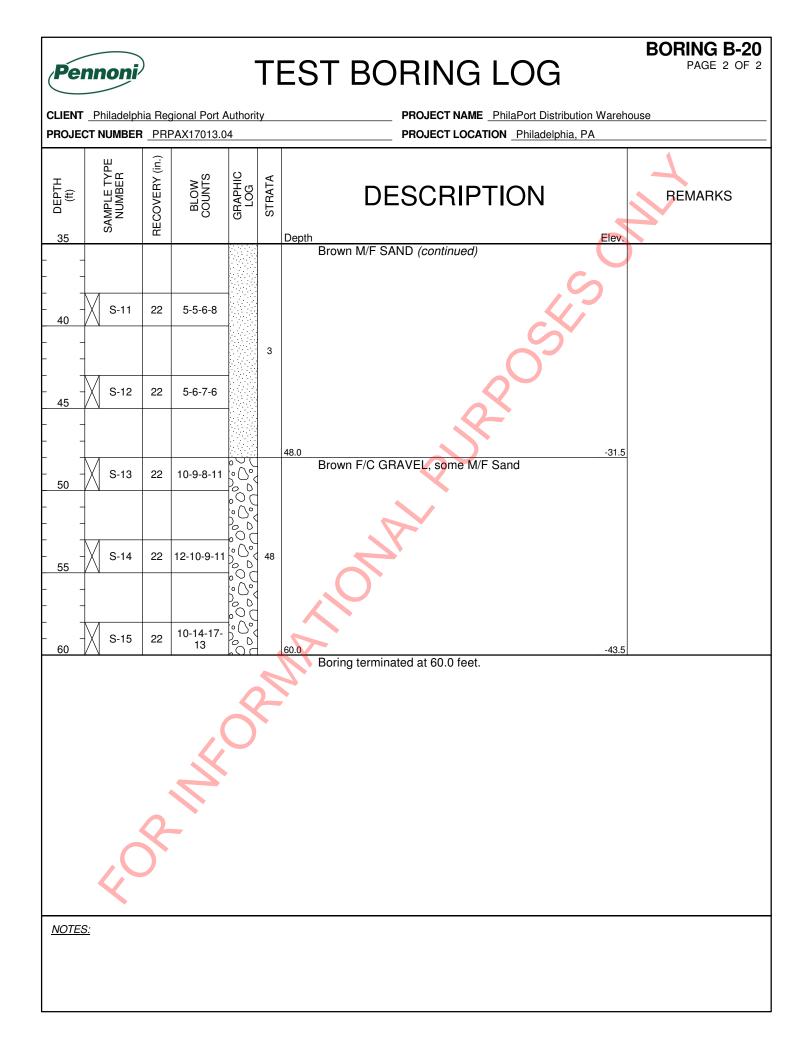












					Test Pit TP-1					
Penno	ni		IESI	PIT LOG	PAGE 1 OF 1					
CLIENT Philad	CLIENT _ Philadelphia Regional Port Authority PROJECT NAME _ PhilaPort Distribution Warehout									
	PROJECT NUMBER PRPAX17013 PROJECT LOCATION Philadelphia, PA DATE STARTED 4/18/19 COMPLETED 4/18/19 GROUND ELEVATION 8.5'									
	EXCAVATION CONTRACTOR Ambient Group, LLC WATER ENCOUNTERED:									
EXCAVATION I OPERATOR / H			er Tire Backhoe	DURING EXCAVATION AT END OF EXCAVATION						
LOGGED BY			CHECKED BY D. Marano	V 0 HRS AFTER EXCAVATION 8.0' / Elev 0.	5'					
O DEPTH (ft) SAMPLE TYPE	NUMBER GRAPHIC LOG	STRATA	DESC		REMARKS					
		P	_0.3ASPHALT Processed Aggregate similar to	8.3						
			1.0	GRAVEL and BRICK FRAGMENTS,						
 		F	4.0 FILL: Black SILT, some F/M Sa	4.5	Trace Timber Asphalt Odor					
NOTES:	S		Test Pit terminated at 9.0 feet.							

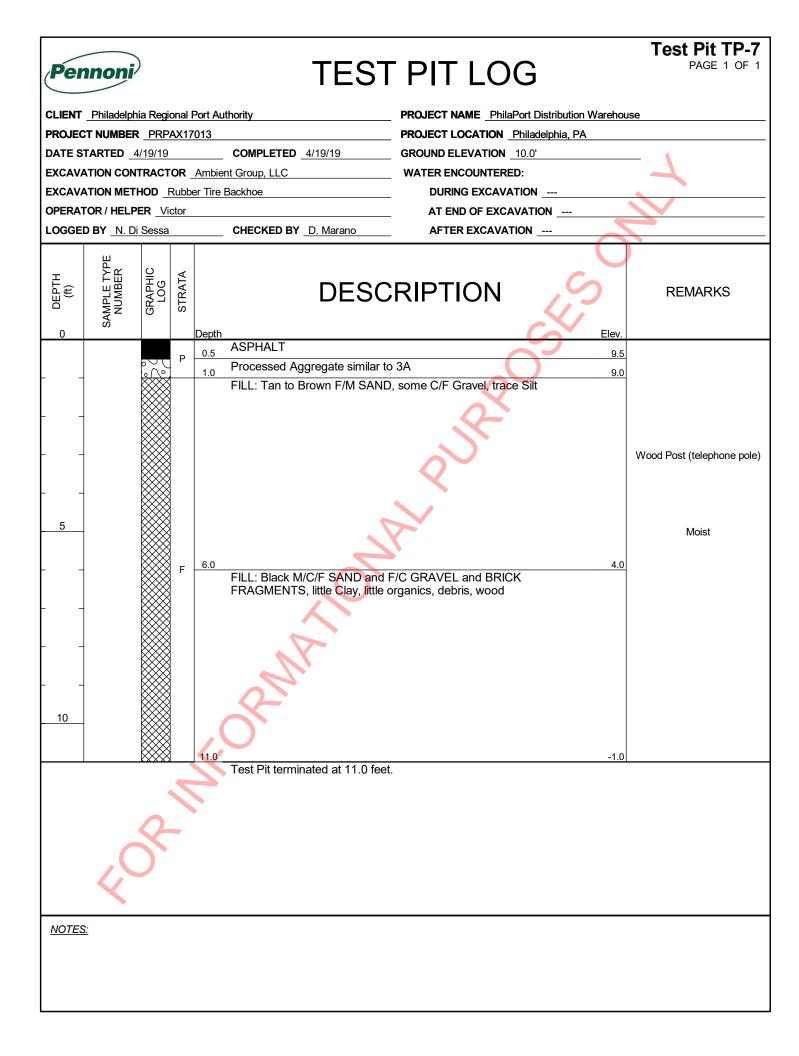
Pennoni		TEST	PIT LOG	Test Pit TP-2 PAGE 1 OF 1
CLIENT _Philadelphia Regi PROJECT NUMBER _PRP			PROJECT NAME _PhilaPort Distribution Warehouse PROJECT LOCATION _Philadelphia, PA	
DATE STARTED <u>4/18/19</u> EXCAVATION CONTRACT EXCAVATION METHOD	OR _A	COMPLETED _4/18/19	GROUND ELEVATION 8.5' WATER ENCOUNTERED: DURING EXCAVATION	4
OPERATOR / HELPER Vi LOGGED BY N. Di Sessa		CHECKED BY _D. Marano	AT END OF EXCAVATION Ψ 0 HRS AFTER EXCAVATION _9.0' / Elev -0.5	
o DEPTH (ft) SAMPLE TYPE NUMBER GRAPHIC LOG		DESC	RIPTION	REMARKS
	P	0.3 ASPHALT Processed Aggregate similar to	3A	
		1.0 FILL: Red-Brown F SAND and 3.0 FILL: Green micaceous F SANI 4.0 FILL: Black F SAND, some SIL	SILT 7.5 SILT 5.5 D and SILT, trace F/C Gravel 4.5	
NOTES:		9.0 Test Pit terminated at 9.0 feet.	-0.5	Oily water surface

						Test Pit TP-3 PAGE 1 OF 1
Per	noni			IESI	PIT LOG	
CLIENT	Philadelphi	a Regi	onall	Port Authority	PROJECT NAME PhilaPort Distribution Warehouse	e
					PROJECT LOCATION Philadelphia, PA	
				COMPLETED 4/18/19 Ambient Group, LLC	GROUND ELEVATION <u>8.0</u> WATER ENCOUNTERED:	-
				er Tire Backhoe	DURING EXCAVATION	
	FOR / HELPE				AT END OF EXCAVATION	
LOGGE	DBY N. Di	Sessa		CHECKED BY D. Marano	AFTER EXCAVATION	
o DEPTH (ft)	SAMPLE TYPE NUMBER	GRAPHIC LOG	STRATA	DESC	RIPTION	REMARKS
		00(Р	0.3 ASPHALT	7.7	
				Processed Aggregate similar to	7.0	
 			F	4.0 FILL: Black F/M SAND, some Cla 6.0 FILL: Black F/M SAND, some to FILL: Black F/M SAND, some to 11.0 Test Pit terminated at 11.0 feet.	4.0 C/F Gravel, trace Silt 2.0 to little Silt, little F Gravel -3.0	
NOTES	<u><u>s</u></u>	\$				

		0				Test Pit TP-4				
Per	noni)		TEST	Γ PIT LOG	PAGE 1 OF 1				
\subseteq										
				Port Authority	PROJECT NAME _ PhilaPort Distribution Warehouse					
					PROJECT LOCATION Philadelphia, PA					
				COMPLETED _4/18/19						
				Ambient Group, LLC er Tire Backhoe	_ WATER ENCOUNTERED: DURING EXCAVATION					
	TOR / HELP				AT END OF EXCAVATION					
	D BY <u>N. D</u>			CHECKED BY D. Marano						
	ш				\bigcirc					
DEPTH (ft)	SAMPLE TYP NUMBER	GRAPHIC LOG	STRATA		RIPTION	REMARKS				
0				Depth 0.3 ASPHALT	Elev. 7.7					
		$\frac{1}{2}$	Р	Processed Aggregate similar t	o 3A					
				1.0 FILL: Gray F/M SAND and F (Gravel, some Clay, trace Brick					
				Fragments						
L _										
					$\mathbf{Q}^{\mathbf{U}}$					
				4.0 FILL: Black E/M SAND, some	4.0 F Gravel, trace Brick Fragments and					
				Silt	Politici, lidee blick i ruginente una					
5			F							
L _			>							
			>							
<u> </u>			>							
			×	9.5 Test Pit terminated at 9.5 feet.	-1.5					
NOTES	<u>S:</u>									

Per	nnoni)		TEST	PIT LOG	Test Pit TP-5 PAGE 1 OF 1			
CLIENT	Philadelphi	ia Regi	onall	Port Authority	PROJECT NAME _ PhilaPort Distribution War	rehouse			
PROJEC	PROJECT NUMBER PRPAX17013 PROJECT LOCATION Philadelphia, PA								
DATE S	TARTED 4	/18/19		COMPLETED _4/18/19	GROUND ELEVATION 10.0'				
				Ambient Group, LLC	WATER ENCOUNTERED:				
				er Tire Backhoe	DURING EXCAVATION				
	OR / HELPI				AT END OF EXCAVATION				
LOGGEI	D BY <u>N. Di</u>	Sessa	1	CHECKED BY D. Marano	✓ 0 HRS AFTER EXCAVATION 9.0' / E	lev 1.0'			
o DEPTH (ft)	SAMPLE TYPE NUMBER	GRAPHIC LOG	STRATA	DESC	RIPTION	REMARKS			
			Р	0.3 ASPHALT		9.7			
		000		1.0 Processed Aggregate similar to		9.0			
				FILL: Brown C/F gravel size RC	OCK FRAGMENTS and F/M SAND,	8.5			
					ravel, trace Silt and Brick Fragments	Rebar Encountered			
						7.0			
			2 2	Cinder Fragments, glass	Brick Fragments, little F Gravel, trace				
					\sim				
5			F	5.0 Ell L: Brown Orange Grav E/M	C SAND, some F/C Gravel, some Silt	5.0			
				9.0		1.0			
NOTES	X	\$	5	Test Pit terminated at 9.0 feet.		1.0			
	<u>~</u>								

)			тгот		Test Pit TP-6 PAGE 1 OF 1		
Per	noni				IE91	PIT LOG			
CLIENT	Philadelph	ia Regi	onal	Port Au	ithority	PROJECT NAME PhilaPort Distribution Warehous	se		
PROJEC	T NUMBER	PROJECT LOCATION _ Philadelphia, PA							
DATE S		/18/19			COMPLETED 4/18/19	GROUND ELEVATION 12.0'	_		
			-		nt Group, LLC	WATER ENCOUNTERED:			
EXCAVA	ATION MET	DURING EXCAVATION AT END OF EXCAVATION							
	FOR / HELP								
LOGGE	d BY <u>N. D</u> i	Sessa			CHECKED BY D. Marano	W 0 HRS AFTER EXCAVATION <u>10.5' / Elev 1</u>	.5'		
o DEPTH (ft)	SAMPLE TYPE NUMBER	GRAPHIC LOG	STRATA	Depth			REMARKS		
		000			_\ASPHALT				
		000	Р	1.0	Processed Aggregate similar to	11.0			
[FILL: Brown F/M SAND, some				
				2.0		10.0			
			2		FILL: Brown to Tan F/M SAND	, little F Gravel, trace Silt			
				3.0		9.0			
			*		FILL: Brown to Black F/M SAN	D, little F Gravel, trace Cinder			
					Fragments and Silt				
5			2	5.0	7	7.0			
					FILL: Black F/M SAND, some S Fragments	Silt, some to little F/C Gravel and Brick			
			F		riaginients				
							Telphone poles		
			2						
							Hole collapsed		
					\mathbf{Q}				
10			2						
Ţ			2	10.5		1.5			
				$\boldsymbol{\checkmark}$	Test Pit terminated at 10.5 feet				
			_	$\mathbf{\Sigma}$	•				
		•							
	C)							
	X								
	•								
<u>NOTES</u>	<u>S:</u>								



Per	nnoni)		TEST	PIT LOG	Test Pit TP-8 PAGE 1 OF 1
	CLIENT Philadelphia Regional Port Authority PROJECT NAME PhilaPort Distribution Warehouse					
PROJEC		R PRP	AX17	013	PROJECT LOCATION Philadelphia, PA	
					GROUND ELEVATION 10.0'	1
	EXCAVATION CONTRACTOR Ambient Group, LLC					4
	EXCAVATION METHOD Rubber Tire Backhoe			er Tire Backhoe	DURING EXCAVATION	
	TOR / HELP				AT END OF EXCAVATION	
LOGGE	D BY <u>N. D</u>	i Sessa		CHECKED BY D. Marano	AFTER EXCAVATION	
o DEPTH (ft)	SAMPLE TYPE NUMBER	GRAPHIC LOG	STRATA	DESC	RIPTION	REMARKS
				0.3 ASPHALT	9.7	
		000	Р	Processed Aggregate similar to	9.0	
				FILL: Tan to Brown F/M SAND		
 			F	4.0 FILL: Black M/C/F SAND and F debris	6.0 F/C BRICK FRAGMENTS, little Clay, -1.0	
NOTES	<u>.</u>	<u></u>	-			

Do	moni			тест		Test Pit TP-9 PAGE 1 OF 1
FCI	Pennoni TEST PIT LOG					
	CLIENT Philadelphia Regional Port Authority PROJECT NAME PhilaPort Distribution Warehouse					
	PROJECT NUMBER PROJECT LOCATION Philadelphia, PA DATE STARTED 4/19/19 GROUND ELEVATION 9.0'					
						-
EXCAVATION CONTRACTOR Ambient Group, LLC WATER ENCOUNTERED: EXCAVATION METHOD Rubber Tire Backhoe DURING EXCAVATION						
	FOR / HELPI			AT END OF EXCAVATION		
	DBY <u>N. Di</u>			CHECKED BY _D. Marano	\mathbf{V} 0 HRS AFTER EXCAVATION <u>9.0' / Elev 0.0</u>	
o DEPTH (ft)	SAMPLE TYPE NUMBER	GRAPHIC LOG	STRATA	DESC	RIPTION	REMARKS
		00(0.3 ASPHALT	8.7	
				Processed Aggregate similar to	8.0	
_				FILL: Black F/C GRAVEL and	F/M/C SAND, little Silt	
 _ 5 			F	4.0 FILL: Brown SILT, some F/M S 6.0 FILL: Black Silty Clay, some F/	3.0	
 _ ⊻ 10				11.0 Test Pit terminated at 11.0 feet	-2.0	
<u>NOTES</u>	<u>.</u>					

Pennoni			TESI	F PIT LOG	Test Pit TP-10 PAGE 1 OF 1
CLIENT _Philadelphia Regional Port Authority PROJECT NAME _PhilaPort Distribution Ware PROJECT NUMBER _PRPAX17013 PROJECT LOCATION _Philadelphia, PA					se
DATE STARTED _	4/19/19	OR _	COMPLETED 4/19/19 Ambient Group, LLC	GROUND ELEVATION 9.0'	
OPERATOR / HELF			CHECKED BY D. Marano	AT END OF EXCAVATION Ψ 0 HRS AFTER EXCAVATION _9.0' / Elev 0.	0'
o DEPTH (ft) SAMPLE TYPE NUMBER	GRAPHIC LOG	STRATA		RIPTION	REMARKS
		Р	Depth <u>0.3</u> ASPHALT Processed Aggregate similar t	8.8	
			1.0 FILL: Black F/C GRAVEL and	8.0	
 		F	4.0 FILL: Brown F/M SAND, some Fragments, trace Clay 9.0 Test Pit terminated at 9.0 feet.	e Silt, little F/C Gravel and Brick	
NOTES:	s S				

Pennoni TEST PIT LOG	Test Pit P-1 PAGE 1 OF 1
CLIENT Philadelphia Regional Port Authority PROJECT NAME PhilaPort Distribution War	ehouse
PROJECT NUMBER PROJECT LOCATION Philadelphia, PA DATE STARTED 4/18/19 GROUND ELEVATION 8.0'	
EXCAVATION CONTRACTOR Ambient Group, LLC WATER ENCOUNTERED:	$- \checkmark$
EXCAVATION METHOD _Rubber Tire Backhoe DURING EXCAVATION OPERATOR / HELPER Victor AT END OF EXCAVATION	
LOGGED BY E. lannetti CHECKED BY D. Marano AFTER EXCAVATION	
	REMARKS
0.5 6" ASPHALT 0.6 P 10 6" Processed Aggregate similar to 3A	7.5
	7.0 6.7
Test Pit terminated at 1.3 feet.	

Pennoni	TEST	PIT LOG	Test Pit P-2 PAGE 1 OF 1
CLIENT Philadelphia Regional Port Au	uthority	PROJECT NAME _ PhilaPort Distribution Warehouse	
PROJECT NUMBER PRPAX17013		PROJECT LOCATION Philadelphia, PA	
DATE STARTED <u>4/18/19</u> EXCAVATION CONTRACTOR Ambie	_ COMPLETED _4/18/19 ent Group, LLC	GROUND ELEVATION 12.0' WATER ENCOUNTERED:	
EXCAVATION METHOD Rubber Tire		DURING EXCAVATION	
OPERATOR / HELPER Victor		AT END OF EXCAVATION	
LOGGED BY E. lannetti	CHECKED BY D. Marano	AFTER EXCAVATION	
o DEPTH SAMPLE TYPE (ft) NUMBER NUMBER LOG STRATA STRATA		RIPTION	REMARKS
0.4	5" ASPHALT	11.6	
<u>P</u> <u>1.2</u>	9" Processed Aggregate similar	10.8	
1.5	Tan F/M/C SAND Test Pit terminated at 1.5 feet.		
NOTES:	CRMA ION		

Pennoni	TEST	PIT LOO	3	Test Pit P-3 PAGE 1 OF 1
CLIENT Philadelphia Regional Port Authority		PROJECT NAME PhilaPo	ort Distribution Warehouse	
PROJECT NUMBER PRPAX17013		PROJECT LOCATION P	niladelphia, PA	
	IPLETED <u>4/18/19</u>	GROUND ELEVATION _1		
EXCAVATION CONTRACTOR Ambient Grou		WATER ENCOUNTERED		
OPERATOR / HELPER Victor		AT END OF EXCAV		
	CKED BY D. Marano	AFTER EXCAVATION		
o DEPTH (ff) (ff) sampLE TYPE NUMBER NUMBER LOG LOG LOG STRATA STRATA		RIPTION	Elev.	REMARKS
	SPHALT rocessed Aggregate similar	to 3A	11.6	
	Pit terminated at 1.1 feet.		10.9	
NOTES:				

NAME _PhilaPort Distribution Warehouse LOCATION _Philadelphia, PA ELEVATION _9.0' NCOUNTERED: ING EXCAVATION ER EXCAVATION ER EXCAVATION ER EXCAVATION REMARKS Elev.
ELEVATION 9.0' NCOUNTERED: NING EXCAVATION ER EXCAVATION ER EXCAVATION ER EXCAVATION ER EXCAVATION ER EXCAVATION ELEV. Concrete slab encountered on one side of test pit
NCOUNTERED: ING EXCAVATION ER EXCAVATION EIEV. EIEV. Concrete slab encountered on one side of test pit
ING EXCAVATION END OF EXCAVATION ER EXCAVATION FION
ER EXCAVATION ER EXCAVATION FION
ER EXCAVATION TION REMARKS Elev
Elev. 8.7 Concrete slab encountered on one side of test pit
Elev. 8.7 Concrete slab encountered on one side of test pit
8.7 Concrete slab encountered on one side of test pit
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\mathcal{Q}^{\sim}

Pennoni TEST	PIT LOG	Test Pit P-5 PAGE 1 OF 1
CLIENT Philadelphia Regional Port Authority	PROJECT NAME _ PhilaPort Distribution Warehouse	
PROJECT NUMBER PRPAX17013	PROJECT LOCATION Philadelphia, PA	
DATE STARTED 4/18/19 COMPLETED 4/18/19		
EXCAVATION CONTRACTOR Ambient Group, LLC EXCAVATION METHOD Rubber Tire Backhoe	WATER ENCOUNTERED:	
OPERATOR / HELPER Victor	AT END OF EXCAVATION	
LOGGED BY _E. lannetti CHECKED BY _D. Marano	AFTER EXCAVATION	
O DEPTH (ft) (ft) (ft) (ft) NUMBER NUMBER NUMBER DEPth DEBC	RIPTION	REMARKS
0.3 4" ASPHALT	8.7	
8" Processed Aggregate simila 1.0 Test Pit terminated at 1.0 feet.	8.0	
NOTES:		

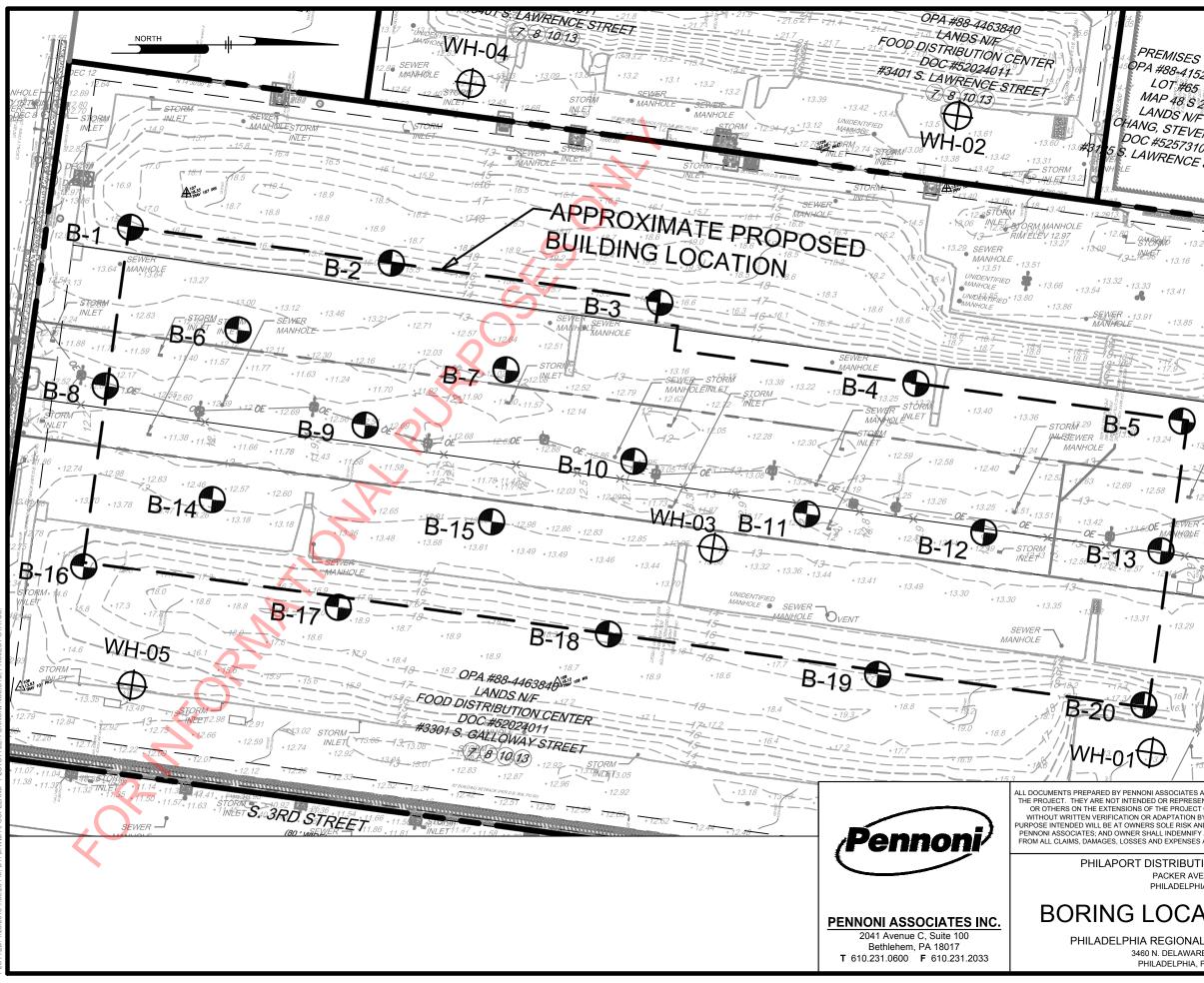
Pennoni TEST	PIT LOG	Test Pit P-6 PAGE 1 OF 1				
CLIENT Philadelphia Regional Port Authority	PROJECT NAME PhilaPort Distribution Warehouse					
PROJECT NUMBER PRPAX17013	PROJECT LOCATION Philadelphia, PA					
DATE STARTED _4/18/19 COMPLETED _4/18/19 EXCAVATION CONTRACTOR _Ambient Group, LLC	GROUND ELEVATION 11.0' WATER ENCOUNTERED:					
EXCAVATION METHOD _ Rubber Tire Backhoe	DURING EXCAVATION					
OPERATOR / HELPER Victor	_ AT END OF EXCAVATION					
LOGGED BY E. lannetti CHECKED BY D. Marano	_ AFTER EXCAVATION					
	RIPTION	REMARKS				
P 9" Processed Aggregate simila	10.7					
<u>1.1</u> <u>1.2</u> /\Tan F/M/C SAND	9.9 7_9.8					
Test Pit terminated at 1.2 feet.						
	×					
	\sim					
	\sim					
Q^{-1}						
\diamond						
\mathbf{O}						
NOTES:						

Pennoni	IESI	PIT LOG	Test Pit P-7 PAGE 1 OF 1
CLIENT _ Philadelphia Regional Port Au	uthority	PROJECT NAME PhilaPort Distribution Warehouse	
PROJECT NUMBER PRPAX17013		PROJECT LOCATION Philadelphia, PA	
DATE STARTED _4/18/19 EXCAVATION CONTRACTOR _Ambie	completed <u>4/18/19</u> ent Group, LLC	GROUND ELEVATION 12.5' WATER ENCOUNTERED:	
EXCAVATION CONTRACTOR Ambie		DURING EXCAVATION	
OPERATOR / HELPER Victor		AT END OF EXCAVATION	
LOGGED BY <u>E. lannetti</u>	CHECKED BY D. Marano	AFTER EXCAVATION	
o DEPTH (ft) SAMPLE TYPE NUMBER NUMBER CRAPHIC LOG STRATA STRATA		RIPTION	REMARKS
0.3 0 0 P	_4" ASPHALT 10" Processed Aggregate simila	12.2	
	Test Pit terminated at 1.2 feet.	11.3	
NOTES:			

Pennoni TEST	PIT LOG	Test Pit P-8 PAGE 1 OF 1
CLIENT Philadelphia Regional Port Authority	PROJECT NAME PhilaPort Distribution Warehouse	
PROJECT NUMBER PRPAX17013	PROJECT LOCATION Philadelphia, PA	
DATE STARTED _4/18/19 COMPLETED _4/18/19 EXCAVATION CONTRACTOR _Ambient Group, LLC	GROUND ELEVATION 9.0' WATER ENCOUNTERED:	1
EXCAVATION METHOD Rubber Tire Backhoe	DURING EXCAVATION	
	_ AT END OF EXCAVATION	
LOGGED BY E. lannetti CHECKED BY D. Marano	AFTER EXCAVATION	
O DESC	RIPTION	REMARKS
	8.7	
	7.8	
Test Pit terminated at 1.2 feet.		
	~~~	
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	$\sim$	
5	$\sim$	
	X .	
	_	
$Q^{-}$		
<u>-</u>		
<u>NOTES:</u>		

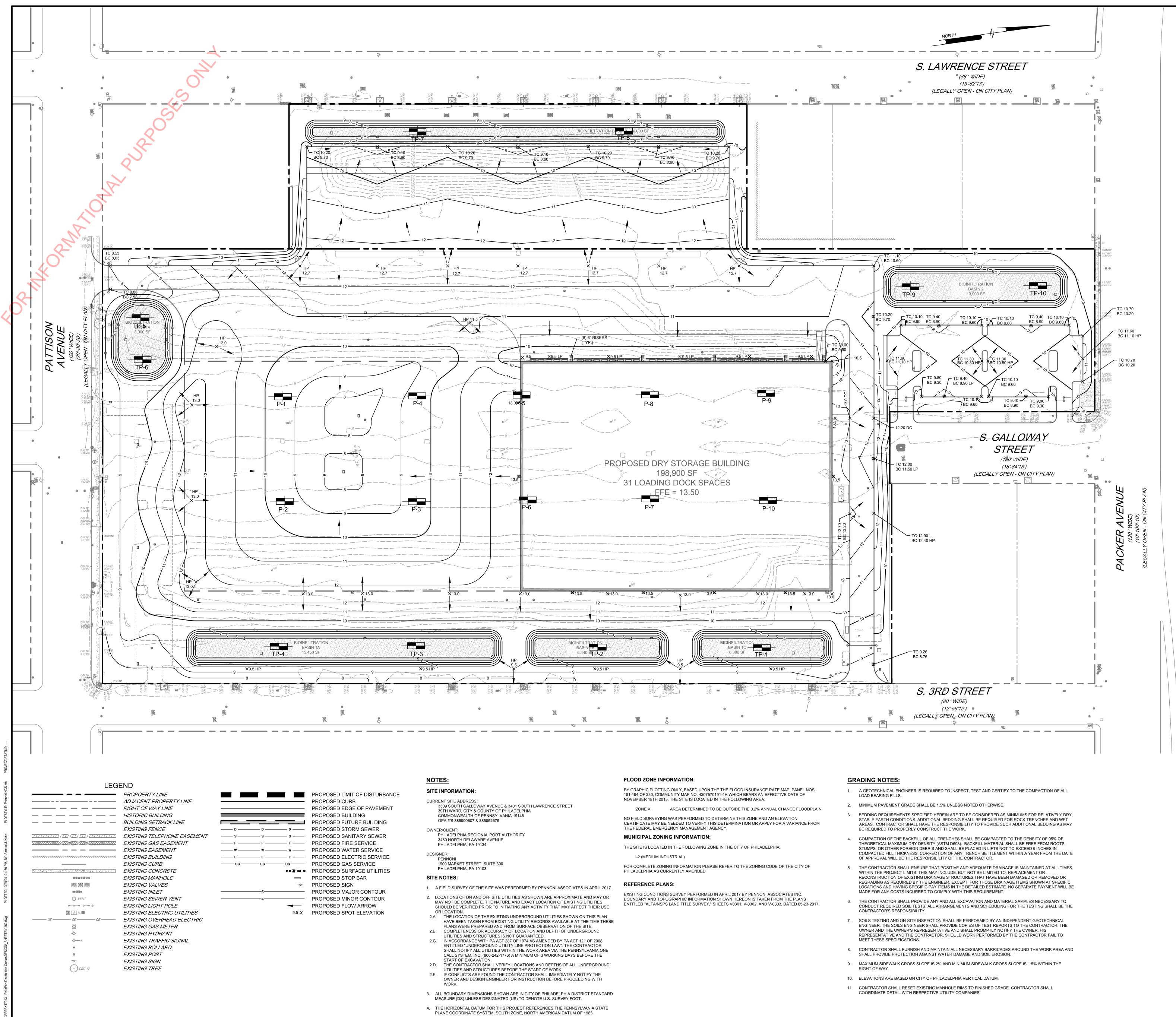
Pennoni TEST PIT LOG	Test Pit P-9 PAGE 1 OF 1
CLIENT Philadelphia Regional Port Authority PROJECT NAME PhilaPort Distribution Warehous	e
PROJECT NUMBER       PRPAX17013       PROJECT LOCATION       Philadelphia, PA         DATE STARTED       4/18/19       GROUND ELEVATION       9.0'	
EXCAVATION CONTRACTOR Ambient Group, LLC       WATER ENCOUNTERED:	
EXCAVATION METHOD Rubber Tire Backhoe DURING EXCAVATION	
OPERATOR / HELPER Victor       AT END OF EXCAVATION         LOGGED BY _E. lannetti       CHECKED BY _D. Marano       AFTER EXCAVATION	
HLGG CLARETYPE DEPTH DESCRIPTION	REMARKS
P 0.6 7" ASPHALT 8.4	
6" Processed Aggregate similar to 3A	
KORMANE KORMANE	
<u>NOTES:</u>	

Pennoni TEST	PIT LOG	Test Pit P-10 PAGE 1 OF 1
CLIENT _ Philadelphia Regional Port Authority	PROJECT NAME _ PhilaPort Distribution Warehouse	
PROJECT NUMBER PRPAX17013	PROJECT LOCATION _Philadelphia, PA	
DATE STARTED _4/18/19       COMPLETED _4/18/19         EXCAVATION CONTRACTOR _Ambient Group, LLC	GROUND ELEVATION 13.0' WATER ENCOUNTERED:	1
EXCAVATION METHOD _ Rubber Tire Backhoe	DURING EXCAVATION	
OPERATOR / HELPER         Victor           LOGGED BY         E. lannetti         CHECKED BY         D. Marano	AT END OF EXCAVATION AFTER EXCAVATION	
HETYPE AMPLETYPE CGRAPHIC CLOG CLOG CLOG CLOG CRAPHIC CLOG CRAPHIC CLOG CRAPHIC CLOG CRAPHIC CLOG CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAPHIC CRAP	RIPTION	REMARKS
8.5" Processed Aggregate sim	11.8	
Tan F/M/C SAND Test Pit terminated at 1.5 feet.		
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	$\sim$	
	$\boldsymbol{\zeta}$	
RMA		
$\mathbf{O}$		
8		
<u>NOTES:</u>		



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NC	).	DESCRIPTION	DATE	BY
#	#		#	#
		LEGEND		
	B-1	INDICATES APPROXIMATE	· ·	
	$\bullet$	BORING LOCATION AND ID		
	•	NUMBER FOR THE CURREI	NISIUL	JY.
		INDICATES APPROXIMATE	TEST	
	WH-01	BORING LOCATION AND		
	$\oplus$	IDENTIFYING NUMBER		
	$\Psi$	CONDUCTED BY OTHERS F	FOR THE	Ξ
		PRELIMINARY STUDY.		
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	NOTE	<u>=5</u>		
	WAT	ER LEVELS, WHERE SHOWN,	ARE	
		SE OBSERVED AT THE TIME N		
		MAY NOT REFLECT DAILY OF		
		SONAL VARIATIONS IN THE GI	ROUND	
	WAI	ER LEVEL.		
	THE	SUBSURFACE CONDITIONS		
		EALED BY THIS STUDY REPRE	ESENT	
		RENT CONDITIONS AT THE		
		CIFIED TEST LOCATIONS ONL		
		NOT BE INDICATIVE OF CONE	DITIONS	
	ALO	THER LOCATIONS.		
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	100' 200'
ARE INSTRUMENTS OF SERVICE IN RESPECT OF NTED TO BE SUITABLE FOR REUSE BY OWNER	PROJECT PRPAX 17013
OR ON ANY OTHER PROJECT. ANY REUSE Y PENNONI ASSOCIATES FOR THE SPECIFIC ID WITHOUT LIABILITY OR LEGAL EXPOSURE TO	DATE 2018-01-23
AND HOLD HARMLESS PENNONI ASSOCIATES ARISING OUT OF OR RESULTING THEREFROM.	DRAWING SCALE 1"=100'
ION WAREHOUSE	DRAWN BY DAC
IA, PA	APPROVED BY DPM
TION PLAN	DRAWING NO.
L PORT AUTHORITY E AVENUE PA 19134	SHEET 1 OF 1



- 5. THE VERTICAL DATUM FOR THIS PROJECT REFERENCES THE VERTICAL DATUM OF THE CITY OF PHILADELPHIA (CITY).





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## TEST BORING/TEST PIT/AUGER PROBE LOG KEY SHEET

COLUMN	DESCRIPTION
<u>Depth</u>	Depth in feet below ground surface
<u>Description</u>	Description of sample including color, texture, and classification of subsurface material as applicable. Estimated depths to bottom of strata as interpolated from the boring are also shown.
Stratum	Strata numbers as assigned by the geotechnical engineer
Sample No.	Split barrel sample and sample number (S-x) Undisturbed Tube sample and sample number (U-x) Rock core run and core number (R-x) NR indicates no recovery
Blow Counts	<ul> <li>For soils sample (ASTM D 1586): indicates number of blows obtained for each 6 inches penetration of the standard split-barrel sampler.</li> <li>For rock coring (ASTM D 2113): indicates percent recovery (REC) per run and rock quality designation (RQD). RQD is the sum of rock pieces that are 4 inches or longer in length in one core run divided by the total core run.</li> </ul>
Recovery	For soil samples indicates the length of recovery in the sample spoon
Remarks	Special conditions or test data as noted during drilling

Ground Water: Free water level as shown ()*; * Free water level as noted may not be indicative of daily, seasonal, or long term fluctuations.

## **DESCRIPTIVE TERMS**

	RELATIV	E PROPORTIONS	
Descriptive Terr	m	Symbol	Estimated Percentages
Trace		tr	1 to 10
Little		1	10 to 20
Some		sm	20 to 35
And		and	35 to 50
	GRADATION OF COA	RSE GRAINED COMPO	DNENTS
Soil Component	Size Range	Particle Size	
		Maximum	Minimum
Boulders	()		12"
Cobbles		12"	3"
Gravel	Coarse	3"	3/4"
	Fine	3/4"	#4 Sieve
Sand	Coarse	#4 Sieve	#10 Sieve
	Medium	#10 Sieve	#40 Sieve
	Fine	#40 Sieve	#200 Sieve
Silt		#200 Sieve	.005 mm
Clay		.005 mm	-
	<b>COMPOSITION OF COA</b>		
Gradation Designation	<u>Symbol</u>		Proportions
Coarse to Fine	CF	Ũ	an 10% of the component
Coarse to Medium	CM		n 10% Fine
Medium to Fine	MF	2000 41411	10% Coarse
Coarse	С	2000 11011 1070	Fine and Medium
Medium	Μ	10000 111111 - 0 / 1	Coarse and Fine
Fine	F	Less than 10% C	Coarse and Medium

16	DEPARTI	nsylvania MENT OF TRANSPORTATION	ENGINEE	R'S LO	G					Shee	et <u>1</u> of <u>5</u>
Rorin	_	01 ECMS					]		T		
		County: Philadelphia	- Drilling Start: 07	7/27/201	7 5:30	pm		A		NWE	
		Section	-				om	HS		EGISTERI	
		C Site - Port Authority								The	Littete
		Offset						Mar	ng		9/21/17
		Offset	0		-			<u>A</u>	K/1	NGINEE	$\sim$ $/// \sqrt{k}$
	dinates:		CDT 11 5(()					Ĥ	A A	E-053530	
Lat.		Long	Assumed 0.8	Me				20/25		S Y L	TIT
		0 E 2696490.0640 N 14.0 ft						PG/PE	Seal, S	Ignature	e and Date
		Elev./Elapsed Time:	<i>,</i> ,				F	inal Lo	og Ch	ecked	d and Approved
		ft. Elapsed <u>0.0 hr.</u>									lson
		<u>t.</u> Elapsed <u>96.0 hr.</u>						ate: _	9/21/2	2017	
		<u>r B.</u>							Lab T on Sa	esting	Performed
		ied Well Drilling					5	NOT	<u>E:</u> N va	lues ar	nd all graphical mation only.
.om	Puriy.	J					~~	piots	are to	rintor	
	HIC	MATERIAL DESCR	RIPTION	AASHTO	ΤĽ	비민	BLOW COUNTS	N ₆₀	REC	REC	◇ RQD % ◇ ● Soil/Rock Rec. %
ELEV.	GRAPHIC	COMMENTS - OBSEF		/ USCS	SAMPLE	SAMPLE No.	(Blows/	RQD	(ft.)	(%)	<ul> <li>Soil/Rock Rec.% ²⁰ 40 60 80     </li> <li>▲ SPT (N) ▲</li> </ul>
	U P b 4 - r				0 J	S	0.5ft)	%		$\parallel$	▲ SPT (N ₆₀ ) ▲ 10 20 30 40
		BITUMINOUS CONCRETE,									
-		- 5" White crushed gravel be √ layers of pavement.	elween lwo		- 1.0 -						
			0.8'/El. 13.2/			S-1	20-14	19	1.0	100	
-		Subbase.			- 2.0 -						
	0 0 0		1.0'/El. 13.0								
-	0 0 0	SAND and GRAVEL, little S				S-2	15-13-19-22	43	1.6	80	
		dense, moist, heterogeneou sub-angular to angular, non	is, well graded,								
10 -		dark gray, fill.	-plastic, gray to		- 4.0 -						
	0 0 0	- organics, brick, and mica i	in S-3.	a-2-4 / sm							
-				7 311		S-3	15-4-4-11	11	2.0	100	
-	000	•			- 6.0 -						
		- quartz piece stuck in S-4 s - mica in S-4.	shoe.								
	0_0_0]					S-4	37-15-10-12	33	0.5	25	
-	0 ⁻ 0 ⁻ 0 0 ⁻ 0 ⁻ 0					S-4	37-15-10-12	33	0.5	25	
_			8.0'/El. 6.0			S-4	37-15-10-12	33	0.5	25	
-		SILT and CLAY, some Sand	d, soft to very		- 8.0 -	S-4		33	0.5	25	
- - 5 -		soft, wet, heterogeneous, po rounded to sub-angular, low	d, soft to very porly graded,	a-2-4	- 8.0 -	S-4	37-15-10-12 2-2-1-4 <b>Pen=0.50 ts</b>		0.5	25	
- 5 —		soft, wet, heterogeneous, po	d, soft to very porly graded,	a-2-4 / ml	- 8.0 -		2-2-1-4				
- 5 —		soft, wet, heterogeneous, po rounded to sub-angular, low	d, soft to very porly graded, / plastic fines,		 - 8.0 - 		2-2-1-4				
- 5 —		soft, wet, heterogeneous, po rounded to sub-angular, low black, fill,	d, soft to very porly graded,				2-2-1-4 Pen=0.50 ts				
5 -		soft, wet, heterogeneous, por rounded to sub-angular, low black, fill, - tar odor. CLAY and SILT, little Sand,	d, soft to very borly graded, v plastic fines, 10.5'/El. 3.5 very soft, wet,				2-2-1-4	F 4			
5 -		soft, wet, heterogeneous, por rounded to sub-angular, low black, fill, - tar odor. CLAY and SILT, little Sand, heterogeneous, poorly grad	d, soft to very borly graded, v plastic fines, <u>10.5'/El. 3.5</u> very soft, wet, ed, rounded,	/ ml		S-5	2-2-1-4 Pen=0.50 ts 2-1-1-2	F 4	2.0	100	
- 5		soft, wet, heterogeneous, por rounded to sub-angular, low black, fill, - tar odor. CLAY and SILT, little Sand,	d, soft to very borly graded, v plastic fines, <u>10.5'/El. 3.5</u> very soft, wet, ed, rounded,			S-5	2-2-1-4 Pen=0.50 ts 2-1-1-2	F 4	2.0	100	
5 -		soft, wet, heterogeneous, por rounded to sub-angular, low black, fill, - <i>tar odor.</i> CLAY and SILT, little Sand, heterogeneous, poorly grad medium plastic fines, black alluvium,	d, soft to very borly graded, v plastic fines, 10.5'/El. 3.5 very soft, wet, ed, rounded, to dark gray,	/ ml		S-5	2-2-1-4 Pen=0.50 ts 2-1-1-2	F 4	2.0	100	
5		soft, wet, heterogeneous, por rounded to sub-angular, low black, fill, - tar odor. CLAY and SILT, little Sand, heterogeneous, poorly grad medium plastic fines, black	d, soft to very borly graded, v plastic fines, 10.5'/El. 3.5 very soft, wet, ed, rounded, to dark gray,	/ ml		S-5	2-2-1-4 Pen=0.50 ts 2-1-1-2 Pen=0.25 ts WOH-WOH WOH-4	F 4	2.0	100	
5 - -		soft, wet, heterogeneous, por rounded to sub-angular, low black, fill, - tar odor. CLAY and SILT, little Sand, heterogeneous, poorly grad medium plastic fines, black alluvium, Class. on jar samples colled & SB-7T A-7-5(16)/ML	d, soft to very borly graded, v plastic fines, 10.5'/El. 3.5 very soft, wet, ed, rounded, to dark gray,	/ ml		S-5 S-6	2-2-1-4 Pen=0.50 ts 2-1-1-2 Pen=0.25 ts WOH-WOH	F 4	2.0	100	
5		soft, wet, heterogeneous, por rounded to sub-angular, low black, fill, - tar odor. CLAY and SILT, little Sand, heterogeneous, poorly grad medium plastic fines, black alluvium, Class. on jar samples colled & SB-7T	d, soft to very borly graded, v plastic fines, 10.5'/El. 3.5 very soft, wet, ed, rounded, to dark gray,	/ ml		S-5 S-6	2-2-1-4 Pen=0.50 ts 2-1-1-2 Pen=0.25 ts WOH-WOH WOH-4	F 4	2.0	100	



Boring WH-01

ECMS

## **ENGINEER'S LOG**

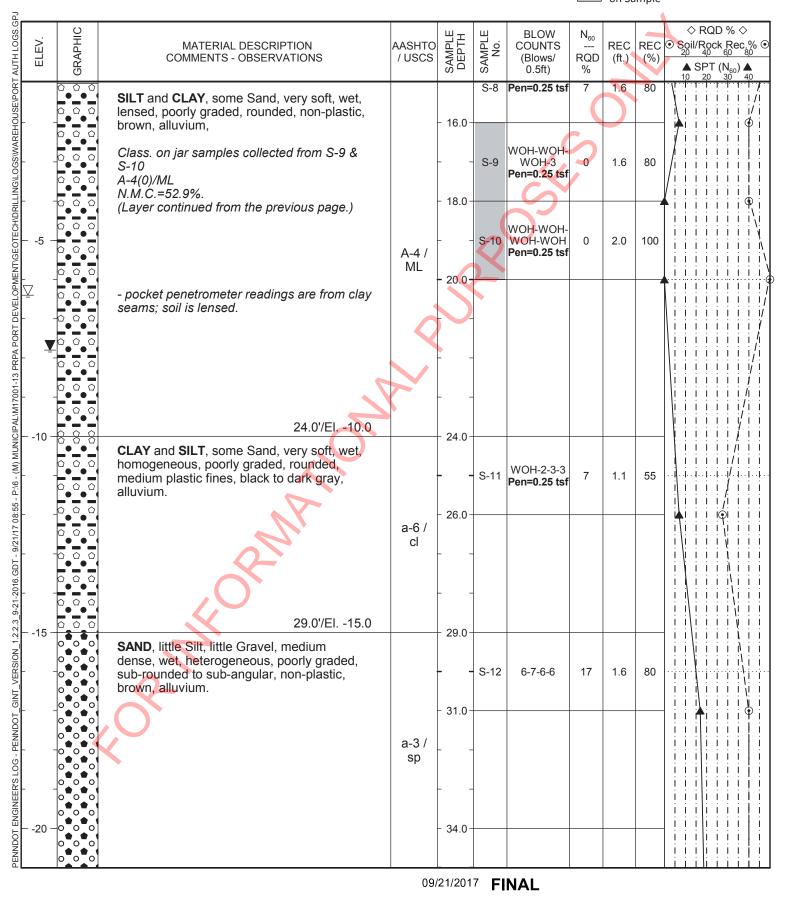
SR _____ Section _____

Sta. _____ Offset _____

District: _____ County: Philadelphia

## Sheet 2 of 5

<u>NOTE:</u> N values and all graphical plots are for information only.





Boring WH-01

# ENGINEER'S LOG

District: _____ County: <u>Philadelphia</u> SR ______ Section _____

Sta. _____ Offset _____

Sheet <u>3</u> of <u>5</u>

**<u>NOTE</u>**: N values and all graphical plots are for information only.

ELEV.	GRAPHIC	MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS	AASHTO / USCS	SAMPLE DEPTH	SAMPLE No.	BLOW COUNTS (Blows/ 0.5ft)	N ₆₀  RQD %	REC (ft.)	REC (%)	⊙ Soil	RQD % √ RQD % //Rock Rec.% 40 60 80 SPT (N ₆₀ ) ▲ 20 30 40
-		<b>SAND</b> , little Silt, little Gravel, medium dense, wet, heterogeneous, poorly graded, sub-rounded to sub-angular, non-plastic, brown, alluvium. ( <i>Layer continued from the previous page.</i> )		- 36.0-	S-13	6-7-7-8	19	1.6	80		
-25 -		- hard to very hard, coarse gravel caused	V	- 39.0 - 	S-14	5-5-8-6	17	1.4	70		
-30 -		drill rig to abnormally vibrate when boring was advanced with tri-cone roller bit while applying downward pressure between 41.0' and 44.0'.	a-3 / sp		S-15	17-7-8-6	20	1.0	50		
-35 -		49.0'/El35.0		- 46.0 -  							
-	0     0     0       0     0     0       0     0     0       0     0     0       0     0     0       0     0     0       0     0     0       0     0     0       0     0     0       0     0     0       0     0     0	SAND and GRAVEL, trace Silt, medium dense, wet, heterogeneous, well graded, sub-angular to angular, non-plastic, brown, alluvium, Class. on jar samples collected from S-16 to S-19 A-1-b/SP-SM N.M.C.=10.5%.	A-1-b / SP-SM	- 51.0-	S-16	20-19-16-16	47	0.8	40		
-40 -											



Boring WH-01

# **ENGINEER'S LOG**

SR _____ Section _____

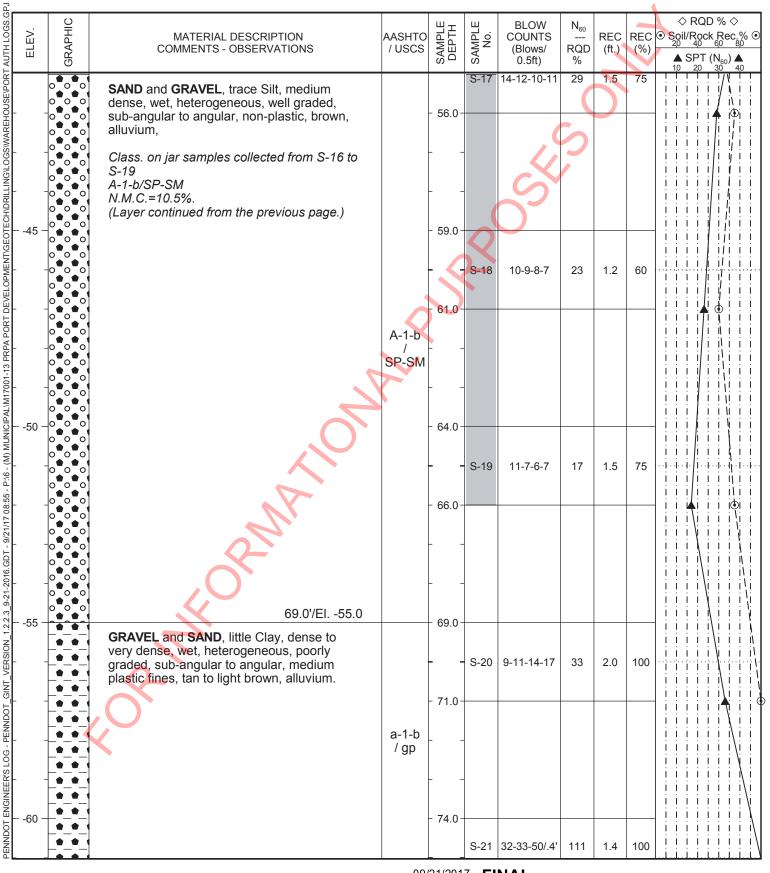
Sta. _____ Offset _____

District: _____ County: Philadelphia

## Sheet <u>4</u> of <u>5</u>

**<u>NOTE</u>**: N values and all graphical plots are for information only.

Lab Testing Performed on Sample





Boring WH-01

ECMS

# **ENGINEER'S LOG**

District: _____ County: Philadelphia

SR ______ Section _____

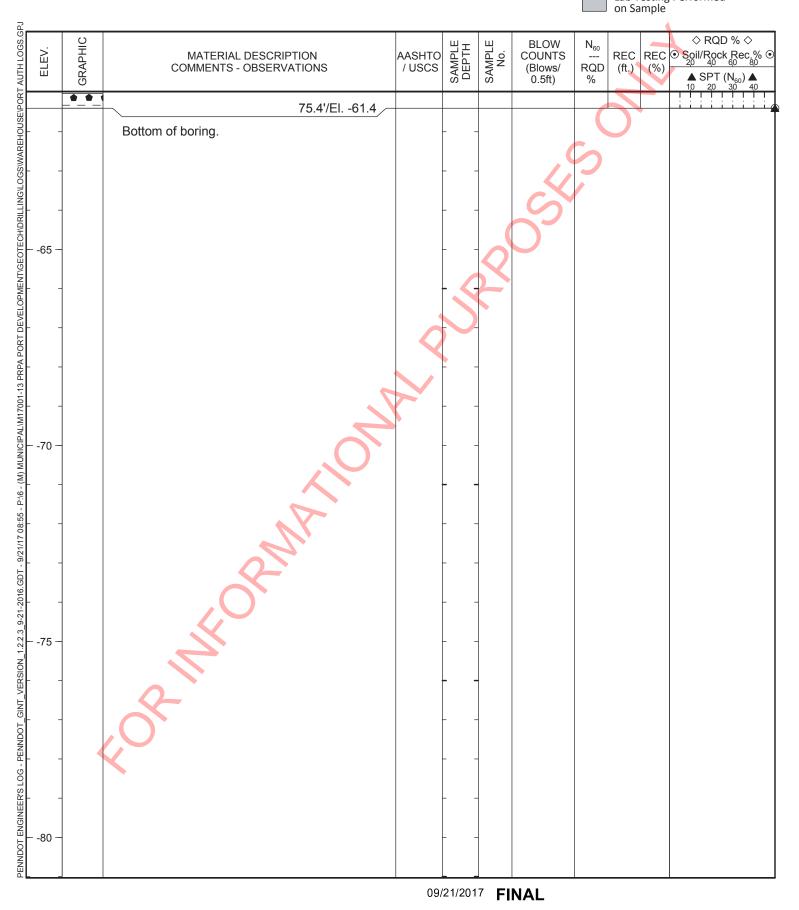
Sta. _____ Offset _____

Sheet <u>5</u> of <u>5</u>

51100 <u>5</u>01 <u>5</u>

<u>NOTE:</u> N values and all graphical plots are for information only.

Lab Testing Performed



	DEPART	INSYLVANIA	ENGINEE	R'S LO	G					Shee	et <u>1</u> c	of_4	
Borin	- ng <b>WH</b> -	- <b>02</b> ECMS					Г		TIT	TIT			
		County: Philadelphia	Drilling Start: _07	7/25/201	7 12:5	8 pm		H		GIQTER		Ĥ.	
		Section	_					AS	PRO	FESSI	ONAL A	FA .	
Basel	line: <u>FD</u>	C Site - Port Authority	Grouting Comple	ete: <u>08/0</u>	1/201				nile	1.Ku	Lill	te	
		Offset	_					HT		NGINEE	9/21/1		
-		Offset			ic			fl-si	K/1	-Ø5353(			
Coor	dinates	:	SPT Hammer Effi	iciency:				É	×××	SYL		ŢŸ	
219	294.31	Long 70 E 2695829.6000 N	Hammer Calibra	tion Dat	e:		L	PG/PE	Seal, S	ignature	e and Dat	te	
Grou	nd Elev	. <u>13.9 ft.</u>	Hole Type:					nalle	og Ch	ockov	hac b	Appro	
Nate	er Level	Elev./Elapsed Time:	Casing Type: <u>HS</u>	SA/FJC -	Spun		ГІ Вл		arrie N			Ahhio	ve
		ft. Elapsed 0.0 hr.							9/21/2				
		ft. Elapsed <u>24.0 hr.</u>							Lab T	esting	Perfor	med	
		y B.	•						on Sa <u>E:</u> N va	Iues a	nd all gi	raphical	I
_om	pany: <u>Al</u>	lied Well Drilling	Inspector Cert. N	10. 410	- 1 /		$\sim$	plots	are fo	r infor	mation	only.	
>	HIC				빌돈	Щ	BLOW	N ₆₀	DEO	DEC		RQD %	
ELEV.	RAPHIC	MATERIAL DESCR COMMENTS - OBSER		AASHTO / USCS		SAMPLE No.	COUNTS (Blows/	RQD	(ft.)	(%)			
	Ū				N U U	N N	0.5ft)	%			10	SPT (N ₆₀	40
-			0.3'/EI. 13.6/		- 1.0 -								
		Subbase.	1.0'/EI. 12.9			S-1	9-8	11	0.8	80			ii
-		Coarse <b>SAND</b> , trace Gravel,		a-3/	- 2.0 -								\$
		homogeneous, poorly grade		sp									1/1
-		non-plastic, light brown, fill.				S-2	6-4-4-6	11	1.2	60			/ ! /! !
10			3.7'/El. 10.2										
10 -		SLAG, ASPHALT MILLINGS	4.0'/El. 9.9/		- 4.0 -						🛉	÷ †	
-	••••						4-1-2-1	<i>,</i>	4 -	7-		$\begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \end{array}$	
		SAND and SILT, very loose the lensed, well graded, sub-rou	nded, low plastic		「 <b>-</b>	S-3	4-1-2-1 Pen=0.50 tsf	4	1.5	75	/		V I
-		fines, dark gray to black, allu	ivium,		- 6.0 -								
		- clay and silt seams from 4. to 8.0'.	2 10 4.5 and 7.5		0.0						[ ]		Ĩ
-						S-4	1-1-1-1 Bon=0 25 tof	3	2.0	100			! ! ! !
	••••	- pocket penetrometer readir	ngs are from clav	a-2-4 / sm			Pen=0.25 tsf						
-		seams.			- 8.0 -								
											\		
5 —	••••					S-5	WOH-2-5-7 Pen=0.25 tsf	9	0.3	15			
											:\! !		
-					- 10.0-							······································	
			10.8'/El. 3.1				4-4-5-5						
-		CLAY and SILT, some Sand				S-6	4-4-5-5 Pen=0.25 tsf	12	1.8	90			ii
_		homogeneous, poorly grade medium plastic fines, dark g											
		alluvium.		a-6 /	- 12.0-						<b> †</b>		
-				cl	L	S-7	3-4-6-7	13	2.0	100	; ; ;		
						3-1	Pen=0.25 tsf	13	2.0				
Zo –	000		14.0'/El0.1		- 14.0-								
	0 0 0			a-3 /	14.0								
	0_0_0]			sp								iii	: :



Boring WH-02

# **ENGINEER'S LOG**

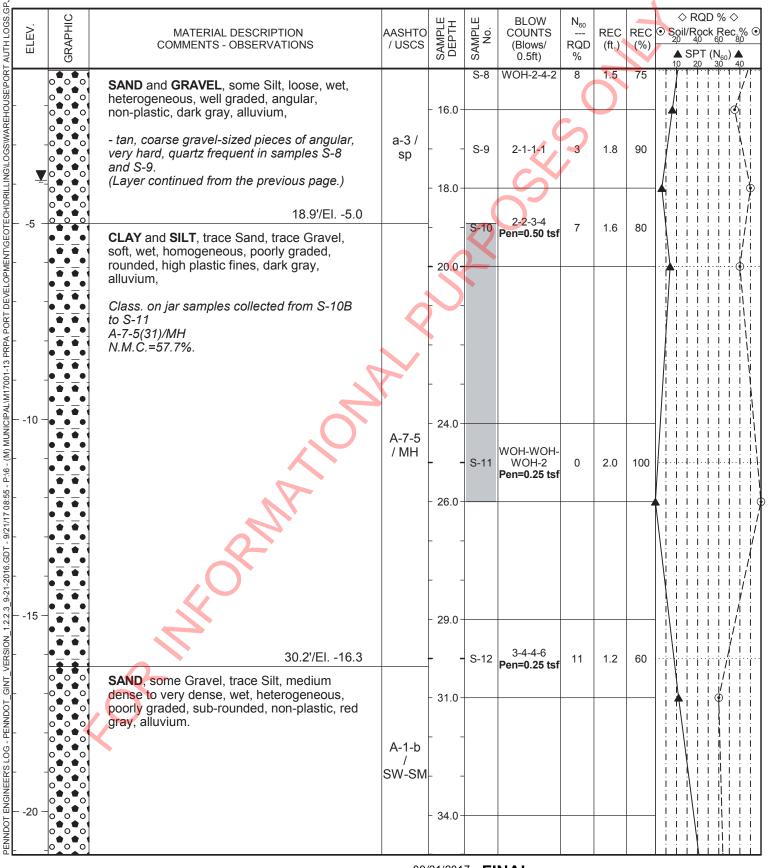
SR _____ Section _____

Sta. _____ Offset _____

District: _____ County: Philadelphia

## Sheet <u>2</u> of <u>4</u>

<u>NOTE:</u> N values and all graphical plots are for information only.





Boring WH-02

# **ENGINEER'S LOG**

SR ______ Section _____

Sta. _____ Offset _____

District: _____ County: Philadelphia

## Sheet <u>3</u> of <u>4</u>

**<u>NOTE</u>**: N values and all graphical plots are for information only.

ELEV.	MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS	AASHTO / USCS	SAMPLE DEPTH	SAMPLE No.	BLOW COUNTS (Blows/ 0.5ft)	N ₆₀  RQD %	REC (ft.)	REC (%)	⊙ Soi	l/Rock	$0\% \Leftrightarrow \frac{1}{60}$	.% ( 80
			- 36.0-	S-13	7-7-10-11	⁷⁸ 23	1.3	65				
	<ul> <li>- tan, coarse gravel-sized pieces of angular,</li> <li>very hard, quartz frequent in samples S-13,</li> <li>S-14, and S-15</li> <li>Class. on jar samples collected from S-14 to</li> <li>S-16</li> <li>A-1-b/SW-SM</li> <li>N.M.C.=13.4%.</li> </ul>	Č.	- 39.0 -	S-14	7-8-10-13	24	1.4	70			·	
		A-1-b / SW-SM	- 44.0- - 46.0-	• S-15	6-7-8-18	20	1.5	75				
-35 - 0 0	<ul> <li>brown, gray, white, green, red and purple, coarse gravel, subrounded to rounded, medium hard to very hard with frequent minerals in alluvial deposit in bottom 6" of S-16.</li> </ul>		 - 49.0-	- S-16	17-35-49-42	112	1.9	95				
-40 -40	o o o o o o o o o o o o o o o o o o o	A-1-a / SP	- 51.0 -  - 54.0 -									



Boring **WH-02** 

ECMS

# **ENGINEER'S LOG**

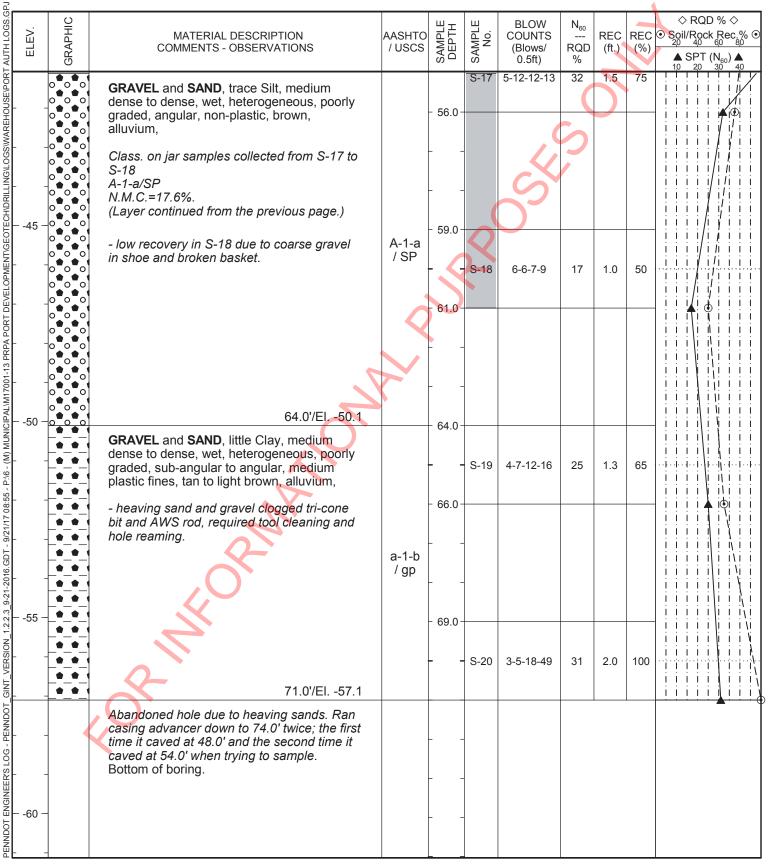
SR _____ Section _____

Sta. _____ Offset _____

District: _____ County: Philadelphia

### Sheet 4 of 4

<u>NOTE:</u> N values and all graphical plots are for information only.



6	DEPART	<b>NSYLVANIA</b> MENT OF TRANSPORTATION	ENGINEE	R'S LO	G					Shee	et <u>1</u> of	5
Boring	WH-	03 ECMS					]		TIT	TTTT NWE		
	-	County: Philadelphia	Drilling Start: _0	7/31/201	7 2:05	pm		H		GISTER		2
R		Section	Drilling Complet	e: <u>08/01</u>	2017	12:45	pm		PROF	ESSIC		Ĥ,
Baselir	ne: <u>FD(</u>	C Site - Port Authority	Grouting Comple	ete: <u>08/0</u>	2/201	7 11:4	15 am			UK.	Lilet	2X
		Offset						H			9/21/17	-A
egme	ent	Offset	Hammer Type: _	Automat	ic			H-	(//)	NGINEE -053530	V /// V	K)
Coordi	nates:		SPT Hammer Eff					Ĥ		SYX		ŕ
Lat	11.00	Long 60 E 2696277.2210 N	Assumed 0.8 Hammer Calibra					PG/PF	Seal Si		and Date	
Groun	44.005 d Elev.	<u>13.1 ft.</u>	Hole Type:									
		Elev./Elapsed Time:	Casing Type: <u>H</u> S	SA/FJC -	Spun						d and Ap	• •
		ft. Elapsed <u>0.0 hr.</u>					2000	1			son	
		Elapsed <u>23.0 hr.</u>						ate:_				
		, В.							on Sa	mple	Performe	
Compa	any: <u>Alli</u>	ied Well Drilling	Inspector Cert. N	lo. <u>410-</u>	17		S	<u>NOTI</u> plots	<u>:</u> N va are fo	lues ar r infor	nd all grap mation or	ohical nly.
	0				111		DIAN		_			QD % ◊
ELEV.	RAPHIC	MATERIAL DESCR		AASHTO / USCS	IPLE PTH	SAMPLE No.	BLOW COUNTS	N ₆₀	REC	REC		
	SRA	COMMENTS - OBSER	VATIONS	/ USCS	SAN	SAN	(Blows/ 0.5ft)	RQD %	(ft.)	(%)		
							,				10 20	$T(N_{60}) \triangleq 30 40$
-			0.4'/El. 12.8									
		Subbase, coarse cobble-siz	/ г		- 1.0 -						İİİİ	İİİİ
0		pieces.		0.24		S-1	16-12	16	1.0	100		
-0	0 0	/	1.0'/El. 12.1	a-2-4 / sm	- 2.0 -						, i i <b>†</b> i	
0		SAND and GRAVEL, some	Silt, medium 🛛 🦿				0 5 7 40					
10 -0		$\sqrt{\frac{1}{2}}$ dense, wet, heterogeneous, $\sqrt{\frac{1}{2}}$ sub-rounded to sub-angular	well graded,	a-6 /		S-2	8-5-7-10 Pen=3.00 ts	<b>f</b> 16	1.0	50		
0		fines, brown and red black,	fill.	cl								
-			3.0'/EI. 10.1/		- 4.0 -						, i i <del>∱</del> i	$\mathcal{P}$
•		CLAY and SILT, some Grav										
-•		wet, heterogeneous, poorly sub-rounded to sub-angular	graded, medium plastic			S-3	7-4-3-3	9	0.3	15		
	• • •	fines, light brown to light gra										
		- trace pyrite in S-2.	4.0'/El. 9.1		- 6.0 -							
_		SAND and SILT, some Grav					2-1-2-3					
<b>_</b>		lensed, well graded, rounde				S-4	Pen=0.25 ts	f 4	2.0	100		
	• • •	plastic fines, dark brown to l	olack, fill.									i i j`
5 -				a-2-4 / sm	- 8.0 -						1111	
•				/ 311		0.5	1-1-2-1			100		
	• • •					S-5	Pen=0.25 ts	f ⁴	2.0	100		
					10.0							
- •]		- tar odor in S-5 and S-6.			- 10.0-							
	••••					S-6	1-1-1-1	. 3	4 7	0.5		
		.()				5-6	Pen=0.25 ts	f ³	1.7	85		
					_ 12.0							
-			12.5'/El. 0.6		- 12.0-						1	
0	0 0					S-7	WOH-1-8-8	12	0.6	30		1/1
0 -0	00					3-1	vv∪⊟-1-8-8	12	0.0	30		
0				A-2-4 / SM	- 14.0-							
					14.0-							
				1			1	1			ידרי ה	(1.1.1.1.



Boring WH-03

# **ENGINEER'S LOG**

SR ______ Section _____

Sta. _____ Offset _____

District: _____ County: Philadelphia

## Sheet <u>2</u> of <u>5</u>

**<u>NOTE</u>**: N values and all graphical plots are for information only.

Lab Testing Performed on Sample

ELEV.	GRAPHIC	MATERIAL DESCRIPTION COMMENTS - OBSERVATIONS	AASHTO / USCS	SAMPLE DEPTH	SAMPLE No.	BLOW COUNTS (Blows/ 0.5ft)	N ₆₀  RQD %	REC (ft.)	REC (%)	⊙ Sc 2(	gil/R	QD % ock R or (N ₆	lec.%	, (
-		<b>SAND</b> , little Silt, trace Gravel, medium dense, wet, heterogeneous, poorly graded, sub-rounded to sub-angular, non-plastic, brown, fill,		- 16.0-	S-8	2-3-7-7	70	1.6	80					
-5 -		Class. on jar samples collected from S-8 to S-9 A-2-4(0)/SM N.M.C.=19.8%.	A-2-4 / SM		S-9	5-4-3-3	9	2.0	100					,
-		(Layer continued from the previous page.) 19.2'/El6.1 CLAY and SILT, trace Sand, stiff, wet, homogeneous, poorly graded, rounded,			S-10	2-2-2-3 Pen=1.00 tsf	5	2.0	100					
-		medium plastic fines, dark gray, fill.	, O	- 20.0-										
 10		5	a-6 / cl											
-		- organics/weeds in sample from 25,2' to 26.0'.		- 24.0-		WOH-2-2-4								
-		26.0%EI12.9		- 26.0-	• S-11	Pen=2.00 tsf	5	2.0	100					
-		<b>SAND</b> , trace Silt, trace Gravel, medium dense to dense, wet, heterogeneous, poorly graded, sub-rounded to angular, non-plastic, brown, alluvium,												
-15 -		Class. on jar samples collected from S-12 to S-13 A-3/SP-SM N.M.C.=22.3%.		- 29.0-										
-		A	A-3 / SP-SM	- 31.0-	S-12	3-4-5-5	12	1.6	80					
-		× V												
-20														
														1



Boring WH-03

# **ENGINEER'S LOG**

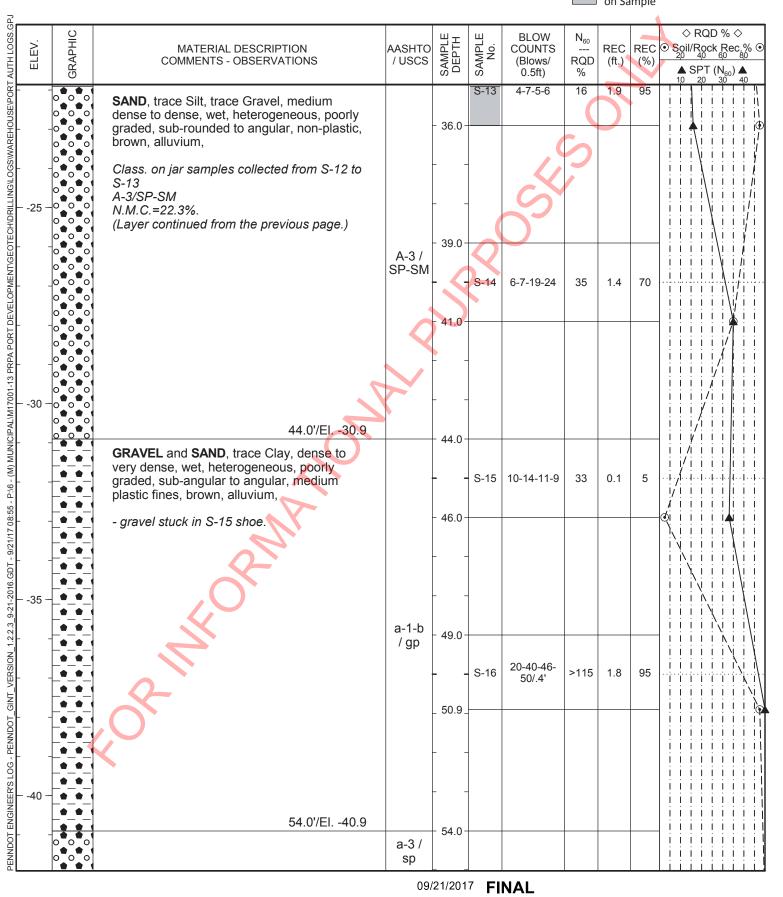
SR _____ Section _____

Sta. _____ Offset _____

District: _____ County: Philadelphia

## Sheet <u>3</u> of <u>5</u>

<u>NOTE:</u> N values and all graphical plots are for information only.





# **ENGINEER'S LOG**

Boring **WH-03** ECMS

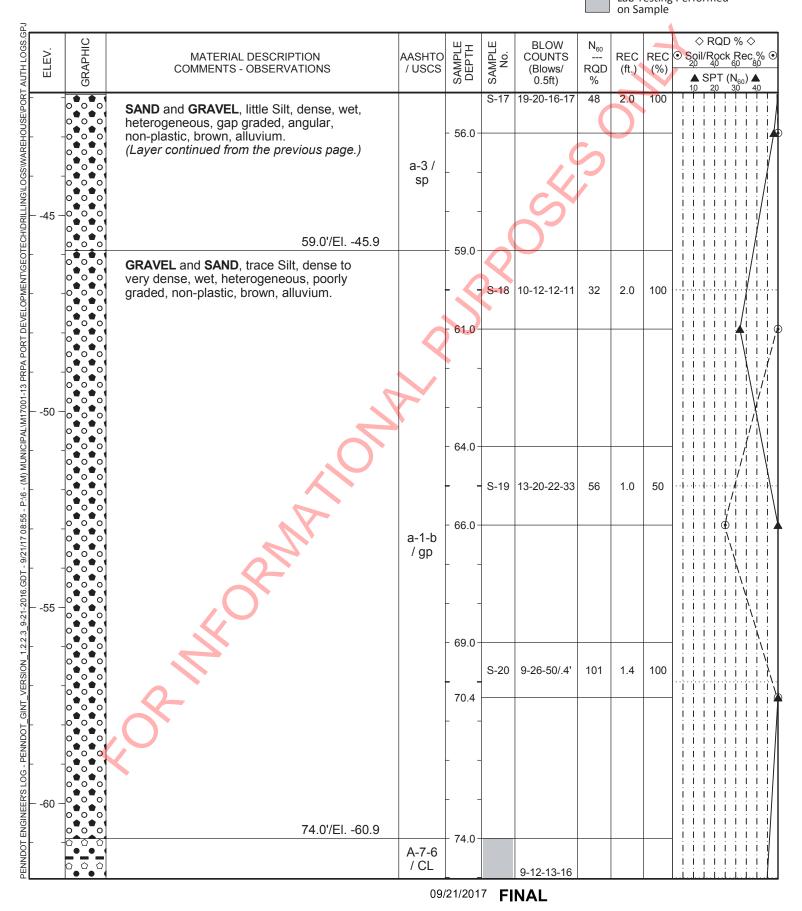
District: _____ County: Philadelphia

Sheet <u>4</u> of <u>5</u>

 SR ______
 Section _____

 Sta. ______
 Offset ______

<u>NOTE:</u> N values and all graphical plots are for information only. Lab Testing Performed





# **ENGINEER'S LOG**

Boring **WH-03** ECMS

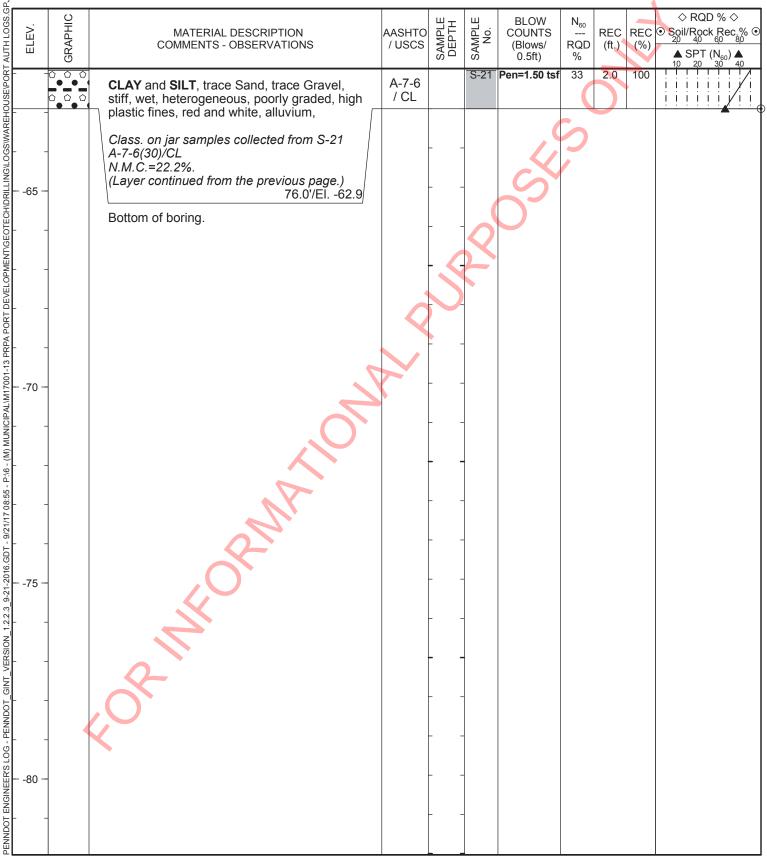
District: _____ County: Philadelphia

Sta. _____ Offset _____

SR ______ Section _____

Sheet <u>5</u> of <u>5</u>

<u>NOTE:</u> N values and all graphical plots are for information only.



1	DEPAR	INSYLVANIA TMENT OF TRANSPORTATION	ENGINEE	R'S LO	G					Shee	et <u>1</u> c	of 5	
Borin	_	- <b>04</b> ECMS										<u> </u>	
		County: Philadelphia	Drilling Start: 07	7/26/201	7 1.00	nm				NWE		A	
		Section	-				pm	- AS		EGISTER		A	
		C Site - Port Authority	<b>e</b> 1							/. h/.		te	1
		Offset						n'a	ng	J. WHI	9/21/1	7	
		Offset	_					A -	E		R //		
	dinates		SPT Hammer Effi	ciency:				Ĥ		=-05353		·//	
		Long							Cool C		and Dat	ha	
		40 E 2695791.4020 N /12.9 ft	Hammer Calibrat Hole Type:					FG/FE	3edi, 3			e	
		Elev./Elapsed Time:						inal Lo					
		<u>) ft.</u> Elapsed <u>0.0 hr.</u>						3y: <u>Ca</u>					
		ft. Elapsed 24.0 hr.						Date:_					
		<u>у В.</u>							on Sa	oldum	Perform		
Com	pany: <u>Al</u>	llied Well Drilling	Inspector Cert. N	o. <u>410-</u>	17		S	NOT plots	<u>E:</u> N va are fo	lues a or infor	nd all gr mation	aphic only	cal
	0						BLOW					, RQD	
ELEV.	GRAPHIC			AASHTO	SAMPLE	SAMPLE No.	COUNTS	N ₆₀	REC	REC	⊙ Soil/I		
Ц	GRA	COMMENTS - OBSER	IVATIONS	/ USCS	SAN	SAI	(Blows/ 0.5ft)	RQD %	(ft.)	(%)		_	N ₆₀ ) ▲ 30 40
		BITUMINOUS CONCRETE.										<del>1  </del>	
			0.5'/El. 12.5										
	0 0 0	Subbase.	$\square$		- 1.0 -	C 1	10.12	16	0.2	20			
	0 0 0		1.0'/El. 11.9/		- 2.0 -	S-1	19-12	16	0.2	20		ļ	
		GRAVEL and SAND, some			2.0							*    	
- 10 -	0 0 0	dense, wet, heterogeneous, angular, non-plastic, dark gr		a-1-b / gp		S-2	5-6-5-6	15	1.0	50		<u>, i i</u>	
	0 0 0	- <u>J</u> - J - J - J		0.		02		10				N I	
					- 4.0 -								İİİ
			4.5'/El. 8.4										
		SLAG, ASPHALT MILLINGS	S, AND TAR,			S-3	8-5-6-8	15	1.6	80	<u>.</u>		Nii
		1111.											
			6.0'/El. 6.9		- 6.0 -								1
		GRAVEL and SAND, some to medium dense, moist, he										\i i	
	<b>o</b> o o	well graded, sub-angular, no				S-4	9-10-9-9	25	1.6	80			
_		gray to black, fill,										ili	
- 5 -		- brick, wood, and asphalt fr	agments.		- 8.0 -								
	0 0 0			a-2-4			WOH-WOF	1_				/	1/1
-		~		/ gm		S-5	2-2	3	1.0	50			//// ////
					40 -								
	0 0 0	- piece of wood stuck in S-6	shoe.		- 10.0-	1						· [ · @ ·	
					_	6.0	2-WOH-		0.2	45	∥i i İ	/ 1	
		<b>,( )</b>				S-6	WOH-3	0	0.3	15			
	000		12.0'/EI. 0.9		- 12.0-							İİ	
	0 0 0	Coarse SAND, little Silt, little			12.0-								
- 0 🔽		to medium dense, wet, hom graded, sub-rounded to sub				S-7	4-5-7-5	16	2.0	100	Ni	1L	
		non-plastic, dark gray, alluvi		a-3 /									
	000			sp	- 14.0-								
	0 0 0			1		1	1	1	1	1	1 i i/i		1 1 1



Boring **WH-04** 

## **ENGINEER'S LOG**

ECMS Distric

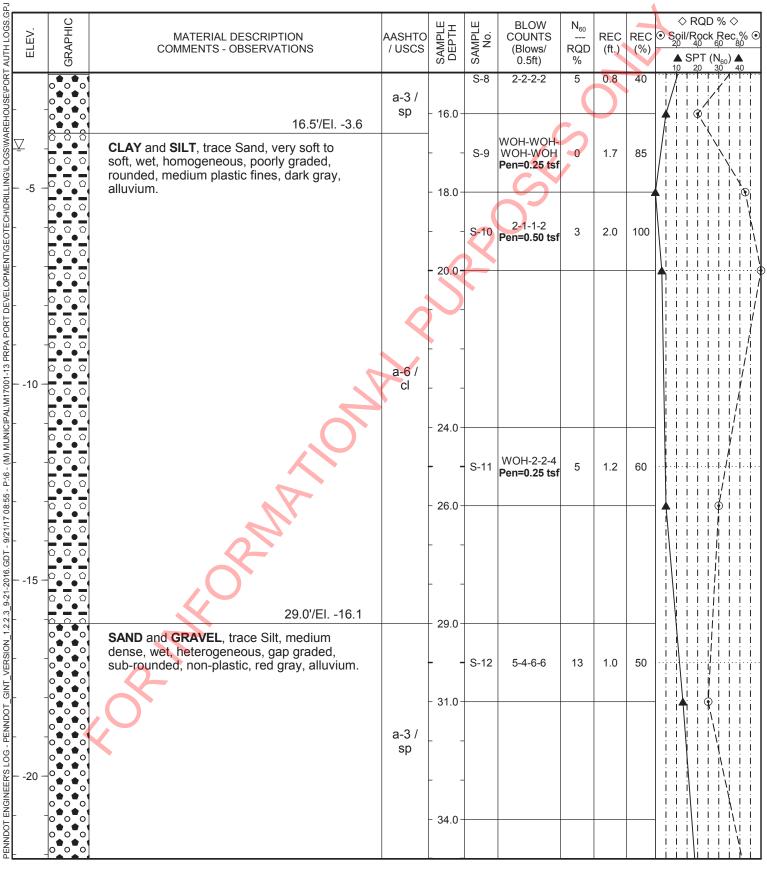
District: _____ County: Philadelphia _____ SR _____ Section _____

Sta. _____ Offset _____

Sheet <u>2</u> of <u>5</u>

<u>NOTE:</u> N values and all graphical plots are for information only.

Lab Testing Performed on Sample





Boring WH-04

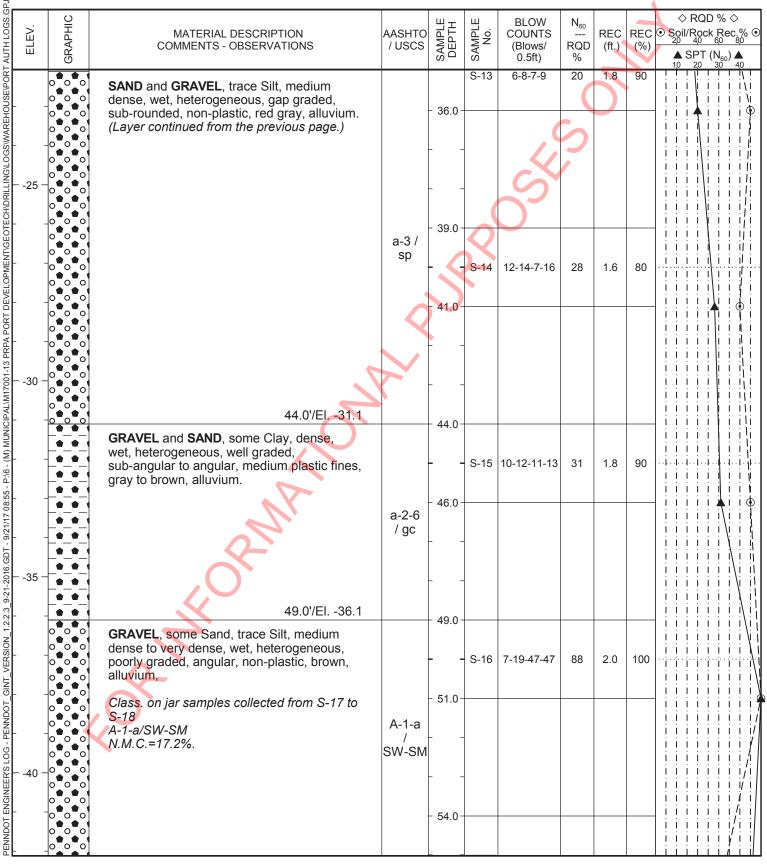
# ENGINEER'S LOG

District: _____ County: Philadelphia _____ SR ______ Section _____

Sta. _____ Offset _____

## Sheet <u>3</u> of <u>5</u>

**<u>NOTE</u>**: N values and all graphical plots are for information only.





## **ENGINEER'S LOG**

Boring WH-04 ECMS

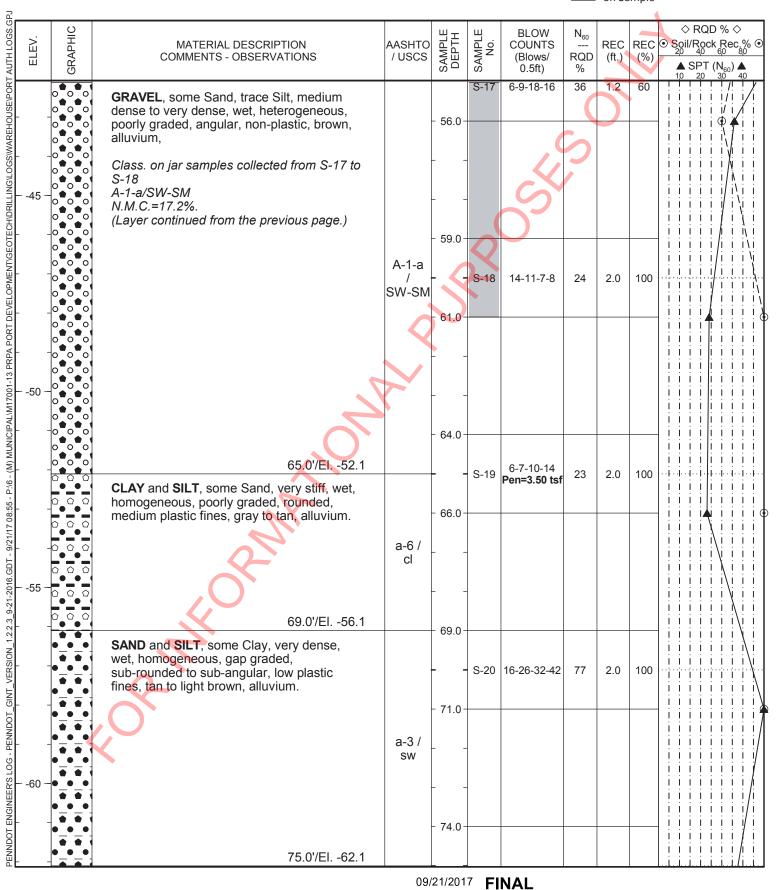
District: _____ County: Philadelphia

SR _____ Section _____

Sta. _____ Offset _____

Sheet <u>4</u> of <u>5</u>

<u>NOTE:</u> N values and all graphical plots are for information only.





# ENGINEER'S LOG

Boring **WH-04** ECMS

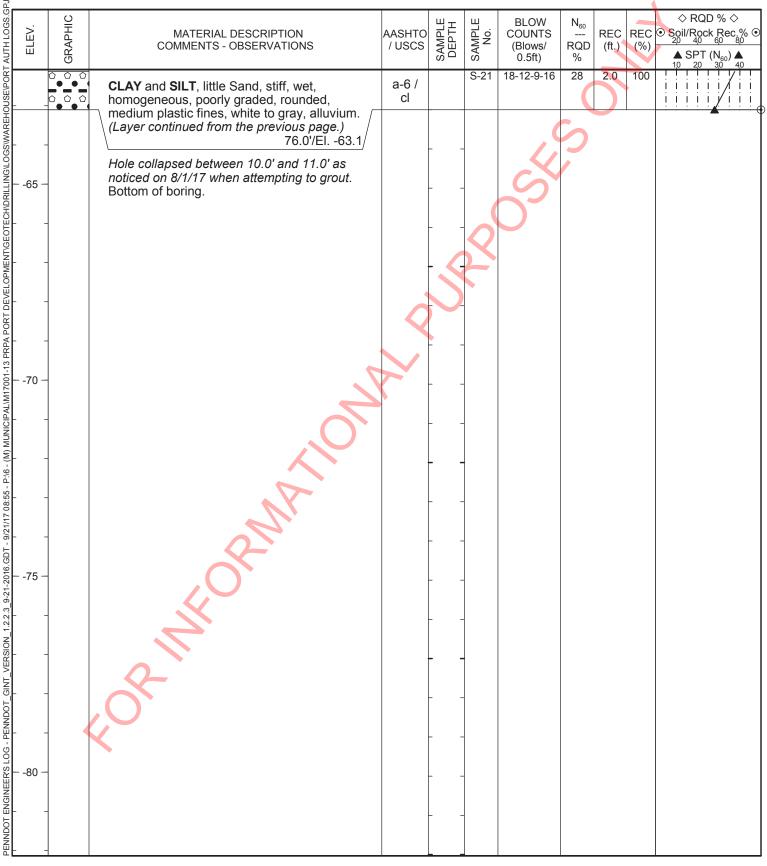
District: _____ County: Philadelphia

Sta. _____ Offset _____

SR ______ Section _____

Sheet <u>5</u> of <u>5</u>

<u>NOTE:</u> N values and all graphical plots are for information only.



	pennsylvania DEPARTMENT OF TRANSPORTATION	ENGINEE	R'S LO	G					She	et <u>1</u> of _	4
Boring	<b>WH-05</b> ECMS								TIT		<u> </u>
-	t: County: Philadelphia	– Drilling Start: 07	7/28/2017	7 2.40	рт		- A	111	NWE		
	Section	-				pm			EGISTEF		À
	ne: FDC Site - Port Authority								ressi /h/		
	Offset						Mar	nAZ	J. MH	9/21/17	
	ent Offset	_					ALS	E	NGINE		
	inates:	SPT Hammer Effi					Ĥ	PE	E-Ø5353	30-E	У
Lat.	Long	Assumed 0.8	Me						SYL		
21842	21.0550 E 2696425.4050 N	Hammer Calibrat					PG/PE	Seal, S	ignatur	e and Date	
	d Elev. <u>13.1 ft.</u>	Hole Type:				F	inal L	og Ch	ecke	d and Ap	proved
	Level Elev./Elapsed Time:									lson .	-
	II <u>11.6 ft.</u> Elapsed <u>-0.1 hr.</u>	-		-	•		Date: _	9/21/2	2017	,	
	<u>7.2 ft.</u> Elapsed <u>47.9 hr.</u> : <u>Gary B.</u>					-		Lab T on Sa	esting	g Performe	d
	any: <u>Allied Well Drilling</u>						NOT	<u>E:</u> N va	lues a	nd all grap rmation on	hical
Joinpa	ally.		10	12			plots	are fo	or info	rmation on	ıly.
				빌폰	Щ.	BLOW	N ₆₀				0D % ◊
ELEV.	이 H MATERIAL DESCI 도 MATERIAL DESCI 전 COMMENTS - OBSEF		AASHTO / USCS	SAMPLE	SAMPLE No.	COUNTS (Blows/	RQD	REC   (ft.)	REC (%)	$\odot$ Soil/Roc $\frac{20}{40}$	
<u> </u>	5			2 N D	Ś	0.5ft)	%			▲ SPT 10 20	$(N_{60}) \underset{30}{\blacktriangle} \underset{40}{\bigstar}$
	BITUMINOUS CONCRETE.										
		0.5'/El. 12.6		- 1.0 -							
	Subbase (pulled from hole				S-1	6-6	8	1.0	100		
		SAND and CLAY, medium dense, moist, heterogeneous, gap graded, medium plastic									
<b>_</b> _											
10 - 1	fines, dark gray, fill,				S-2	5-5-6-10	15	2.0	100		
10 - 1					S-2	5-5-6-10	15	2.0	100		
	- brick, mica and asphalt m		a-2-4		S-2	5-5-6-10	15	2.0	100		
10 -			a-2-4 / sm	- 4.0 -	S-2	5-5-6-10	15	2.0	100		
	- brick, mica and asphalt m		1. 1	- 4.0 - - <b>4</b> .0 -	S-2	5-5-6-10 8-11-12-13		2.0	100		
	- brick, mica and asphalt m		1. 1	- 4.0 - - <b>4</b> .0 -							
	- brick, mica and asphalt m		1. 1	- 4.0 - - <b>-</b> -							
	- brick, mica and asphalt m	D'-6.0'.	1. 1								
	- brick, mica and asphalt mi - burnt shale waste from 4.0	0'-6.0'. 7.0'/El. 6.1	1. 1								
	<ul> <li>brick, mica and asphalt mice</li> <li>burnt shale waste from 4.0</li> <li>SILT and CLAY, some Same</li> </ul>	0'-6.0'. 7.0'/El. 6.1 d, trace Gravel,	/ sm 		S-3	8-11-12-13	31	2.0	100		
	- brick, mica and asphalt mi - burnt shale waste from 4.0 SILT and CLAY, some Sand	0'-6.0'. 7.0'/El. 6.1 d, trace Gravel, oorly graded,	/ sm		S-3	8-11-12-13	31	2.0	100		
	<ul> <li>brick, mica and asphalt mice</li> <li>burnt shale waste from 4.0</li> <li>SILT and CLAY, some Sand soft, wet, heterogeneous, prounded to sub-angular, low black, fill,</li> </ul>	0'-6.0'. 7.0'/El. 6.1 d, trace Gravel, oorly graded,	/ sm 	- 6.0 -	S-3	8-11-12-13	31	2.0	100		
	<ul> <li>brick, mica and asphalt mice</li> <li>burnt shale waste from 4.0</li> <li>SILT and CLAY, some Sand soft, wet, heterogeneous, prounded to sub-angular, low</li> </ul>	0'-6.0'. 7.0'/El. 6.1 d, trace Gravel, oorly graded,	/ sm 	- 6.0 -	S-3	8-11-12-13	31	2.0	100		
	<ul> <li>brick, mica and asphalt mice</li> <li>burnt shale waste from 4.0</li> <li>SILT and CLAY, some Sand</li> <li>Silt of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of the solution of t</li></ul>	0'-6.0'. 7.0'/El. 6.1 d, trace Gravel, oorly graded, v plastic fines, 8.5'/El. 4.6	/ sm 	- 6.0 -	S-3	8-11-12-13 6-6-8-9	19	2.0	100		
	<ul> <li>brick, mica and asphalt mice</li> <li>burnt shale waste from 4.0</li> <li>SILT and CLAY, some Sand</li> <li>Soft, wet, heterogeneous, prounded to sub-angular, low</li> <li>black, fill,</li> <li>burnt shale waste in S-4.</li> <li>SAND and SILT, very loose</li> <li>o</li> <li>o</li> <li>o</li> <li>o</li> <li>o</li> <li>o</li> </ul>	$2^{-6.0'}$ . 7.0'/El. 6.1 d, trace Gravel, oorly graded, v plastic fines, 8.5'/El. 4.6 to medium , poorly graded,	/ sm 	- 6.0 -	S-3	8-11-12-13 6-6-8-9	19	2.0	100		
	<ul> <li>brick, mica and asphalt mice</li> <li>burnt shale waste from 4.0</li> <li>SILT and CLAY, some Sand</li> <li>Soft, wet, heterogeneous, prounded to sub-angular, low</li> <li>black, fill,</li> <li>burnt shale waste in S-4.</li> <li>SAND and SILT, very loose dense, wet, heterogeneous</li> <li>sub-angular to sub-rounded</li> </ul>	$2^{-6.0'}$ . 7.0'/El. 6.1 d, trace Gravel, oorly graded, v plastic fines, 8.5'/El. 4.6 to medium , poorly graded,	/ sm 	- 6.0 - 	S-3	8-11-12-13 6-6-8-9	19	2.0	100		
	<ul> <li>brick, mica and asphalt mice</li> <li>burnt shale waste from 4.0</li> <li>SILT and CLAY, some Sand soft, wet, heterogeneous, prounded to sub-angular, low black, fill,</li> <li>burnt shale waste in S-4.</li> <li>SAND and SILT, very loose dense, wet, heterogeneous sub-angular to sub-rounded black, fill,</li> </ul>	$2^{-6.0'.}$ 7.0'/El. 6.1 d, trace Gravel, oorly graded, v plastic fines, 8.5'/El. 4.6 to medium , poorly graded, l, non-plastic,	/ sm 	- 6.0 - 	S-3	8-11-12-13 6-6-8-9	19	2.0	100		
	<ul> <li>brick, mica and asphalt mice</li> <li>burnt shale waste from 4.0</li> <li>SILT and CLAY, some Sand</li> <li>Soft, wet, heterogeneous, prounded to sub-angular, low</li> <li>black, fill,</li> <li>burnt shale waste in S-4.</li> <li>SAND and SILT, very loose dense, wet, heterogeneous</li> <li>sub-angular to sub-rounded</li> </ul>	$2^{-6.0'.}$ 7.0'/El. 6.1 d, trace Gravel, oorly graded, v plastic fines, 8.5'/El. 4.6 to medium , poorly graded, l, non-plastic,	/ sm a-4 / ml a-2-4	- 6.0 -  - 8.0 -  - 10.0 -	S-3 S-4 S-5	8-11-12-13 6-6-8-9 2-1-2-1	31 19 4	2.0 2.0 1.0	100 100 50		
	<ul> <li>brick, mica and asphalt mice</li> <li>burnt shale waste from 4.0</li> <li>SILT and CLAY, some Sand soft, wet, heterogeneous, prounded to sub-angular, low black, fill,</li> <li>burnt shale waste in S-4.</li> <li>SAND and SILT, very loose dense, wet, heterogeneous sub-angular to sub-rounded black, fill,</li> </ul>	$2^{-6.0'.}$ 7.0'/El. 6.1 d, trace Gravel, oorly graded, v plastic fines, 8.5'/El. 4.6 to medium , poorly graded, l, non-plastic,	/ sm a-4 / ml	- 6.0 - 	S-3 S-4 S-5	8-11-12-13 6-6-8-9 2-1-2-1	31 19 4	2.0 2.0 1.0	100 100 50		
	<ul> <li>brick, mica and asphalt mice</li> <li>burnt shale waste from 4.0</li> <li>SILT and CLAY, some Sand soft, wet, heterogeneous, prounded to sub-angular, low black, fill,</li> <li>burnt shale waste in S-4.</li> <li>SAND and SILT, very loose dense, wet, heterogeneous sub-angular to sub-rounded black, fill,</li> </ul>	$2^{-6.0'.}$ 7.0'/El. 6.1 d, trace Gravel, oorly graded, v plastic fines, 8.5'/El. 4.6 to medium , poorly graded, l, non-plastic,	/ sm a-4 / ml a-2-4	- 6.0 -  - 8.0 -  - 10.0 -	S-3 S-4 S-5	8-11-12-13 6-6-8-9 2-1-2-1	31 19 4	2.0 2.0 1.0	100 100 50		
	<ul> <li>brick, mica and asphalt mice</li> <li>burnt shale waste from 4.0</li> <li>SILT and CLAY, some Sand soft, wet, heterogeneous, prounded to sub-angular, low black, fill,</li> <li>burnt shale waste in S-4.</li> <li>SAND and SILT, very loose dense, wet, heterogeneous sub-angular to sub-rounded black, fill,</li> </ul>	$2^{-6.0'.}$ 7.0'/El. 6.1 d, trace Gravel, oorly graded, v plastic fines, 8.5'/El. 4.6 to medium , poorly graded, l, non-plastic,	/ sm a-4 / ml a-2-4	- 6.0 -  - 8.0 -  - 10.0 -	S-3 S-4 S-5	8-11-12-13 6-6-8-9 2-1-2-1	31 19 4 13	2.0 2.0 1.0	100 100 50		
	<ul> <li>brick, mica and asphalt mice</li> <li>burnt shale waste from 4.0</li> <li>SILT and CLAY, some Sand soft, wet, heterogeneous, prounded to sub-angular, low black, fill,</li> <li>burnt shale waste in S-4.</li> <li>SAND and SILT, very loose dense, wet, heterogeneous sub-angular to sub-rounded black, fill,</li> </ul>	$2^{-6.0'.}$ 7.0'/El. 6.1 d, trace Gravel, oorly graded, v plastic fines, 8.5'/El. 4.6 to medium , poorly graded, l, non-plastic,	/ sm a-4 / ml a-2-4	- 6.0 -  - 8.0 -  - 10.0 -	S-3 S-4 S-5 S-6	8-11-12-13 6-6-8-9 2-1-2-1 2-8-2-1	31 19 4 13	2.0 2.0 1.0	100 100 50 80		
	<ul> <li>brick, mica and asphalt mice</li> <li>burnt shale waste from 4.0</li> <li>SILT and CLAY, some Sand soft, wet, heterogeneous, prounded to sub-angular, low black, fill,</li> <li>burnt shale waste in S-4.</li> <li>SAND and SILT, very loose dense, wet, heterogeneous sub-angular to sub-rounded black, fill,</li> </ul>	$2^{-6.0'.}$ 7.0'/El. 6.1 d, trace Gravel, oorly graded, v plastic fines, 8.5'/El. 4.6 to medium , poorly graded, l, non-plastic,	/ sm a-4 / ml a-2-4	- 6.0 -  - 8.0 -  - 10.0 -	S-3 S-4 S-5 S-6	8-11-12-13 6-6-8-9 2-1-2-1 2-8-2-1	31 19 4 13	2.0 2.0 1.0	100 100 50 80		



ECMS

Boring WH-05

### **ENGINEER'S LOG**

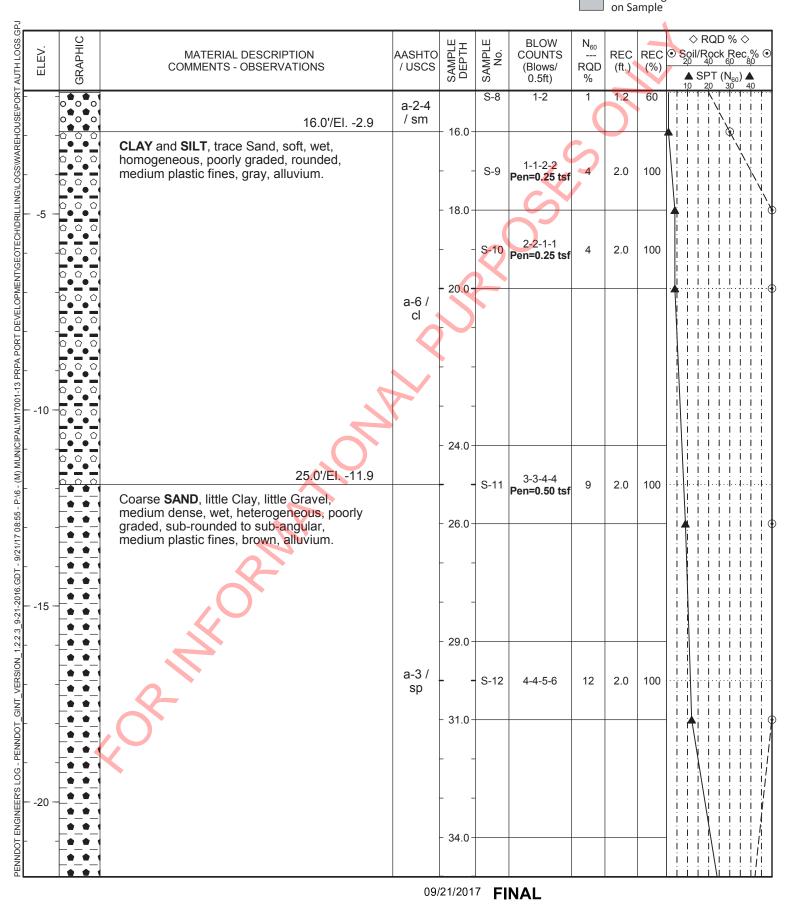
District: _____ County: Philadelphia _____ SR ______ Section _____

Sta. _____ Offset _____

#### Sheet <u>2</u> of <u>4</u>

<u>NOTE:</u> N values and all graphical plots are for information only.

Lab Testing Performed





ECMS

Boring WH-05

### ENGINEER'S LOG

SR _____ Section _____

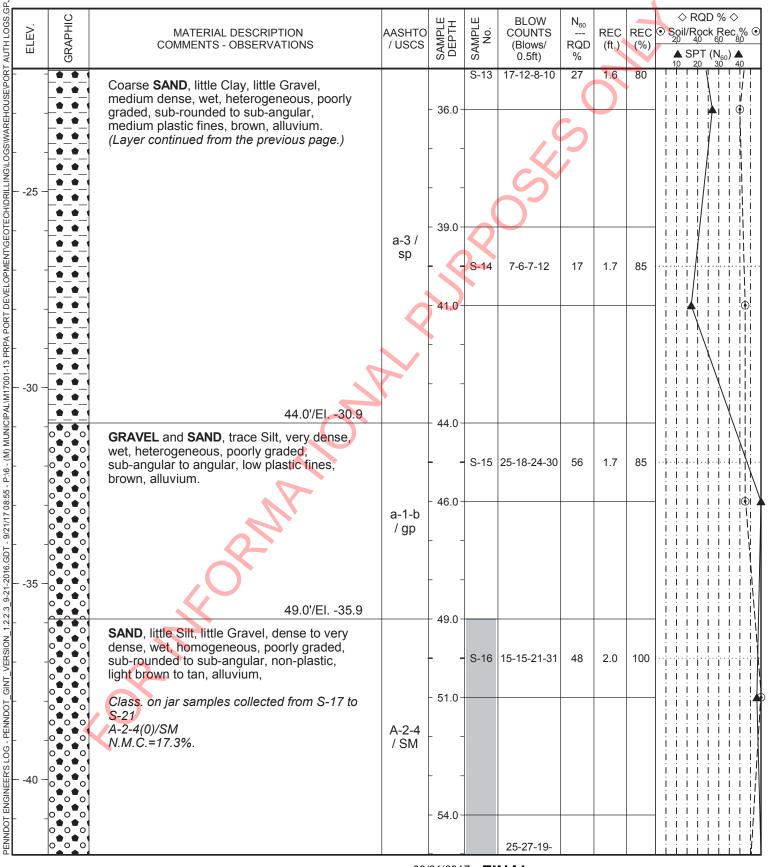
Sta. _____ Offset _____

District: _____ County: Philadelphia

#### Sheet <u>3</u> of <u>4</u>

**<u>NOTE:</u>** N values and all graphical plots are for information only.

Lab Testing Performed on Sample



09/21/2017 FINAL



ECMS

Boring WH-05

### **ENGINEER'S LOG**

SR _____ Section _____

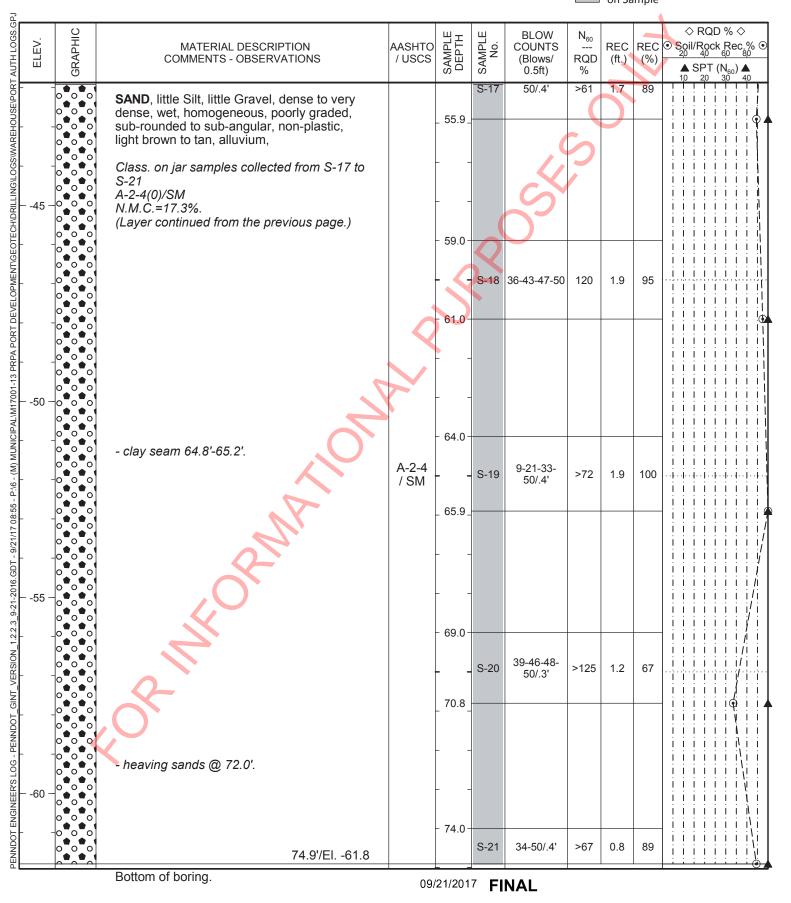
Sta. _____ Offset _____

District: _____ County: Philadelphia

#### Sheet <u>4</u> of <u>4</u>

**<u>NOTE</u>**: N values and all graphical plots are for information only.

Lab Testing Performed on Sample

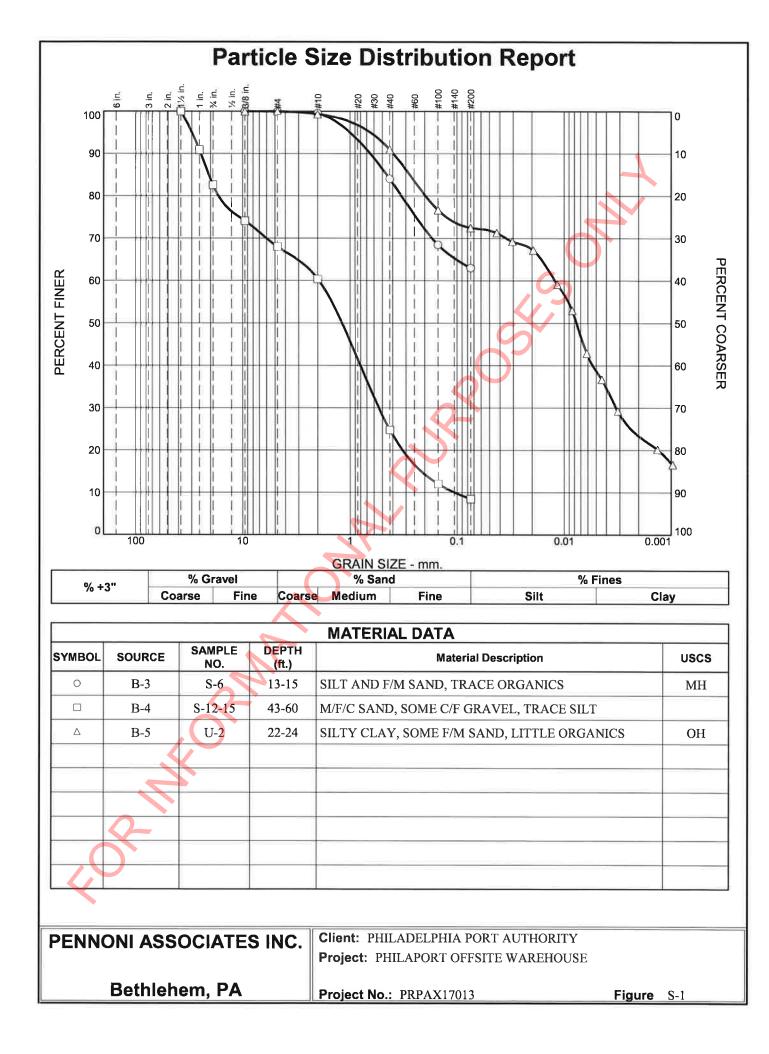


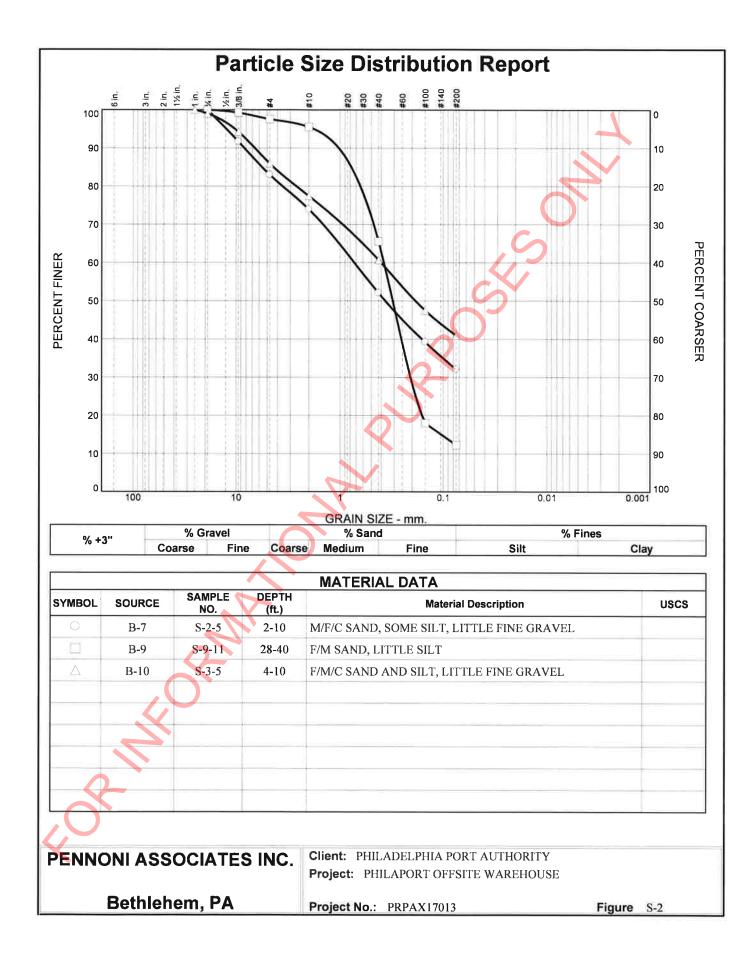
ADIX B - Labor.

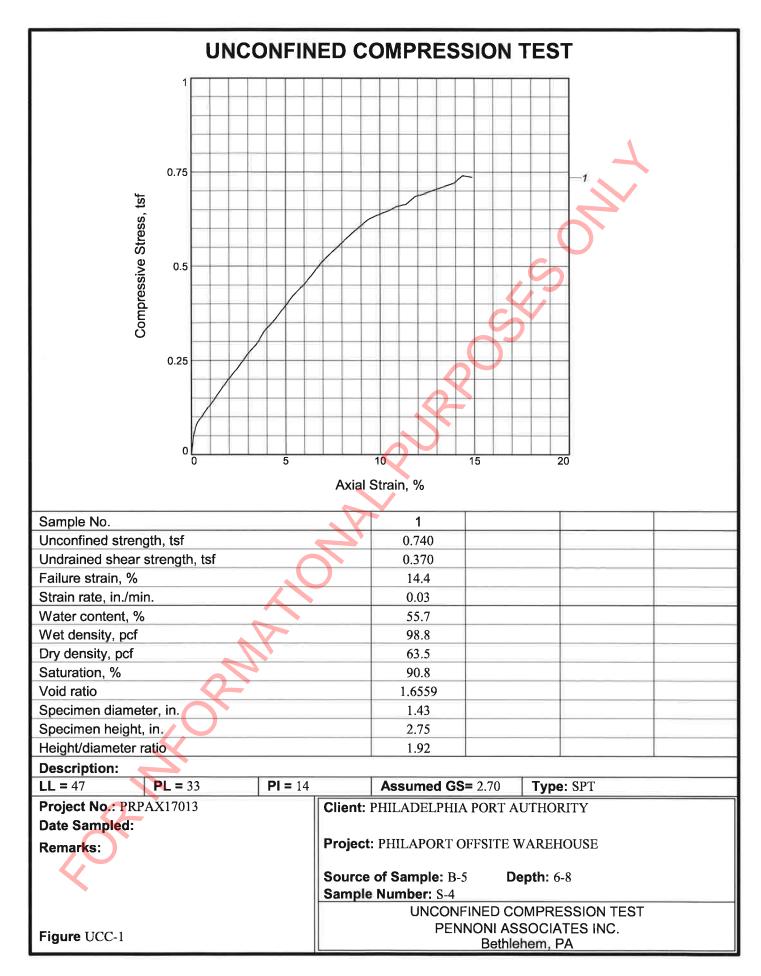


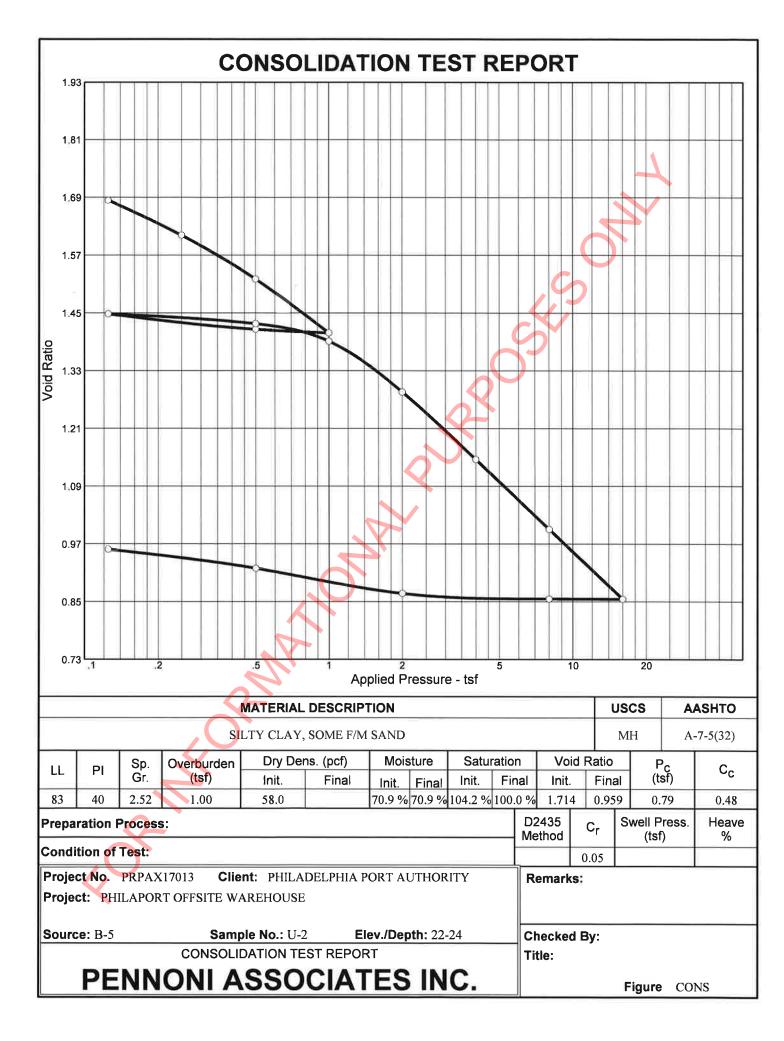
1		· · · · · · · · · · · · · · · · · · ·	r	-	-	_	_	_	_	_	_	_	_	_	_	-	-	<u> </u>		 			_	_	_	_	_	_		_	
	ЧСТН	(%) NIVALS TVIXV					14.4																								
	SHEAR STRENGTH	COHESION (f2l)					0.37																						e		
	SHEAR	ELKENGLH (121) COWEKESZIAE NACONEINED					0.74																						PRPAX 17013	L-1	
	<b>OKGANIC CONTENT %</b>						7.9	10.5						26.2														1	PRP.		l
	COWFRESSION INDEX (Cc)							0.49										Γ										0.:		E NO.	
	KECOW6KE22ION INDEX (C ¹ )							0.03										Γ	Γ						V			JOB No.		IABLE NO.	
	N						0.95																	2							
	N	GETANDARD/MODIFIED																				Ņ							SOOS		l
	COMPACTION DATA	CONTENT % OPTIMUM MOISTURE																		C	X C								'AREH		
DATA	COM	DENZILA (bei) WAXIMUM DRY																		)									PHILAPORT DISTRIBUTION WAREHOUSE	PHILADELPHIA, PA	
	VOLUMETRIC	S&TURATION % DECREE OF					91	100									C		K										RIBUT	DELP	
		(9) ΟΙΤΑЯ ΟΙΟΥ					1.66	1.71							1		Þ												T DIST	PHILA	
ABUKAIUKY		DRY UNIT WEIGHT (pei)					63.5	58.0							K													T:	APOR	NO.	
LAB		SPECIFIC GRAVITY (G) (*) ASSUMED					2.70*	2.52																				<b>PROJECT:</b>	IHH	LUCATION:	
5	% M	WOISTURE CONTENT w %			11.8		55.7	70.9	27.3		20.5		35.4	131.2															2018	8/0	
<b>NININIAK</b>		<b>ΓΙΟΠΙΣΙΧ ΙΝDEX Ι</b> ^Γ					1.6	<u>C:</u> 0																				DATE	1/22/	UAIE:	
	PLASTICITY	brvelicila index 1 ^b	NP				14	40						NP																N22	
	PLAST	PLASTIC LIMIT WP	86		5		33	43																			0				
		LIQUID LIMIT WI	84					83																				Y:	.714	BY:	
	GRAIN SIZE DISTRIBUTION	% AVTO/LTIS	63	ノ	6			34/39	32		12		41															DRAWN BY	RJE	CHECKED	
	GRAIN SIZE ISTRIBUTIO	% anvs	37		60			27	51		85		46															DRA			
	DIS	CRAVEL %			31				17		ω		13																NC.		
	SOIL GROUP SYMBOL						oL	НО																					TES I		
		DEPTH (ft)	13-15		43-60		6-8	22-24	2-10		28-40		4-10	18-20															<b>PENNONI ASSOCIATES INC.</b>		
		SAMPLE NUMBER	S-6		S-12-15		S-4	U-2	S-2-5		S-9-11		S-3-5	S-7															ONI A		
		BOBINC NUMBER	B-3		B-4		B-5		B-7		B-9		B-10																PENN		

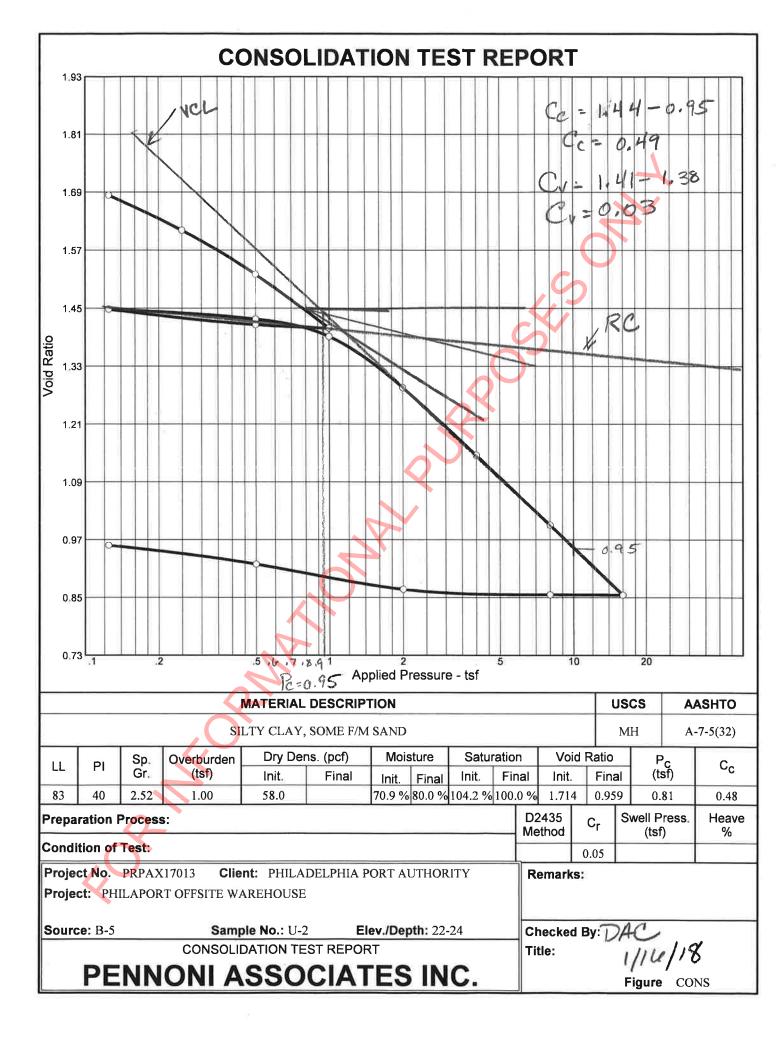
SUMMARY OF LABORATORY DATA

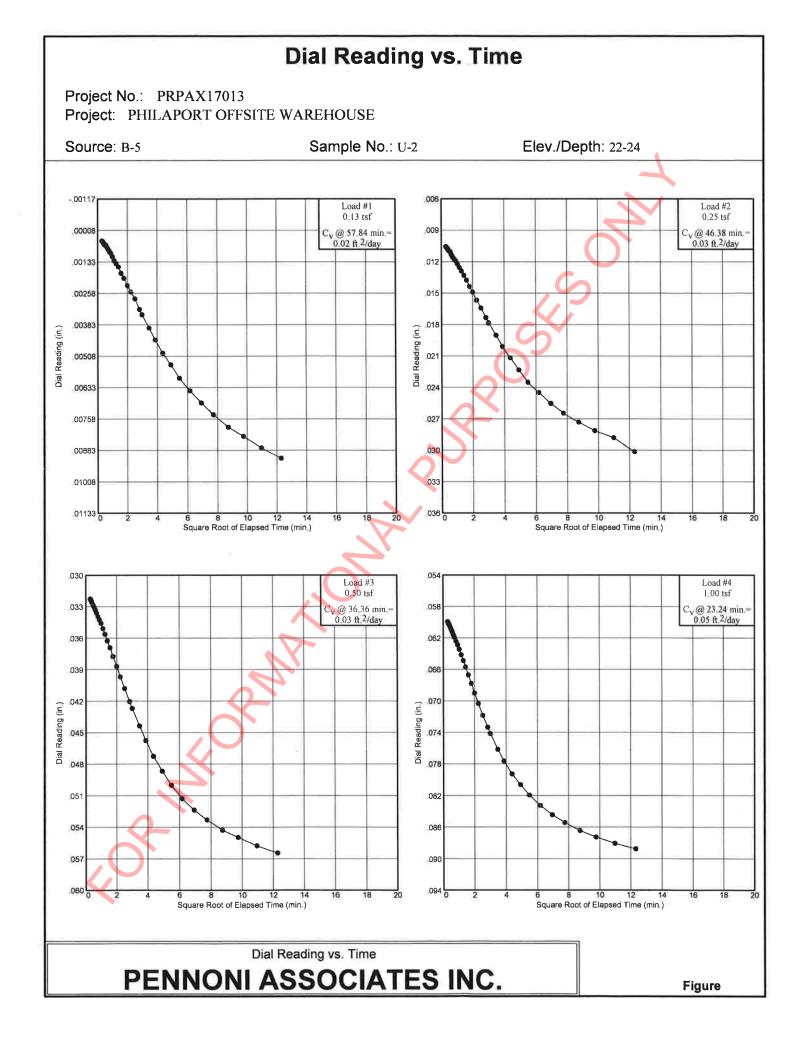


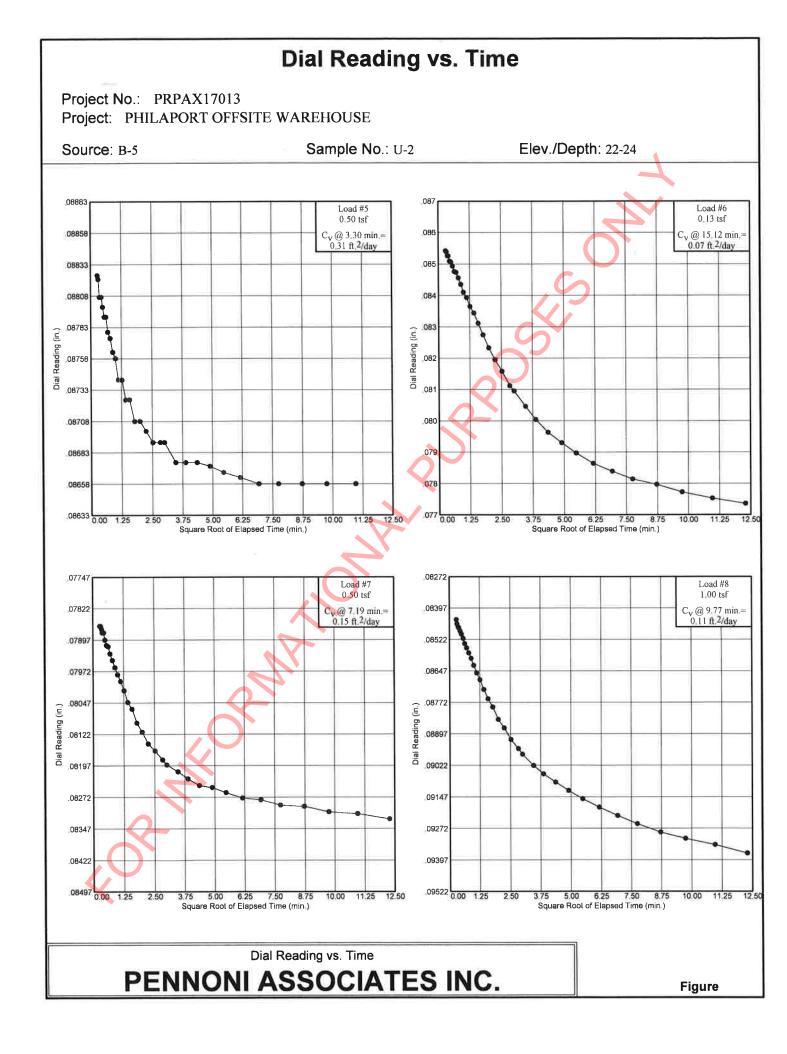


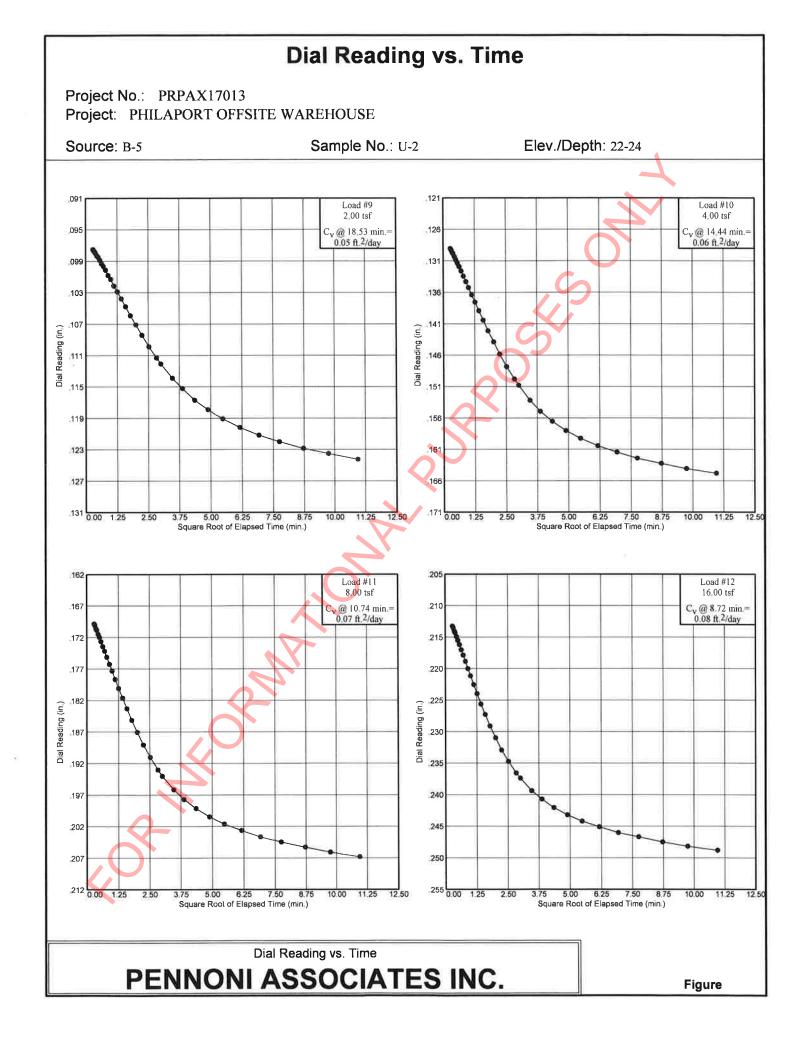


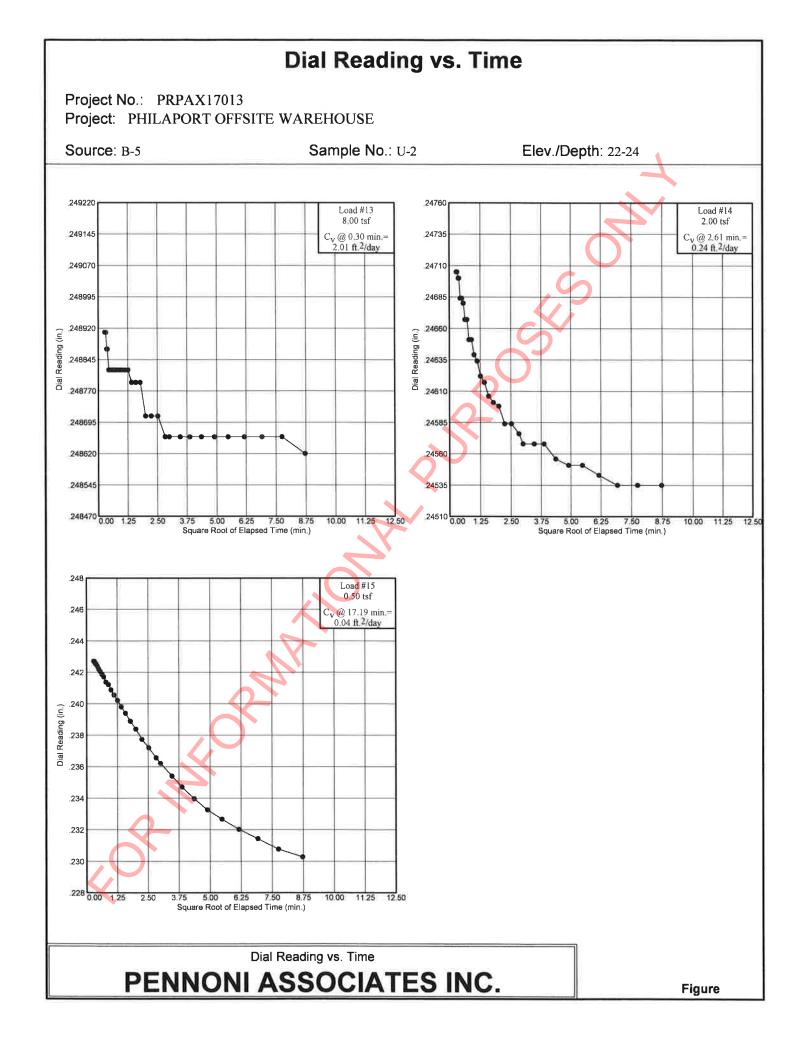












### LABORATORY TESTING PROCEDURES

All testing is either done in accordance with the indicated ASTM Designation-latest edition, or with other standard or generally accepted engineering practice as described:

- <u>Consolidation Test of Soils</u> Preparation of samples and testing procedures generally follow the methods described in Lambe, op. Cit. In addition, the time of loading may be selected on the basis of:
  - a. Controlled rate of percent of consolidation
  - b. Controlled pore pressure gradient
  - c. Controlled strain

The method of test is selected to suit the soil type in question and the test is conducted in accordance with generally accepted engineering practice.

- 2. Atterberg Limits Plasticity Indices
  - a. Liquid limit of soils, ASTM D 4318
  - b. Plastic limit and plasticity index of soils, ASTM D 4318
  - c. Shrinkage factors of soils, ASTM D 427

(Moisture content is also determined with the Atterberg Limit test, and liquidity index is also computed)

- 3. <u>Moisture Content of Soil</u> ASTM D 2216
- Particle Size Analysis of Soils ASTM D 421, Dry preparation of soil samples; ASTM D 422, Sieve and/or hydrometer analysis.
- <u>Triaxial Compression Test of Soils</u> Sample preparation, apparatus, and testing generally follow the procedures outlined in <u>Soil</u> <u>Testing for Engineers</u>, T.W. Lambe, John Wiley & Sons, Inc., New York, 1951 and in <u>The</u> <u>Measurement of Soil Properties in the Triaxial</u> <u>Test</u>, Alan W. Bishop & D.J. Henkel, 2nd Edition, St. Martin's Press, New York, 1962
- Unconfined Compression Strength of Cohesive Soil ASTM D 2166

- 7. <u>Specific Gravity of Soils</u> ASTM D 854
- Unit Weight Determination of Soils See ASTM D 2166 for preparation of specimen except that sample size may differ. For moisture content see ASTM D 2216.
- <u>Visual Identification of Soil Samples</u> All soil samples are visually identified and/or classified. The classification system used is shown in Table L-1.
- 10. Identification of Rock

Rock core samples are identified by the character and appearance of newly fractured surfaces of unweathered pieces, by core conditions and characteristics, and by the determination of simple physical and chemical properties.

- 11. Compaction Test of Soils
  - Moisture-density relations of soils using 5.5 lb. hammer and 12 in. drop, ASTM D 698
  - b. Moisture-density relations of soils using 10
     lb. hammer and 18 in. drop, ASTM D 1557
- Maximum and Minimum Densities of Granular Soils Testing procedures follow D.M. Burmeister, "Suggested Method of Test for Maximum and Minimum Densities of Granular Soils" cited in Proceedings for Testing Soils, Fourth Edition,
  - ASTM, Philadelphia. 1964, pp 175-177.
- Bearing Ratio of Laboratory Compacted Soils ASTM D 1883 (Sometimes called California Bearing Ratio or CBR)
- 14. Organic Content

A modified dichromate oxidation method using ferrous ammonium sulfate is employed in determining the percent of organic matter in soil.

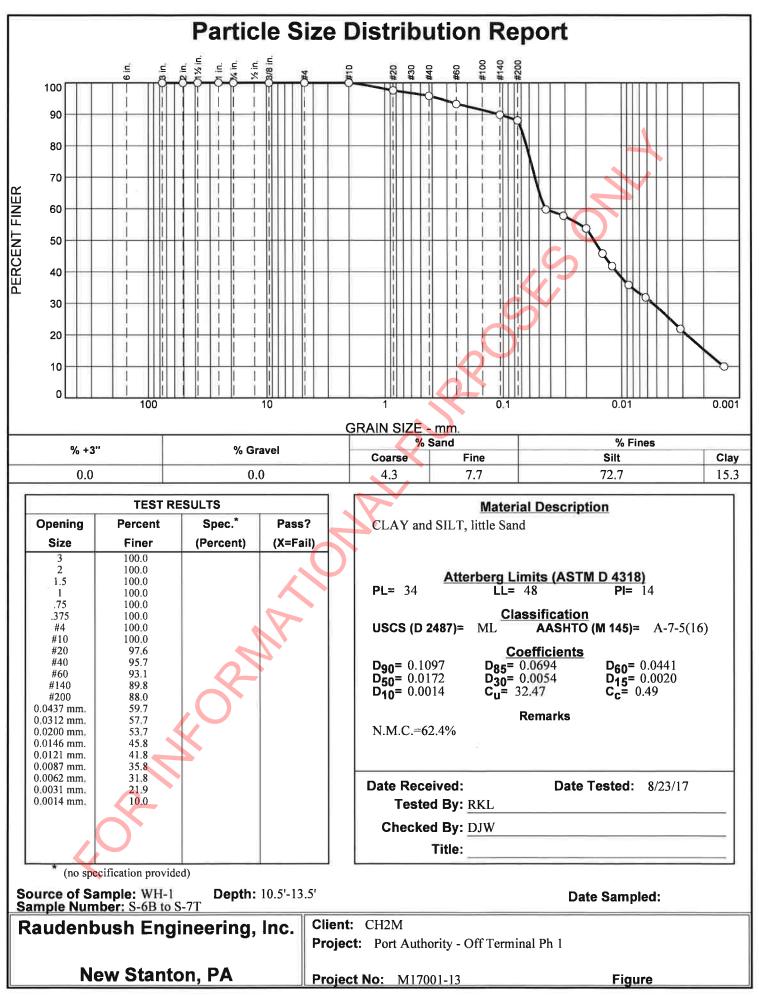


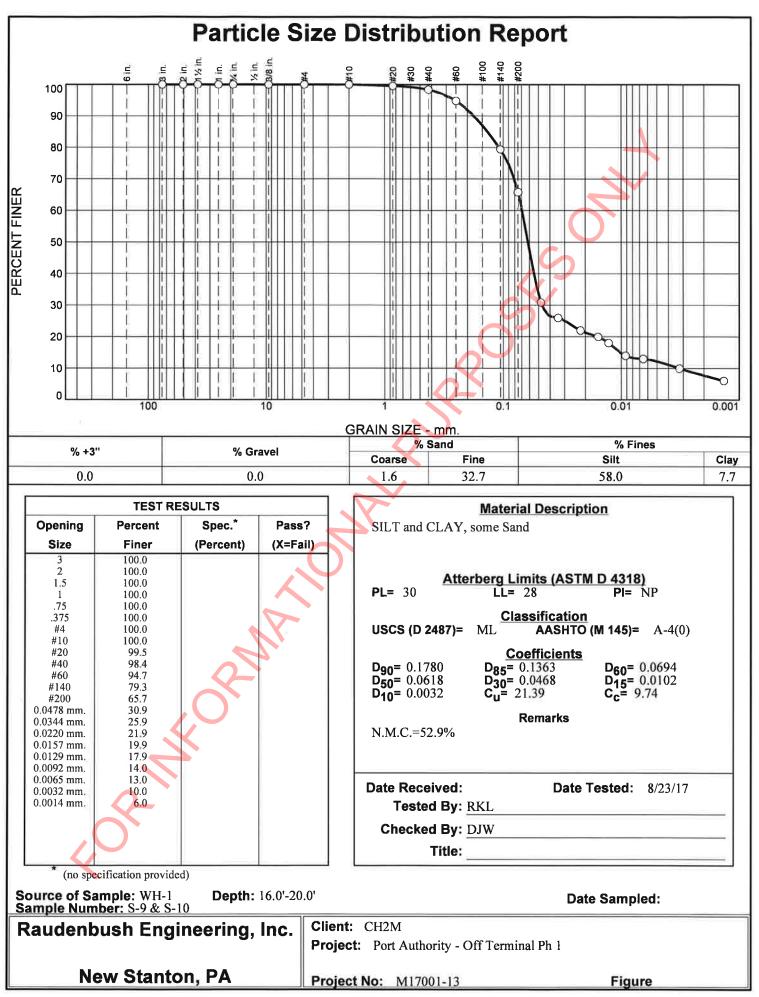
### WATER CONTENT DETERMINATION

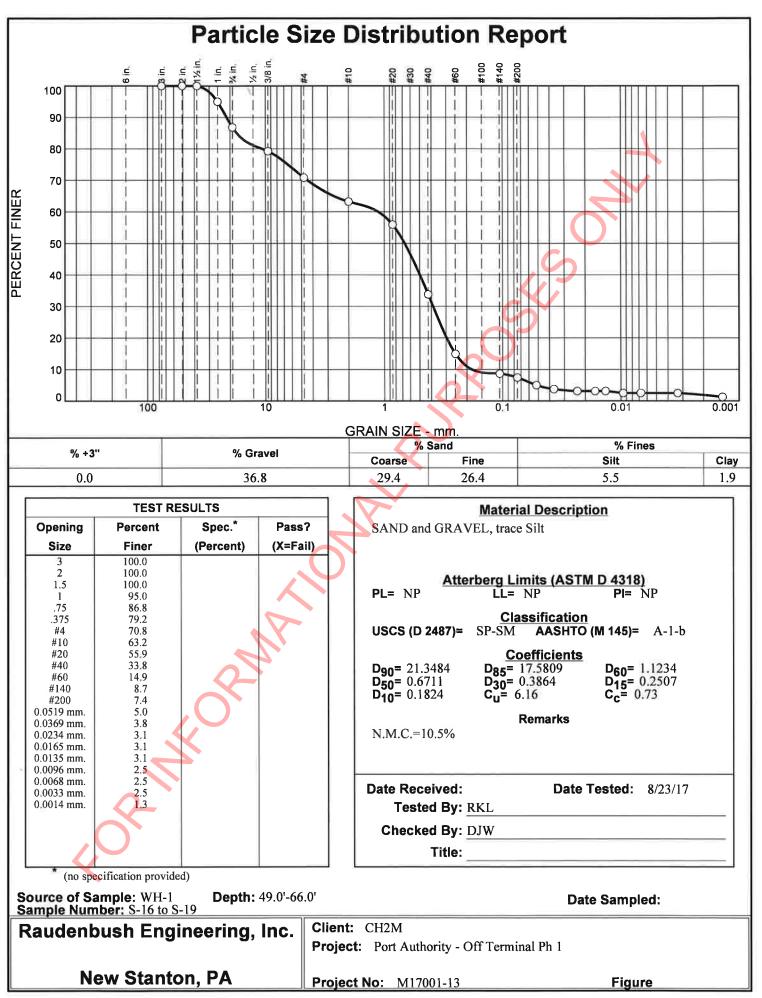
(ASTM D2216-10) / (AASHTO T265)

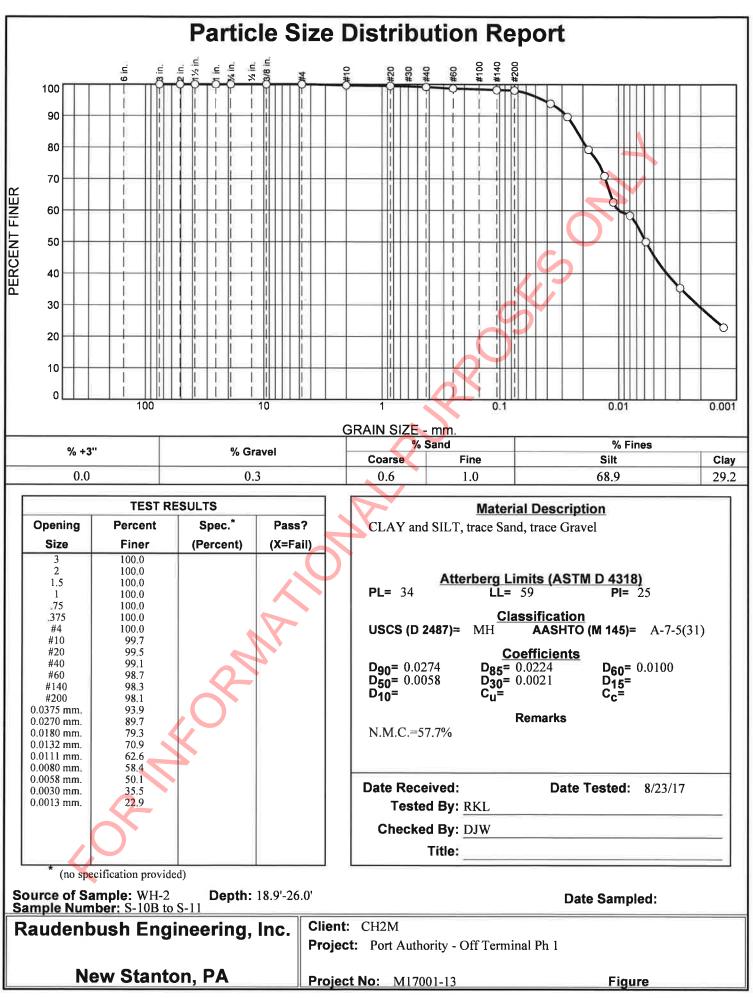
Client:	CH2M			Project #:	M17001-13
Project:	Port Authority Off-T	erminal Ph.	1	Test Date:	8/18/2017
Project Location:	Philidelphia, PA			Tested By:	RKL
j	,			Chk'd By:	MDH
				Cilled Dy.	
			0		
Lab Sample No.:	70213	70214	70215	70216	70217
Boring No.:	<b>WH-1</b>	<b>WH-1</b>	<b>WH-</b> 1	WH-2	WH-2
Depth (ft):	10.5-13.5	16.0-20.0	49.0-66.0	18.9-26.0	39.0-51.0
Sample No.:	S-6B & S-7T	S-9 & S-10	S-15 & S-16	S-10B & S-11	S-14 to S-16
Water Content (%):	62.4%	52.9%	10.5%	57.7%	13.4%
Lab Sample No.:	70218	70219	70220	70221	70222
Boring No.:	WH-2	WH-3	WH-3	WH-3	WH-4
Depth (ft):	54.0-61.0	14.0-18.0	29.0-36.0	74.0-76.0	55.0-61.0
Sample No.:	S-17 & S-18	S-8 & S-9	S-12 & S-13	S-21	S-17 & S-18
Water Content (%):	17.6%	19.8%	22.3%	22.2%	17.2%
Lab Sample No.:	70223				
Boring No.:	WH-5				
Depth (ft):	49.0-74.9				
Sample No.:	S-17 to S-21				
Water Content (%):	17.3%				
X					

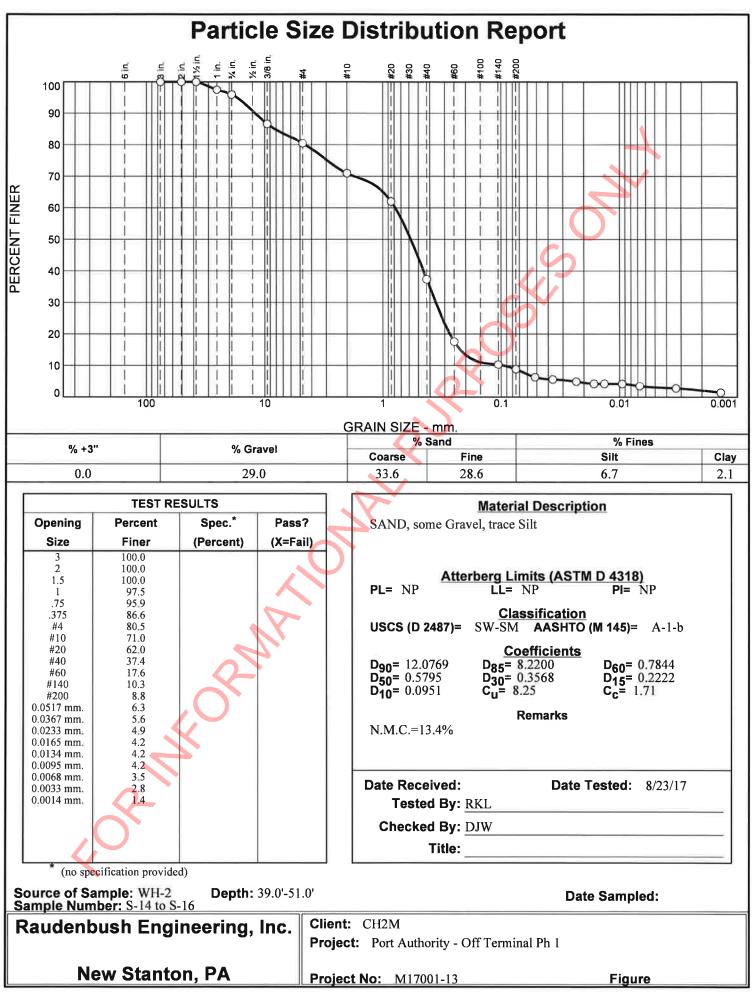
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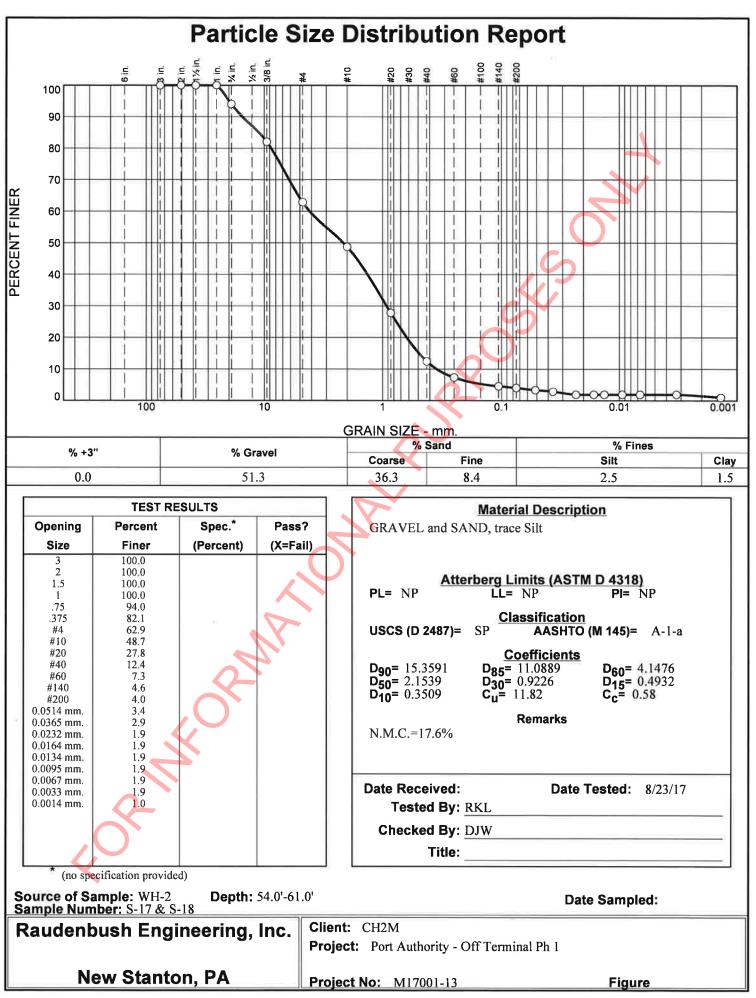


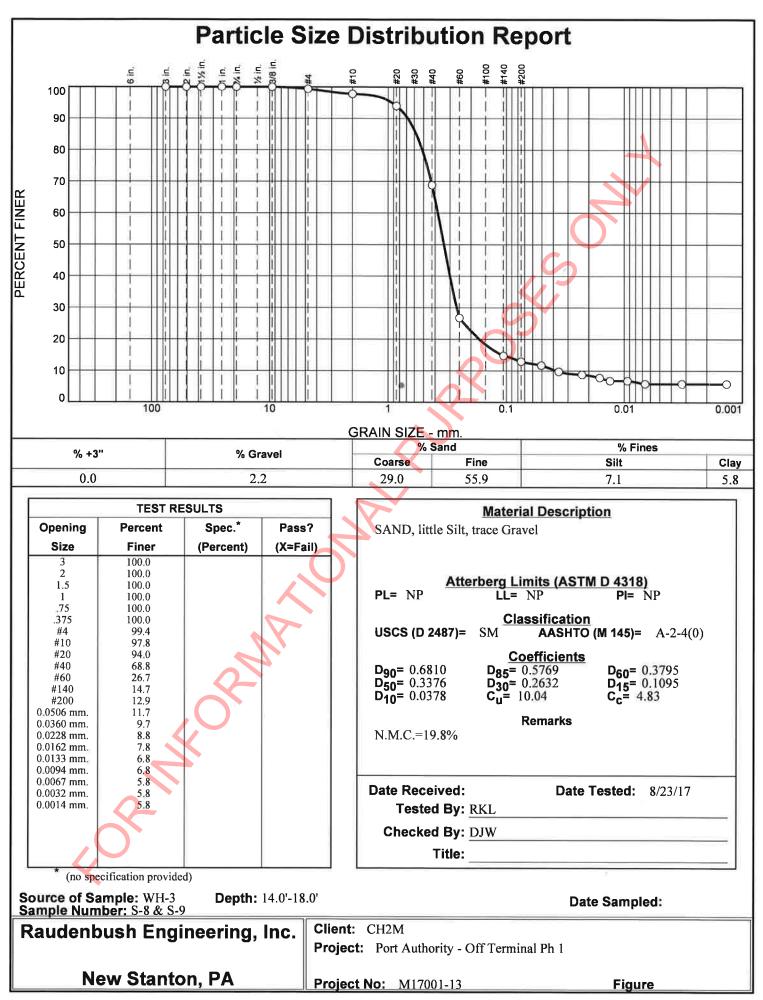




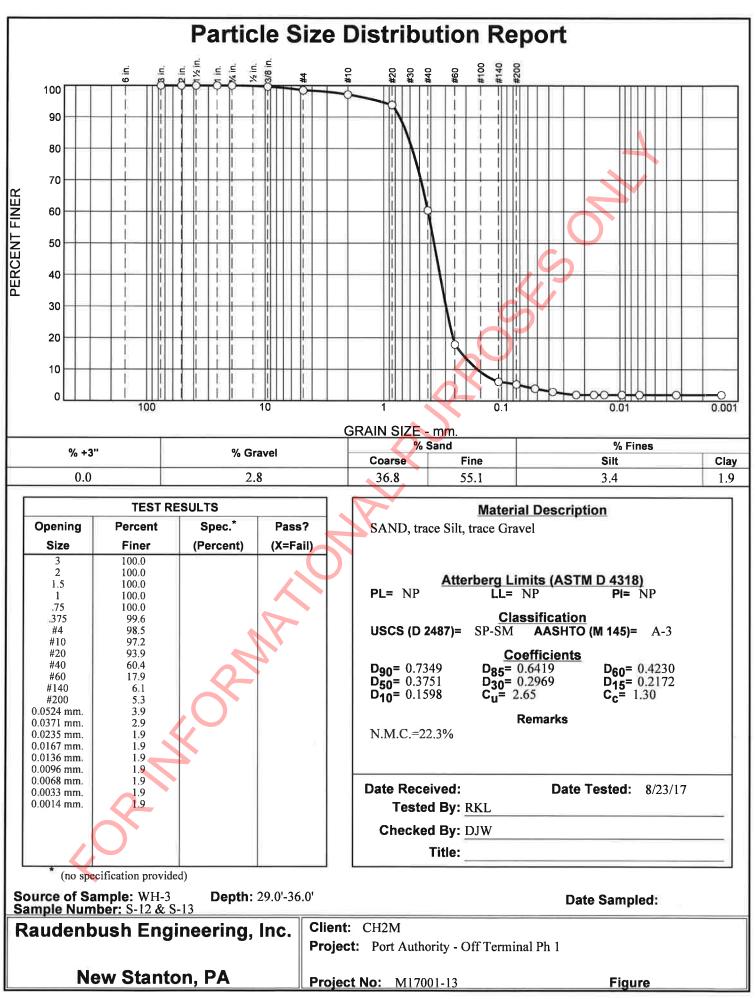




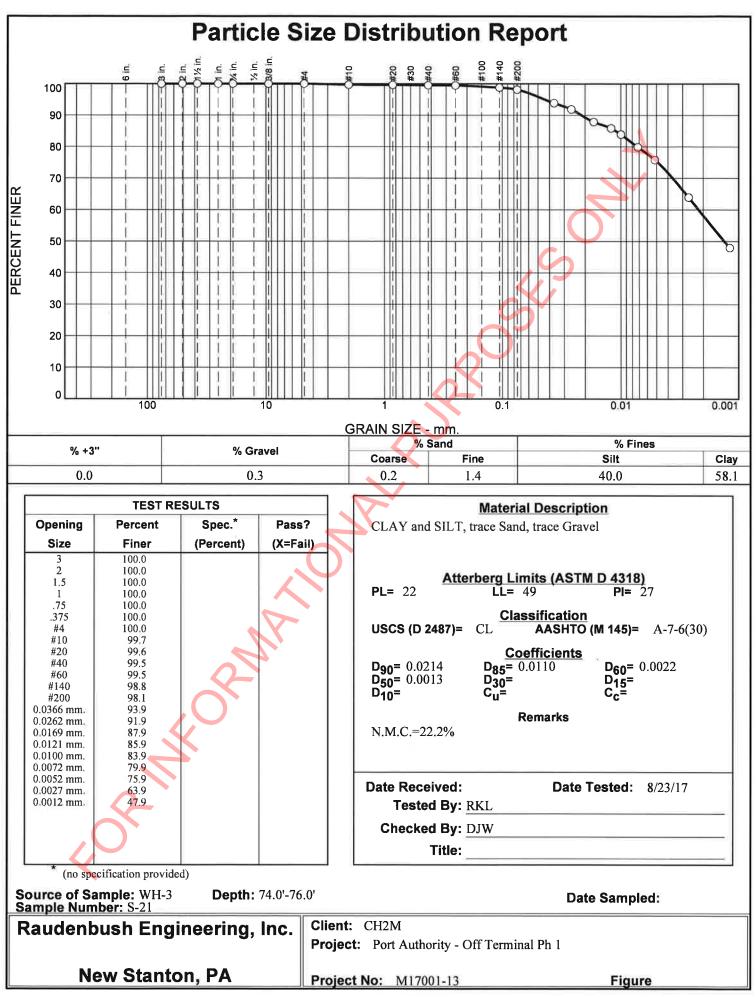


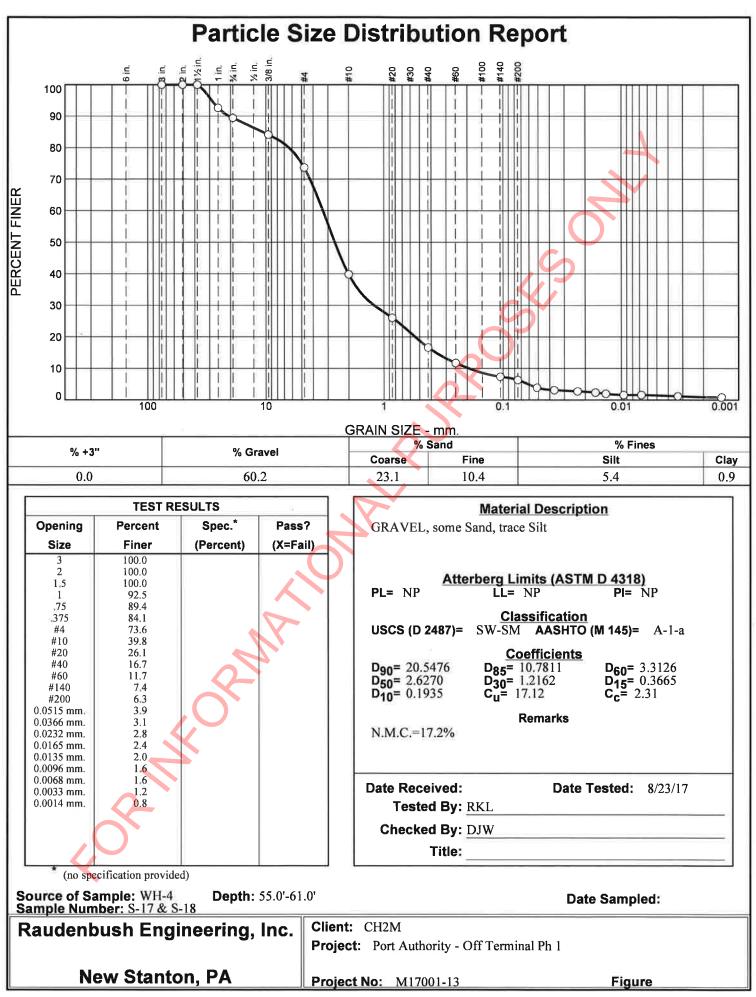


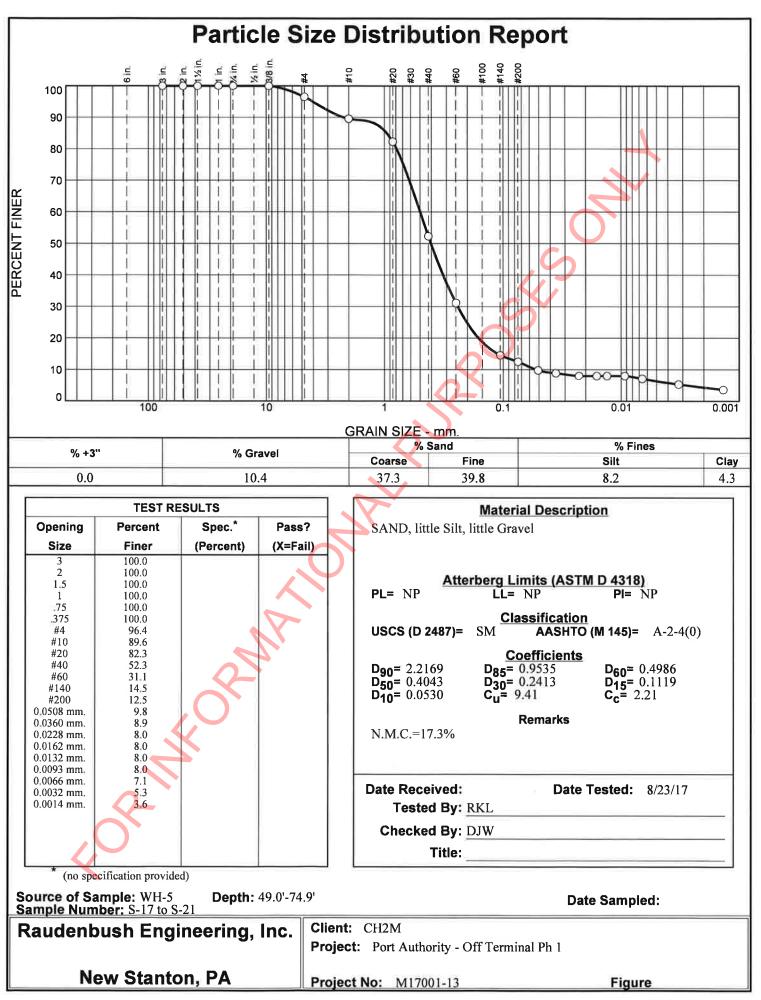
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### STANDARD SYMBOLS

В	Width of footing	Р	deviator stress			
с	cohesion	Pc	estimated probable preconsolidation pressure			
$c_{\rm v}$	coefficient of consolidation	Po	existing overburden pressure			
C _c C	compression index	$\mathbf{q}_{a}$	allowable soil bearing pressure			
C C ₃	coefficient of secondary compression swelling index	Q	triaxial compression test unconsolidated and undrained			
$C_u$	uniformity coefficient (D ₆₀ /D ₁₀₎	Qc	triaxial compression test consolidated and undrained			
CBR	California Bearing Ratio	S	triaxial compression test consolidated			
$\mathbf{D}_{\mathrm{f}}$	depth of foundation	2	and drained			
$D_p$	diameter of grain corresponding to percentage p on grain size curve	Sr v	degree of saturation pore-water pressure			
$D_{10}$	effective grain size	U	degree of consolidation			
Е	modulus of linear deformation	Uc	unconfined compression test			
		Wf	moisture content at end of test			
Es	Young's Modulus	$\mathbf{W}_1$	liquid limit			
e	void ratio	Wn	natural moisture content			
Fs	factor of safety	Wp	plastic limit			
		γ	unit weight			
G	specific gravity	$\boldsymbol{\gamma}_{\mathrm{d}}$	dry unit weight			
h	hydraulic head	<b>γ</b> ь	submerged unit weight			
Н	stratum thickness	ε	unit linear strain			
i	hydraulic gradient	$\boldsymbol{\epsilon}_{\mathrm{f}}$	unit linear strain at failure			
		σ	normal stress			
$I_L$	liquidity index	$\sigma_1$	major principal stress			
$I_P$	plasticity index	σ3	minor principal stress			
k	coefficient of permeability	τ	shear stress			
k _h	coefficient of horizontal subgrade	φ	angle of internal friction			
	reaction	ka	coefficient of active pressure			
k _v	coefficient of vertical subgrade	$\mathbf{k}_{\mathbf{p}}$	coefficient of passive pressure			
·	reaction	δ	friction angle			
1	length of footing	tan <b>δ</b>	friction factor			
n	porosity					

55 Le Pave APPEDIX D – Pavement Thickness



			-
Boring No.	Thickness of Bituminous Concrete (in)	Thickness of Processed Aggregate (in)	
B-1	5	7	
B-2	5	6	
B-3	5		
B-4	6		
B-5	5		
B-6	8	5	
B-7	7		
B-8	5		
B-9	6	4	
B-10	5		
B-11	4	6*	
B-12	4	6*	
B-13	7	2	
B-14		12	
B-15			
B-16			
B-17			
B-18			
B-19		6	
B-20	6	1	

TABLE 1 – Pavement Thickness in Borings Performed During 2017 Study TABLE 2 – Pavement Thickness in Test pits Performed During 2019 Study

Test-pit No.	Thickness of Bituminous Asphalt (in)	Thickness of Processed Aggregate (in)
TP-1	4	8
TP-2	4	8
TP-3	4	8
TP-4	4	8
TP-5	4	8
TP-6	2.5	9.5
TP-7	0.5	0.5
TP-8	4	8
TP-9	4	8
TP-10	4	8
P-1**	6	6
P-2**	5	9
P-3	5	8
P-4	4	11
P-5	4	8
P-6**	4	9
P-7	4	10
P-8	4	10
P-9	7	6
P-10**	4	8.5

*: Noted in boring logs as "Concrete"

**: Sand noted below processed aggregate

ion vt ' **APPEDIX E – Important Information** is Ge. About This Geotechnical Engineering Report by GBA



# Important Information about This Geotechnical-Engineering Report

Subsurface problems are a principal cause of construction delays, cost overruns, claims, and disputes.

While you cannot eliminate all such risks, you can manage them. The following information is provided to help.

# Geotechnical Services Are Performed for Specific Purposes, Persons, and Projects

Geotechnical engineers structure their services to meet the specific needs of their clients. A geotechnical-engineering study conducted for a civil engineer may not fulfill the needs of a constructor — a construction contractor — or even another civil engineer. Because each geotechnical- engineering study is unique, each geotechnical-engineering report is unique, prepared *solely* for the client. No one except you should rely on this geotechnical-engineering report without first conferring with the geotechnical engineer who prepared it. *And no one* — *not even you* — should apply this report for any purpose or project except the one originally contemplated.

#### **Read the Full Report**

Serious problems have occurred because those relying on a geotechnical-engineering report did not read it all. Do not rely on an executive summary. Do not read selected elements only.

# Geotechnical Engineers Base Each Report on a Unique Set of Project-Specific Factors

Geotechnical engineers consider many unique, project-specific factors when establishing the scope of a study. Typical factors include: the client's goals, objectives, and risk-management preferences; the general nature of the structure involved, its size, and configuration; the location of the structure on the site; and other planned or existing site improvements, such as access roads, parking lots, and underground utilities. Unless the geotechnical engineer who conducted the study specifically indicates otherwise, do not rely on a geotechnical-engineering report that was:

- not prepared for you;
- not prepared for your project;
- not prepared for the specific site explored; or
- completed before important project changes were made.

Typical changes that can erode the reliability of an existing geotechnical-engineering report include those that affect:

- the function of the proposed structure, as when it's changed from a parking garage to an office building, or from a lightindustrial plant to a refrigerated warehouse;
- the elevation, configuration, location, orientation, or weight of the proposed structure;
- the composition of the design team; or
- project ownership.

As a general rule, *always* inform your geotechnical engineer of project changes—even minor ones—and request an

assessment of their impact. Geotechnical engineers cannot accept responsibility or liability for problems that occur because their reports do not consider developments of which they were not informed.

### Subsurface Conditions Can Change

A geotechnical-engineering report is based on conditions that existed at the time the geotechnical engineer performed the study. *Do not rely on a geotechnical-engineering report whose adequacy may have been affected by*: the passage of time; man-made events, such as construction on or adjacent to the site; or natural events, such as floods, droughts, earthquakes, or groundwater fluctuations. *Contact the geotechnical engineer before applying this report to determine if it is still reliable.* A minor amount of additional testing or analysis could prevent major problems.

#### Most Geotechnical Findings Are Professional Opinions

Site exploration identifies subsurface conditions only at those points where subsurface tests are conducted or samples are taken. Geotechnical engineers review field and laboratory data and then apply their professional judgment to render an opinion about subsurface conditions throughout the site. Actual subsurface conditions may differ — sometimes significantly — from those indicated in your report. Retaining the geotechnical engineer who developed your report to provide geotechnical-construction observation is the most effective method of managing the risks associated with unanticipated conditions.

### A Report's Recommendations Are Not Final

Do not overrely on the confirmation-dependent recommendations included in your report. *Confirmationdependent recommendations are not final*, because geotechnical engineers develop them principally from judgment and opinion. Geotechnical engineers can finalize their recommendations *only* by observing actual subsurface conditions revealed during construction. *The geotechnical engineer who developed your report cannot assume responsibility or liability for the report's confirmation-dependent recommendations if that engineer does not perform the geotechnical-construction observation required to confirm the recommendations' applicability.* 

# A Geotechnical-Engineering Report Is Subject to Misinterpretation

Other design-team members' misinterpretation of geotechnical-engineering reports has resulted in costly

problems. Confront that risk by having your geotechnical engineer confer with appropriate members of the design team after submitting the report. Also retain your geotechnical engineer to review pertinent elements of the design team's plans and specifications. Constructors can also misinterpret a geotechnical-engineering report. Confront that risk by having your geotechnical engineer participate in prebid and preconstruction conferences, and by providing geotechnical construction observation.

### Do Not Redraw the Engineer's Logs

Geotechnical engineers prepare final boring and testing logs based upon their interpretation of field logs and laboratory data. To prevent errors or omissions, the logs included in a geotechnical-engineering report should *never* be redrawn for inclusion in architectural or other design drawings. Only photographic or electronic reproduction is acceptable, *but recognize that separating logs from the report can elevate risk.* 

# Give Constructors a Complete Report and Guidance

Some owners and design professionals mistakenly believe they can make constructors liable for unanticipated subsurface conditions by limiting what they provide for bid preparation. To help prevent costly problems, give constructors the complete geotechnical-engineering report, but preface it with a clearly written letter of transmittal. In that letter, advise constructors that the report was not prepared for purposes of bid development and that the report's accuracy is limited; encourage them to confer with the geotechnical engineer who prepared the report (a modest fee may be required) and/ or to conduct additional study to obtain the specific types of information they need or prefer. A prebid conference can also be valuable. Be sure constructors have sufficient time to perform additional study. Only then might you be in a position to give constructors the best information available to you, while requiring them to at least share some of the financial responsibilities stemming from unanticipated conditions.

#### Read Responsibility Provisions Closely

Some clients, design professionals, and constructors fail to recognize that geotechnical engineering is far less exact than other engineering disciplines. This lack of understanding has created unrealistic expectations that have led to disappointments, claims, and disputes. To help reduce the risk of such outcomes, geotechnical engineers commonly include a variety of explanatory provisions in their reports. Sometimes labeled "limitations," many of these provisions indicate where geotechnical engineers' responsibilities begin and end, to help others recognize their own responsibilities and risks. *Read these provisions closely*. Ask questions. Your geotechnical engineer should respond fully and frankly.

### **Environmental Concerns Are Not Covered**

The equipment, techniques, and personnel used to perform an *environmental* study differ significantly from those used to perform a *geotechnical* study. For that reason, a geotechnicalengineering report does not usually relate any environmental findings, conclusions, or recommendations; e.g., about the likelihood of encountering underground storage tanks or regulated contaminants. *Unanticipated environmental problems have led to numerous project failures*. If you have not yet obtained your own environmental information, ask your geotechnical consultant for risk-management guidance. *Do not rely on an environmental report prepared for someone else.* 

# Obtain Professional Assistance To Deal with Mold

Diverse strategies can be applied during building design, construction, operation, and maintenance to prevent significant amounts of mold from growing on indoor surfaces. To be effective, all such strategies should be devised for the express purpose of mold prevention, integrated into a comprehensive plan, and executed with diligent oversight by a professional mold-prevention consultant. Because just a small amount of water or moisture can lead to the development of severe mold infestations, many mold- prevention strategies focus on keeping building surfaces dry. While groundwater, water infiltration, and similar issues may have been addressed as part of the geotechnical- engineering study whose findings are conveyed in this report, the geotechnical engineer in charge of this project is not a mold prevention consultant; none of the services performed in connection with the geotechnical engineer's study were designed or conducted for the purpose of mold prevention. Proper implementation of the recommendations conveyed in this report will not of itself be sufficient to prevent mold from growing in or on the structure involved.

### Rely, on Your GBC-Member Geotechnical Engineer for Additional Assistance

Membership in the Geotechnical Business Council of the Geoprofessional Business Association exposes geotechnical engineers to a wide array of risk-confrontation techniques that can be of genuine benefit for everyone involved with a construction project. Confer with you GBC-Member geotechnical engineer for more information.





GEOTECHNICAL BUSINESS COUNCIL of the Geoprofessional Business Association

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